

KLEIN ROAD
Phase 2
Summary of Needs Study

August 2018

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Klein Road Phase 2 Summary of Needs Study

EXECUTIVE SUMMARY

Pape-Dawson Engineers, Inc. (Pape-Dawson) was contracted to perform preliminary engineering services in support of developing a bond level estimate for Klein Road Phase 2 (Project). The subject roadway is in Guadalupe County south of IH-35, west of Lake Dunlap in the City of New Braunfels (City). Project limits are from S Walnut Ave to FM 725. The parcels along the 0.96-mile corridor include residential low density and open land uses with zoning consisting of single-family, two-family, and agricultural/pre-development districts.

Project development will proceed through schematic phase with an estimated construction cost. PS&E and Construction phases are pending voter approval of the May 2019 Proposed Bond Program.

The City is holding a public meeting on September 11, 2018 to engage the community and agency stakeholders. Feedback from this meeting may establish additional Project needs and will be incorporated where possible into the schematic design.

Detailed survey, environmental, and geotechnical services were deferred to PS&E phase at the request of the City until additional funding for those activities becomes available. Assumptions related to those disciplines are documented in the Summary of Needs Study based on field observations and information provided by the City from Klein Road Phase 1. Pape-Dawson has identified risks in proceeding with schematic design in these areas, including possible typical section element modification or elimination at PS&E phase if factors detrimental to the Project cost, schedule, or permitting become known at that time.

The Summary of Needs Study includes detailed analysis for roadway, temporary traffic control plan, drainage, and traffic operations along Klein Road. See below for a summary of the key findings:

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Roadway

- Apparent right of way (ROW) is narrow (60-75 feet) relative to the roadway's Minor Arterial designation, which requires a 70' ROW. The City's standard Minor Arterial typical section cannot be met without ROW acquisition
- ROW acquisition is needed to the east side
- Multiple overhead and underground utilities are anticipated to conflict with proposed improvements due to narrow ROW and sidewalk/shared-use path locations

Temporary Traffic Control

- Road closure at an existing low water crossing will be required during construction. Detour routes will have minimal impacts on emergency service response times when dispatched from area emergency service stations
- Detour routes will affect a small subset of school-bound roadway users within the attendance zones of Klein Road Elementary and New Braunfels Middle Schools

Drainage

- A storm sewer system is needed to replace the existing drainage swales and provide relief to the Ranch Estates community along Bonnies Way, an area of noted offsite flooding
- An existing low water crossing needs to be replaced due to safety concerns during inclement weather. Two alternatives are presented to replace the crossing: a bridge-class multi-box culvert or a span bridge on drilled shafts

Traffic

- Each roadway intersection studied (S Walnut Ave, Roadrunner Ave/Stoeger Dr, Dove Crossing Dr, and FM 725) currently operates at an acceptable level of service C or better
- Projected annual traffic growth is estimated to be 5% per year, causing each intersection to operate at an unacceptable level of service by 2040
- A 4-lane roadway section with a median for left turn channels is needed to meet 2040 projected traffic demands, which is incompatible with existing ROW
- Alternative lane configurations and innovative intersection designs have been identified to maximize capacity improvements in areas of feasible ROW acquisition

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1 INTRODUCTION

Pape-Dawson Engineers, Inc. (Pape-Dawson) was contracted to perform preliminary engineering services in support of developing a bond level estimate for Klein Road Phase 2 (Project). The subject roadway is in Guadalupe County south of IH-35, west of Lake Dunlap in the City of New Braunfels (City). Project limits of the 0.96-mile study corridor are from S Walnut Ave to FM 725, which serves as the northern extension of Klein Road Phase 1—a project under construction at time of study from FM 1044 to S Walnut Ave.

1.1 Purpose

The Project is under consideration for inclusion in the City's 2019 Proposed Bond Program – a funding mechanism (pending voter approval) that will enable regional infrastructure improvements to address current and expected community growth. The 2012 New Braunfels Regional Transportation Plan (RTP, see **Appendix A1**) indicates ultimate configuration of Klein Road as a 'Minor Arterial,' a City designation for a roadway with 70' right of way (ROW), 4~12' lanes, curb, and sidewalk on both sides (see **Appendix A2**). Existing Klein Road consists of 2~12' lanes, no curb, drainage swales, and an isolated sidewalk segment not connected with the area's broader pedestrian facility network. Significant infrastructure investment is needed to meet the vision for Klein Road established in the RTP, the timing of which will be critical to keeping up with traffic demand. Although existing intersections perform at level of service C or better (see **Section 5.1 Existing Conditions**), future annual traffic growth is estimated at 5% -- an indication that existing roadway infrastructure will quickly become undersized relative to demand if no action is taken.

If funded, the Project will include the expansion of Klein Road, utility adjustments/relocations, traffic control, drainage, signing, pavement marking, illumination, sidewalk and shared use path improvements.

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In addition to serving adjacent residential and commercial land uses, Klein Road provides access to an existing elementary school, middle school, school district transportation center, three churches, and a planned major sports complex. These factors establish Klein Road as a key north-south link in the area's transportation network to distribute high traffic volumes during peak hours and special events. Klein Road Phase 1 improvements are currently under construction and address current and expected traffic demand through additional roadway capacity and intersection improvements at FM 1044 and S Walnut Ave, defined in the RTP as Parkway and Principal Arterial respectively. Klein Road Phase 2 extends Phase 1 improvements to the next Principal Arterial north, FM 725. This provides an extended and continuous Minor Arterial typical section between three major east-west roadways that provide regional access to IH-35. When completed, Klein Road Phases 1 and 2 will address current and growing traffic demand, primarily driven by residential development of existing agricultural/pre-development districts.

According to the RTP, a new location roadway (Mary Blvd) will extend Klein Road's Minor Arterial section north from FM 725 across the Guadalupe River, terminating at SH 46. Once realized, the Klein/Mary corridor will serve as a 5-mile long parallel north-south alternative to County Line Road and IH-35, providing regional traffic congestion relief. While the Mary corridor is currently unfunded, constructing Klein Road Phase 2 is the logical next step for the City to address current and expected growth.

2 ROADWAY

Comprehensive roadway improvement needs are examined with respect to existing land use and right of way acquisition; zoning and future land use; bicycle and pedestrian facilities, community involvement, pavement evaluation, and utilities.

2.1 Existing Land Use and Right Of Way Acquisition

Existing land uses of parcels adjacent to the Project corridor include: Residential Low Density (less than 5 units/acre), Open, Drainage, Commercial, Institution, and Schools. The apparent

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ROW established by these parcels, based on observed features and publicly available parcel data from the Guadalupe County Appraisal District, varies in width from approximately 60-75 feet. ROW widths are inconsistent and can be attributed to asymmetric development, or ROW dedication, along the corridor. Most development has occurred to the west, creating a uniform ROW limit (ie, a nearly constant offset west of existing Klein Road's centerline). In contrast, the eastern ROW line is an inconsistent offset from existing Klein Road's centerline: ~60' offset from the western ROW limit at undeveloped eastern parcels, ~70' where development has occurred on both sides of the roadway.

The path of least resistance for potential ROW acquisition lies on the east side of the road due to fewer affected owners and lower property values. Acquiring approximately 10' of additional ROW from 11 open, commercial, and institutional parcels would provide a uniform 70' ROW to accommodate the Minor Arterial typical section. Acquiring additional ROW beyond 70' is infeasible as doing so would require acquisition from an additional 16 developed parcels if acquired on the east side only (48 parcels if acquisition is done symmetrically about the existing Klein Road centerline). Additionally, acquisition of ROW from developed parcels would greatly increase the cost of acquisition and impact of the Project on the community it serves. Thus, the Minor Arterial typical section is the largest feasible for the corridor and requires ROW acquisition.

An existing Klein Road schematic was developed for the entire Klein Road Phase 1 and Phase 2 limits as part of the Klein Road Phase 1 project. Pape-Dawson examined the portion of the schematic covering the Project limits for a comparison of ROW acquisition needs with the following observations:

- The existing schematic does not propose ROW acquisition where development has occurred on both sides of the roadway between Benneli Dr and Roadrunner Ave/Stoeger Dr – this is consistent with Pape-Dawson's determination that ROW acquisition at this location is infeasible.

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- ROW acquisition was proposed along the east and west sides of the road from S Walnut Ave to Wise Owl for a total ROW width of 78'-102'. Due to the maximum 70' ROW available between Benneli Dr and Roadrunner Ave/Stoeger Dr, acquisition of ROW to the west provides little additional benefit.
- “Corner Clips” at Quail Ridge Dr and Benneli Dr are non-standard, rectangular in shape that may limit available intersection sight distance. Larger, chamfered ROW “corner clips” are needed at these locations.

Apparent ROW will establish the boundary for concept design alternatives and schematic design, as conventional survey of actual ROW and easement limits has been deferred until the PS&E phase (see **Section 7 SURVEY**). Using apparent ROW is a concern for the schematic phase, as design is based on approximated ROW limits. If existing ROW is determined at PS&E phase to be more restrictive than apparent ROW (or outside stakeholders control easements within areas to be acquired), schematic design features may be subject to adjustment or elimination at PS&E phase.

2.2 Zoning and Future Land Use

The zoning of parcels adjacent to the Project corridor include: APD (Agricultural/Pre-Development), C-1B (General Business), C-3 (Commercial), PD (Planned Development), R-1A-6.6 (Single-Family), and R-2A (Single-Family and Two-Family) districts. The City’s future land use maps indicate residential low density to the east for nearly the entire corridor limits, with commercial development expected near the project’s termini (S Walnut Ave and FM 725). These observations form the basis for expected development and associated traffic projections further detailed in **Section 5.2 Traffic Projections**.

2.3 Bicycle and Pedestrian Facilities

An isolated 5-foot wide sidewalk segment exists on the east side of Klein Road from Benelli Dr to Roadrunner Ave/Stoeger Dr (see **Figure 1**). No other existing pedestrian or bicycle facilities exist

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within the project limits. Prior City direction has been to explore opportunities to bring connectivity to isolated bicycle or pedestrian facilities where possible.



Figure 1: Klein Road Existing Pedestrian Facilities

The 2010 City of New Braunfels Hike and Bike Trail Plan (**Appendix A6**) identifies the Project corridor for a future hike and bike trail. If constructed, the Project's bicycle and pedestrian improvements will extend an existing shared use path along S Walnut Ave, similar facilities currently under construction within Klein Road Phase 1, and provide future connectivity with off-street trails envisioned along an existing drainage channel Guadalupe River Tributary 22 (see

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Section 4 DRAINAGE) and FM 725. Additionally, the Project will connect the isolated internal pedestrian facility networks of the White Wing, Dove Crossing, Ranch Estates, and Whispering Valley subdivisions enabling a fully walkable community.

Due to restrictive ROW between Benelli Dr and Roadrunner Ave/Stoeger Dr, separate off-street bicycle and pedestrian facilities are not considered feasible. However, a 10' shared use path offers the most compact solution to fulfilling the Hike and Bike Plan vision and connecting existing pedestrian facility networks. This is consistent with the existing schematic prepared during Klein Road Phase 1 development – a 10' shared use path is indicated on the east side of the road with 6' sidewalk on the west (see **Appendix A5**).

Key criteria governing the horizontal layout of sidewalk and shared use paths relates to the clear width provided along the route. Above-ground features such as mailboxes, utility poles or pedestals, or traffic signal equipment commonly present obstructions to or restrictions on the clear width that can be achieved. The Proposed Accessibility Guidelines for Pedestrian Facilities in the Public Right-of-Way (PROWAG) and the AASHTO Guide for the Planning, Design, and Operation of Bicycle Facilities (PDOBF) will govern the areas viable for above-ground feature placement relative to sidewalks and shared use paths.

Based on the AASHTO criteria review, a 5' minimum separation of the shared use path from the back of curb is required, otherwise a physical barrier is needed to separate the vehicular and bicycle/pedestrian facilities. No above-ground feature may be placed within the shared use path or within a 2' buffer zone either side of the shared use path. Thus the 3' of space remaining between the back of curb and the buffer zone may contain above-ground features. Conversely, sidewalks offer more flexibility for reduced clear width than shared use paths in that the minimum clear width is 4 feet exclusive of the width of the curb. If ROW determinations during PS&E phase present a challenge to fitting the standard 10' shared use path with 5' separation from back of curb, the 6' wide western sidewalk may be subject to width reduction (4' minimum) or

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elimination if utility placement dictates or ROW cannot be acquired. Existing utilities and their placement relative to these facilities is discussed further in **Section 2.6 Utilities**.

2.4 Community Involvement

Klein Road Phase 1 design included a public meeting to obtain community input regarding concerns along Klein Road and suggestions for proposed improvements. Comments received from the public focused on drainage and traffic issues such as:

- Downstream flooding at the cross culvert under S Walnut Ave
- Design Speed and Marked Speed Limit perceived as being too low
- Traffic control (access to emergency services, area schools, and increased delays during construction)

Public comments from Phase 1 design will be considered for Phase 2 design where applicable. Pape-Dawson will participate in a City-led public meeting to be held on September 11, 2018 and present the Project schematic design to receive additional input from the public.

2.5 Pavement Evaluation

Existing pavement conditions within the Project limits are similar to those described in the Klein Road Phase 1 Geotechnical Engineering Study, where noted pavement deficiencies included rutting, longitudinal and edge cracking in the outer tire paths in both directions of travel. The sources of pavement deficiencies were examined through soil borings at 12 locations within the Klein Road Phase 1 limits. The geotechnical engineer's findings cited significant swell/heave potential of the pavement (2.5-6.25 inches) due to the subsurface stratigraphy "generally described as highly plastic, dark brown clay overlying hard, plastic to highly plastic tan clay," soil types known for high susceptibility for swell/heave in the presence of water. Swell/heave mitigation strategies recommended in the Klein Road Phase 1 Geotechnical Engineering Study included: "soil treatment with lime or other chemicals, removal and replacement of high plasticity index soils,

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and drains or barriers to collect or inhibit moisture infiltration.” Of these strategies, the Klein Road Phase 1 project adopted 12” of lime treated subgrade, 9” flexible base, Tensar TX-5 geogrid, and 4” of hot mixed asphalt concrete. The Project will match Klein Road Phase 1 pavement section elements to develop a bond-level estimate of construction cost of pavement elements, however, the soil stratigraphy and recommended mitigation for swell/heave may change after more detailed geotechnical investigation is performed at PS&E phase.

2.6 Utilities

Klein Road Phase 2 utility locations were obtained through a Quality Level D investigation utilizing field observations of surface features, utility maps provided by the City, and Texas 811 One Call utility location services. Quality Level D data establishes the utility providers in the area and their general line locations but is not intended to serve as design level information. See **Appendix A7** for an existing utility base map indicating Quality Level D approximate utility locations. **Table 1** includes a summary of the utility types and owners known to exist within the project limits. The Project’s schematic design will avoid as many utility conflicts as feasible, identify specific areas of concern, affected owners, and recommended relocation/mitigation strategies.

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Table 1: Existing Utility Types and Owners

| <u>Utility Type</u> | <u>Utility Owner</u> | <u>Notes</u> |
|----------------------------|-----------------------------------|---|
| Underground Communications | AT&T | Along east and west side of road |
| Gas | CenterPoint Energy | Existing stub just north of S Walnut Ave |
| Overhead Communications | Green Valley Electric Cooperative | Along east side of road on GVEC poles with various crossings west |
| Overhead Electric | | Along east side of road |
| Water | Green Valley SUD | 12" PVC, runs along east side of road with some crossings to west, some water easements exist |
| Sanitary Sewer | Guadalupe-Blanco River Authority | East side of road, outside of ROW (not within project limits) |
| Sanitary Sewer | New Braunfels Utilities | West side of road, outside of ROW (not within project limits) |
| Overhead Communications | Spectrum | Along east side of road on GVEC poles with various crossings west |
| Underground Communications | | Crossing from east side to west at various locations with small segments on west side of road |
| Underground Communications | ZAYO | Intersection of W Klein Road & FM 725 |

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Pape-Dawson anticipates multiple utility conflicts with the Project improvements. Conflicts are listed by type, including:

Pole mounted utilities

- Utility poles and pole mounted utilities (overhead electric and communications) will conflict with bicycle and pedestrian facilities primarily on the east side of the roadway due to existing pole placement relative apparent ROW. Based on the Minor Arterial typical section, the travel lanes will be widened within 1-2' of the existing eastern ROW limit, leaving little room for the bicycle and pedestrian facilities envisioned for the corridor (see **Section 2.3 Bicycle and Pedestrian Facilities**). Bicycle and pedestrian facilities on the east side of the road will generally occupy the portion of ROW to be acquired. Allowing pole mounted utilities to remain in areas of ROW acquisition would violate PDOBF criteria for shared use path width, clearance, and lateral buffer zones. Therefore, utility poles will need to be relocated to the eastern acquired ROW limits to avoid conflict with bicycle and pedestrian facilities. An alternative would be to relocate those conflicting facilities to the west side of the roadway where utility poles may encroach on the sidewalk up to a minimum of 4' clear width provided at the narrowest locations. Secondly, existing pole mounted utilities could be relocated underground to avoid conflict with bicycle and pedestrian facilities altogether. Consolidation of existing overhead and underground electric and telecommunications utilities in an underground utility corridor (ie, duct banks) offers the most compact solution to mitigating conflicts with bicycle and pedestrian facilities but are typically more costly to construct than pole mounted utilities.

Underground utilities

- Underground communication lines will conflict with storm sewer, pavement section, shared-use path, and sidewalk improvements. Existing underground telecommunications lines run parallel to the roadway on both sides, limiting potential horizontal placement of storm sewer facilities outside the roadway. Additionally, lateral underground

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communication lines consist of coaxial lines with 24” cover and fiber lines with 36” cover. If the pavement section adopted for the Project closely matches that of Klein Road Phase 1, the minimum depth of excavation is 25”, excluding profile adjustments that may raise or lower the roadway at these locations. Thus, the depth of pavement section over existing lateral communication lines establishes a need to lower those lines to avoid potential disruption due to construction activities. Existing utility pedestals serving underground telecommunication utilities north of Ranch Estates Blvd will conflict with the clear width requirements for sidewalk improvements in the area if not relocated. The proposed design will also widen the roadway or add sidewalk/shared-use path facilities above existing underground communication lines, which will lead to costly future maintenance if these underground utilities are not relocated to grass parkway portions of the typical section.

- The existing 12” water main runs parallel to Klein Road on the east side but has lateral connections to the west side at multiple locations. While the depth of the water main is unknown, it is assumed to conflict with storm sewer improvements at a minimum of 5 lateral crossing locations (1 per residential subdivision street intersecting Klein Road from the west) and 5 service taps for lots with Klein Road frontage. Lateral and service tap connections will need to be relocated deeper underground to avoid conflicts with the proposed storm sewer system. The water main east of the road is far enough removed from the road that it should not conflict with proposed improvements. However, Klein Road Phase 1 improvements included relocating and increasing the size of an existing water main. These same improvements will be considered for Phase 2 if the existing 12” water line is nearing end of life cycle or if the utility owner indicates future upgrades are needed to meet demand of adjacent development.
- Sanitary sewer utilities were identified within existing residential subdivisions on both sides of Klein Road, but no lines were observed within the apparent ROW. Klein Road serves as the “sewer divide” for the area, meaning two different sanitary sewer service

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providers (New Braunfels Utilities and Guadalupe-Blanco River Authority) maintain separate sanitary sewer service areas on either side of Klein Road. There were no observed sanitary sewer crossings beneath Klein Road as these two providers have no need to connect lines with each other. Thus, there are no anticipated sanitary sewer conflicts for the Project. Sanitary sewer locations were confirmed through correspondence with New Braunfels Utilities and Guadalupe-Blanco River Authority.

Additional coordination with local utility owners will be required to determine if any utility projects, including planned upgrades or new utility line construction, is planned within Phase 2 project limits.

3 TEMPORARY TRAFFIC CONTROL PLAN

Construction of Klein Road from S Walnut Ave to just north of Roadrunner Ave / Stoeger Dr and from just south of Dove Crossing Dr to FM 725 will be conducted with two-lane two-way traffic control. Removal of an existing low water crossing will be conducted with full roadway closure.

3.1 Two-Lane, Two-Way Traffic

Under a two-lane, two-way traffic control configuration the roadway will be constructed in halves, starting on the east side. The sequence of construction for this traffic control scheme includes:

1. Clear ROW
2. Relocate utilities to ultimate configuration
3. Temporary pavement widening to the west (approx. 15')
4. Install Low-profile concrete traffic barrier (LPCTB) using 10' lane widths measured from the western temporary pavement, divert traffic to the west side
5. Construct the eastern side of the roadway up to, but not including the final asphalt course
6. Shift traffic to the east, construct the western side of the roadway up to, but not including the final asphalt course

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7. Remove LPCTB, construct final asphalt course
8. Install permanent pavement markings, medians, illumination, and landscaping

The primary benefit of this traffic control alternative is that traffic remains open during construction. However, a key disadvantage is diminished ride quality, particularly on the temporary widening, which could generate negative feedback from the public. Additionally, placing and removing the temporary widening is considered a sunk cost, or expense incurred but not directly reflected in the ultimate improvements.

3.3 Road Closure at Guadalupe River Tributary 22 (Low Water Crossing)

Replacing the low water crossing will require a road closure between Roadrunner Ave and Dove Crossing Dr. The proposed structure will be constructed at a significantly higher elevation than the existing crossing, requiring material and equipment staging areas adjacent to the work area and thus making it infeasible to keep the road open to traffic during construction. A viable detour route was selected based on minimal additional distance and time delay added to local trips due to road closure while avoiding the use of local residential roads for through traffic. Specific analysis of the detour impacts relative to the following trip generators was conducted:

Emergency Services

The detour route will have minimal impacts on emergency service response times for fire, EMS, and police dispatched from nearest service stations because those stations are all located west of the project limits. The most efficient routes for dispatched emergency vehicles to the Project limits already utilize S Walnut Ave and FM 725 to access Klein Road, thus emergency response times are not anticipated to increase because of a closure at the Tributary 22. See **Figure 2** for the emergency service stations and proposed detour route. Although not preferred due to their local street classification, Dove Crossing Dr and Divine Way offer parallel route alternatives to FM 725 and W County Line Rd respectively and could be utilized by emergency services to access the Project limits if conditions warrant.

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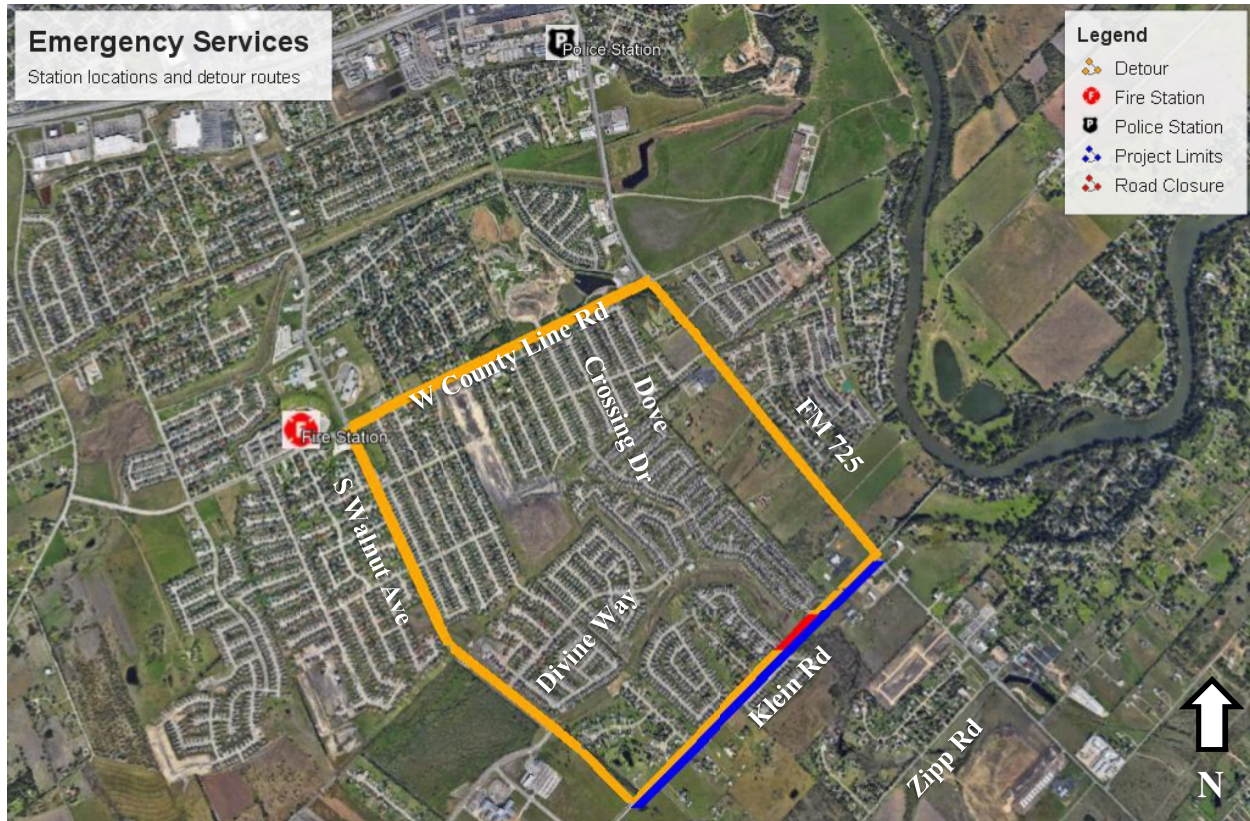


Figure 2: Emergency Service Stations and Phase 2 Detour Routes

Klein Road Elementary School

Pape-Dawson determined the detour route will cause some delay for trips to/from Klein Road Elementary School. A majority of the Klein Road Elementary School attendance zone is located south and east of the school. The most efficient existing route to the elementary school is to travel west on FM 725 and south on Klein Road until reaching the school. Traffic that currently accesses the school using Klein Road will need to be detoured as shown in **Figure 3**. The detour will add approximately 1.9 miles for most vehicles to reach the school, however, an alternative route utilizing local streets Dove Crossing Dr and Divine Way can reduce the added travel distance to approximately 0.5 miles, or minimal delay. While the local street alternative route is more direct than the detour route indicated in **Figure 3**, it would not be an ideal marked detour due to the increase in traffic on local streets.

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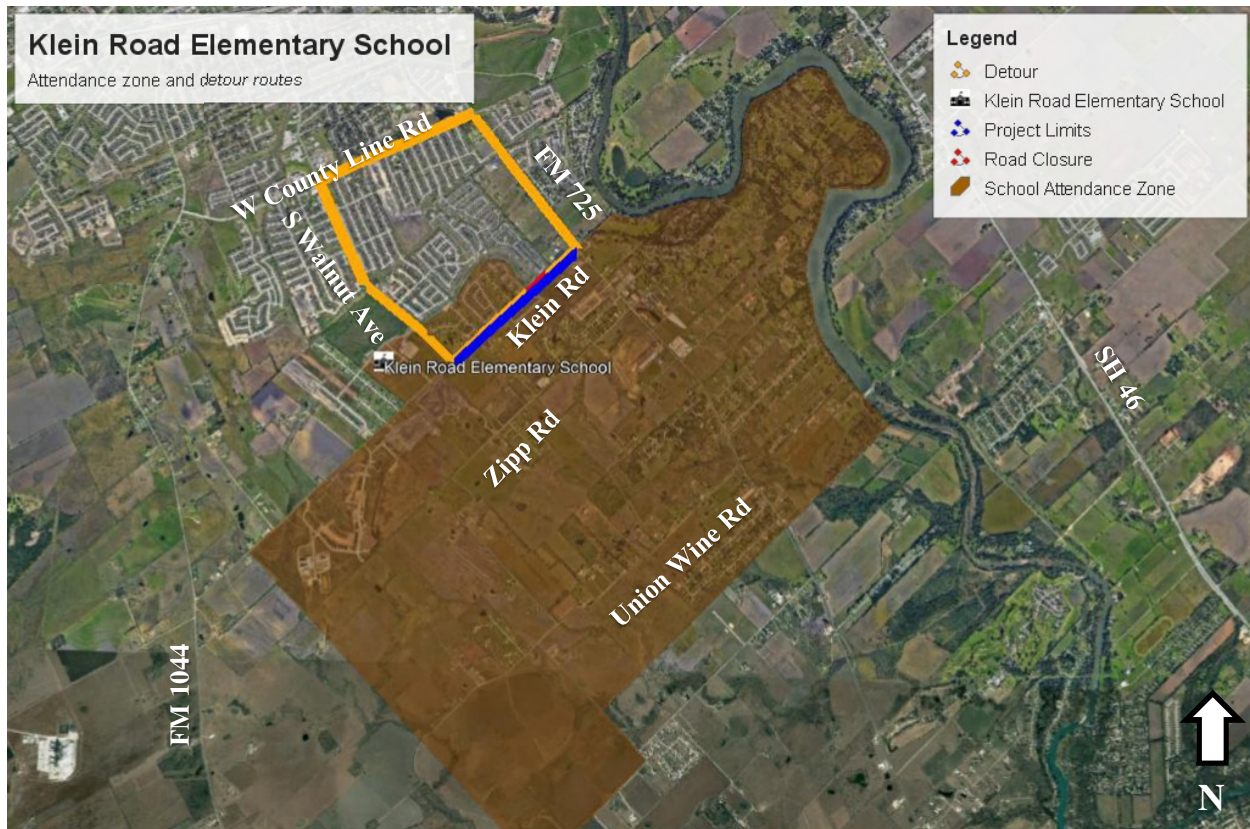


Figure 3: Klein Road Elementary School and Phase 2 Detour Routes

New Braunfels Middle School

Pape-Dawson determined the proposed detour routes will have similar delay for trips to/from New Braunfels Middle School. The New Braunfels Middle School attendance zone is located east and south of the school. The most efficient existing route to the middle school is to travel west on FM 725 and south on Klein Road until reaching the school. Traffic that currently accesses the school using Klein Road will need to be detoured as shown in **Figure 4**. Delay due to the detour is similar to that of trips to/from Klein Road Elementary School discussed in the previous section.

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Figure 4: New Braunfels Middle School and Phase 2 Detour Routes

Construction sequencing of the drainage improvements at Tributary 22 should begin at the end of school session to minimize the impact of delays on school-bound trips. Public information campaigns, portable changeable message signs, and highly visible detour signing will also assist in notifying the public to expect delays during the construction process. Additionally, other City departments should be notified of the closure internally for solid waste collection route modifications. Impacts to postal services are considered negligible as there is sufficient local road connectivity surrounding the closure.

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4 DRAINAGE

4.1 Existing Conditions

A low water crossing exists on Klein Road located between the Roadrunner Ave and Dove Crossing Dr intersections at Guadalupe Tributary 22 (see **Appendix B1**). Two preliminary alternative improvements for the low water crossing have been analyzed:

- Bridge-class multi-box culvert
- Span bridge with drilled shafts

Each alternative will remove the low water crossing to improve safety, emergency response capabilities during adverse and extreme weather, and commute delays. Both alternatives also meet the 2016 TxDOT Hydraulic Drainage Manual (HDM) requirements that the project “will not cause adverse impacts to adjacent properties” (HDM 5-8) and that raising the water surface elevation “will not cause any adverse impacts” (HDM 5-14) to adjacent properties.

The existing low water crossing is the drainage low point for the Project, meaning all runoff is conveyed to this tributary. Existing roadside ditches and driveway culverts exist on both sides of Klein Road providing runoff conveyance.

The project area soils from the Klein Road Phase 1 Geotechnical Engineering Study (see **Section 9 GEOTECHNICAL STUDY** for a more detailed discussion) were analyzed based on runoff potential, percentage of clay, and other various material properties described in Part 630 of the USDA National Engineering Handbook, Chapter 7. Phase 1 soils were determined to be Type D because the soil contains greater than 40% clay with a high shrink-swell potential. Soil characteristics, which influence the curve number utilized for the NRCS Hydrograph Method, are assumed to be consistent with Klein Road Phase 1 and will be confirmed with further geotechnical study during the PS&E phase.

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Hydrologic and hydraulic analysis for the existing and proposed drainage design is typically performed utilizing elevation and slope data provided by conventional survey. However, the drainage analysis conducted for the Project schematic design is based on LiDAR topography, as conventional survey was deferred until the PS&E phase. LiDAR topography is not detailed enough to design and construct safe, appropriately sized drainage improvements. However, the analysis conducted is satisfactory for the purpose of order-of-magnitude structure sizing and preliminary estimating. Detailed drainage design will be modified at the PS&E phase to address any inconsistencies between LiDAR and conventional survey topography and fine tune construction cost estimates.

4.2 Storm Sewer System

As stated in **Section 2.1 Existing Land Use and Right Of Way Acquisition**, ROW is a restrictive factor for Project elements. The proposed roadway, bicycle and pedestrian improvements will require all available existing ROW plus approximately 10' along the eastern ROW limit to be acquired from undeveloped parcels. Consequently, roadside ditches are not viable to convey runoff towards Guadalupe Tributary 22 due to their horizontal space requirements. A storm sewer system will be required to replace drainage conveyance provided by existing roadside ditches, as is common for urban corridors. Per the City of New Braunfels – 2016 Drainage and Erosion Control Design Manual 2018-1 (DECDM) 2018-1 Section 7.2, “storm drain systems shall be designed for the 25-year design storm and evaluated for the 100-year design storm.” The storm sewer will include two separate systems each draining toward Guadalupe Tributary 22, one from S Walnut Ave and the other from FM 725. The storm sewer system should not be located beneath proposed pavement, shared-use path, or sidewalk to prevent high future maintenance costs and road closures.

4.3 Hydrologic Analysis – Low Water Crossing

A hydrologic analysis was conducted to determine the peak discharges for the existing low water crossing. The contributing area was delineated for the low water crossing using ArcGIS (v.10.2.2) and LiDAR topography. Total contributing area was found to be 1.75 square miles with boundaries

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extending from the intersection of McCrae and Klein Road to the intersection of FM 725 and Klein Road (see **Appendix B2**).

Using HEC-HMS (v. 4.2) and the NRCS Hydrograph method, existing flows were calculated at the tributary crossing. Rainfall depth and intensities (**Table 2** and **Table 3**) were sourced from the DECDM. Per the DECDM, flow information was analyzed for ultimate development conditions. Information on the calculated flows are summarized in **Table 4**.

Table 2: New Braunfels Rainfall Intensity Constants

| <u>Year</u> | <u>Intensity Constants</u> | | |
|-------------|----------------------------|----------|----------|
| | b | d | e |
| 2 | 69.7 | 12.03 | 0.857 |
| 5 | 61.2 | 9.61 | 0.762 |
| 10 | 59.8 | 7.69 | 0.720 |
| 25 | 64.6 | 7.14 | 0.691 |
| 50 | 68.4 | 6.40 | 0.673 |
| 100 | 74.9 | 5.95 | 0.663 |

Table 3: New Braunfels Area Depth-Duration Values

| <u>Year</u> | <u>Area Depth-Duration (inches)</u> | | | | | | | | | |
|-------------|-------------------------------------|---------------|-------------|-------------|-------------|-------------|--------------|--------------|--------------|--------------|
| | 5-Min | 15-Min | 1-Hr | 2-Hr | 3-Hr | 6-Hr | 12-Hr | 24-Hr | 2-Day | 3-Day |
| 2 | 0.51 | 1.05 | 1.65 | 2.19 | 2.44 | 2.87 | 3.10 | 3.34 | 3.98 | 4.31 |
| 5 | 0.66 | 1.34 | 2.33 | 3.08 | 3.48 | 4.17 | 4.45 | 4.83 | 5.66 | 6.20 |
| 10 | 0.80 | 1.58 | 2.84 | 3.72 | 4.23 | 5.11 | 5.49 | 6.06 | 7.00 | 7.72 |
| 25 | 0.96 | 1.89 | 3.56 | 4.61 | 5.26 | 6.41 | 7.07 | 8.06 | 9.08 | 10.11 |
| 50 | 1.11 | 2.16 | 4.17 | 5.32 | 6.10 | 7.47 | 8.50 | 9.96 | 10.99 | 12.34 |
| 100 | 1.28 | 2.47 | 4.84 | 6.08 | 6.99 | 8.61 | 10.18 | 12.30 | 13.30 | 15.04 |

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Table 4: Guadalupe Tributary 22 Flows

| <u>Drainage</u> <u>Area ID</u> | <u>Area</u> <u>(Sq mi)</u> | <u>Method</u> | <u>Percent</u> <u>Impervious</u> | <u>NRCS</u> <u>CN</u> | <u>Lag Time</u> <u>(min)</u> | <u>AEP Storm</u> <u>Event Flows</u> <u>(CFS)</u> | |
|-----------------------------------|-------------------------------|---------------|-------------------------------------|--------------------------|---------------------------------|--|-----------|
| | | | | | | <u>2%</u> | <u>1%</u> |
| A | 1.75 | NRCS | 40.3% | 88 | 23.6 | 5,021 | 6,260 |

The existing tributary is identified as Tributary 22 on FEMA FIRM Panel 48187C0115F (see **Appendix B1**). The project location is designated as Zone A, representing the area subject to flooding by the 1% annual chance flood, and no base flood elevations have been determined.

4.4 Hydraulic Analysis – Overview of Low Water Crossing

A hydraulic analysis was conducted for the existing low water crossing and two proposed alternatives to assess the performance of each under existing and ultimate development conditions. HEC-RAS (v. 5.0.3) was used to create models and perform hydraulic calculations. Cross sections were taken upstream and downstream of the low water crossing (see **Appendix B3**).

According to Section 9.1 of the DECDM, the cross structure at the project location must meet the following requirements:

- 2% Annual Exceedance Probability (AEP) event runoff with headwater one foot below the top of the structure
- 1% AEP event water surface shall not encroach through half of roadway lanes

All results from the hydraulic analysis can be found in **Appendix B4**.

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4.5 Hydraulic Analysis – Existing Low Water Crossing

The existing low water crossing (see **Figure 5**) consists of three 24-inch corrugated metal pipes (CMPs) with the roadway functioning as a weir. Pipe sizes were field verified on 7/10/2018.

The existing culverts are undersized as their capacity is less than the discharge reaching the crossing. Hydraulic analysis of the existing conditions showed the 2% AEP storm event overtops the low water crossing by 3.73' and showed the 1% AEP storm event overtops by 4.04'. Storm runoff overtopping the road renders Klein Road impassable to traffic, creates unsafe driving conditions, and degrades the existing roadway structure. There are no active measures (such as lockable traffic gates) prohibiting vehicles from attempting to cross the tributary during roadway inundation, which can lead to dangerous (including fatal) outcomes.



Figure 5: Klein Road Existing Low Water Crossing

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4.6 Hydraulic Analysis - Proposed Bridge-Class Multi-Box Culvert

A bridge-class multi-box culvert is the first proposed design alternative to replace the low water crossing. Box culverts were analyzed to determine the sizes needed to provide enough capacity for flows reaching the crossing. Pape-Dawson determined sixteen 12'x9' box culverts are needed to prevent overtopping during the 1% AEP event and provide required freeboard during the 2% AEP event, as described in **Section 4.3 Hydrologic Analysis – Low Water Crossing**. The calculated existing and proposed 2% AEP water surface elevations (WSELs) are shown in **Table 5**.

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Table 5: Klein Road – 2% AEP WSEL Culvert Analysis

| <u>River</u> | <u>Existing 2% AEP WSEL</u> | <u>Proposed 2% AEP WSEL</u> | <u>ΔWSEL (Prop-Exist)</u> |
|-----------------------|------------------------------------|------------------------------------|----------------------------------|
| <u>Station</u> | <u>(ft)</u> | <u>(ft)</u> | <u>(ft)</u> |
| 5301 | 631.27 | 631.27 | 0.00 |
| 4940 | 630.09 | 630.09 | 0.00 |
| 4745 | 629.62 | 629.62 | 0.00 |
| 4533 | 629.15 | 629.16 | 0.01 |
| 4333 | 628.14 | 628.16 | 0.02 |
| 4125 | 627.50 | 627.53 | 0.03 |
| 3928 | 627.03 | 627.08 | 0.05 |
| 3720 | 626.63 | 626.72 | 0.09 |
| 3533 | 626.38 | 626.50 | 0.12 |
| 3329 | 625.99 | 624.62 | -1.37 |
| 3296 | Crossing | | |
| 3251 | 624.15 | 624.38 | 0.23 |
| 3050 | 623.61 | 623.61 | 0.00 |
| 2842 | 622.21 | 622.21 | 0.00 |
| 2637 | 621.41 | 621.41 | 0.00 |
| 2425 | 620.61 | 620.61 | 0.00 |
| 2217 | 619.99 | 619.99 | 0.00 |

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The calculated existing and proposed 1% AEP WSELs are shown in **Table 6**.

Table 6: Klein Road – 1% AEP WSEL Culvert Analysis

| <u>River</u> | <u>Existing 1% AEP WSEL</u> | <u>Proposed 1% AEP WSEL</u> | <u>ΔWSEL (Prop-Exist)</u> |
|----------------|-----------------------------|-----------------------------|---------------------------|
| <u>Station</u> | <u>(ft)</u> | <u>(ft)</u> | <u>(ft)</u> |
| 5301 | 631.75 | 631.75 | 0.00 |
| 4940 | 630.55 | 630.55 | 0.00 |
| 4745 | 630.10 | 630.11 | 0.01 |
| 4533 | 629.68 | 629.69 | 0.01 |
| 4333 | 628.58 | 628.61 | 0.03 |
| 4125 | 627.92 | 627.99 | 0.07 |
| 3928 | 627.43 | 627.55 | 0.12 |
| 3720 | 627.00 | 627.18 | 0.18 |
| 3533 | 626.75 | 627.00 | 0.25 |
| 3329 | 626.30 | 625.37 | -0.93 |
| 3296 | Crossing | | |
| 3251 | 624.49 | 624.79 | 0.30 |
| 3050 | 623.95 | 623.95 | 0.00 |
| 2842 | 622.51 | 622.51 | 0.00 |
| 2637 | 621.71 | 621.71 | 0.00 |
| 2425 | 620.95 | 620.95 | 0.00 |
| 2217 | 620.34 | 620.34 | 0.00 |

In both 1% and 2% AEP events, proposed WSELs are greater than existing WSELs directly upstream and downstream of the crossing. This increase is not a concern at time of study as it does not impact any structures or private property downstream. Topography obtained by conventional survey will examine the changes to calculates WSELs at the 1% and 2% AEP events to confirm this model result. If zero rise in calculated WSELs is required, regardless of impact to structures

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or private property, channel grading may alleviate these local increases in WSELs. Review of the environmental assessment, to be completed in the PS&E phase, will be required to ensure channel grading avoids impacts to jurisdictional waters, endangered species, and other sensitive environmental features.

Due to the proposed increase in culvert size, Klein Road is proposed to be elevated approximately 10' to implement the bridge class multi-box culvert alternative – a significant change to the roadway profile anticipated between the intersection with Roadrunner Ave/Stoeger Dr to the south and the intersection with Dove Crossing Dr to the north. Roadway profile changes will require storm sewer improvements to ensure runoff from the roadway reaches Tributary 22.

The box culverts will be precast and future maintenance will be required to prevent cracking and degradation of the boxes and wingwalls due to the high number of boxes needed.

4.7 Hydraulic Analysis - Proposed Span Bridge with Drilled Shafts

A span bridge with drilled shafts is the second design alternative analyzed to replace the low water crossing. The bridge would span 315' and include 30" diameter piers spaced 50' apart. Hydraulic analysis confirmed this alternative would prevent overtopping during the 1% AEP event and provide required freeboard during the 2% AEP event, as described in **Section 4.3 Hydrologic Analysis – Low Water Crossing**. The calculated existing and proposed 2% AEP WSELs are shown in **Table 7**.

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Table 7: Klein Road – 2% AEP WSEL Bridge Analysis

| <u>River Station</u> | <u>Existing 2% AEP WSEL (ft)</u> | <u>Proposed 2% AEP WSEL (ft)</u> | <u>ΔWSEL (Prop-Exist) (ft)</u> |
|----------------------|----------------------------------|----------------------------------|--------------------------------|
| 5301 | 631.27 | 631.27 | 0.00 |
| 4940 | 630.09 | 630.09 | 0.00 |
| 4745 | 629.62 | 629.62 | 0.00 |
| 4533 | 629.15 | 629.15 | 0.00 |
| 4333 | 628.14 | 628.14 | 0.00 |
| 4125 | 627.50 | 627.47 | -0.03 |
| 3928 | 627.03 | 626.98 | -0.05 |
| 3720 | 626.63 | 626.55 | -0.08 |
| 3533 | 626.38 | 626.27 | -0.11 |
| 3329 | 625.99 | 625.60 | -0.39 |
| 3296 | Crossing | | |
| 3251 | 624.15 | 624.19 | 0.04 |
| 3050 | 623.61 | 623.61 | 0.00 |
| 2842 | 622.21 | 622.21 | 0.00 |
| 2637 | 621.41 | 621.41 | 0.00 |
| 2425 | 620.61 | 620.61 | 0.00 |
| 2217 | 619.99 | 619.99 | 0.00 |

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The calculated existing and proposed 1% AEP WSELs are shown in **Table 8**.

Table 8: Klein Road – 1% AEP WSEL Bridge Analysis

| <u>River</u> <u>Station</u> | <u>Existing 1% AEP WSEL</u> <u>(ft)</u> | <u>Proposed 1% AEP WSEL</u> <u>(ft)</u> | <u>ΔWSEL (Prop-Exist)</u> <u>(ft)</u> |
|--------------------------------|--|--|--|
| 5301 | 631.75 | 631.75 | 0.00 |
| 4940 | 630.55 | 630.55 | 0.00 |
| 4745 | 630.10 | 630.10 | 0.00 |
| 4533 | 629.68 | 629.68 | 0.00 |
| 4333 | 628.58 | 628.58 | 0.00 |
| 4125 | 627.92 | 627.92 | 0.00 |
| 3928 | 627.43 | 627.43 | 0.00 |
| 3720 | 627.00 | 626.99 | -0.01 |
| 3533 | 626.75 | 626.74 | -0.01 |
| 3329 | 626.30 | 626.23 | -0.07 |
| 3296 | Crossing | | |
| 3251 | 624.49 | 624.53 | 0.04 |
| 3050 | 623.95 | 623.95 | 0.00 |
| 2842 | 622.51 | 622.51 | 0.00 |
| 2637 | 621.71 | 621.71 | 0.00 |
| 2425 | 620.95 | 620.95 | 0.00 |
| 2217 | 620.34 | 620.34 | 0.00 |

A marginal decrease in WSEL is observed directly upstream of the crossing and a marginal increase in WSEL is seen directly downstream of the crossing. The increase in WSEL downstream does not result in any adverse impacts to surrounding structures. The minimal change in WSEL downstream indicates channel grading should not be needed for this alternative. Correction of

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topography assumed in the model using conventional survey data will confirm this conclusion at PS&E phase.

4.8 Drainage Criteria

As previously stated, analysis regarding the proposed alternative designs for the low water crossing use criteria set by the DCEDM. The DCEDM provides more restrictive drainage criteria than the TxDOT HDM. For example, the DCEDM uses the 2% AEP event as the basis for design with a strict requirement for the 1% AEP event: the “100-year water surface shall not encroach through half of roadway lanes”. For the multi-box culvert design, these requirements caused the need for an approximate 10’ rise in roadway profile elevation and the necessity for sixteen proposed boxes to achieve drainage capacity. In the case of the bridge design, these requirements led to the 315’ long proposed span length.

In contrast, the HDM uses the 4% AEP event as the basis for design with the 1% AEP event used as a check for arterial roadways. The less-restrictive criteria mandated by the TxDOT HDM allows for multiple design benefits. While the roadway will still require an elevation increase to meet HDM requirements, this elevation increase would be smaller than that needed using DCEDM criteria. Also, the proposed number of culvert boxes or proposed bridge span would be decreased because capacity requirements would be less restrictive under the HDM. The City should consider using alternative criteria such as the HDM rather than the DCEDM if cost or constructability become a concern for the project.

4.9 Flooding at S Walnut Ave and Settlers Crossing

During a Klein Road Phase 1 public meeting, comments were received regarding increased instances of flooding occurring in the Ranch Estates community along Bonnies Way (approximately 0.3 miles northwest of the intersection of Klein Road and S Walnut Ave). Though this flooding occurs outside the project limits, Pape-Dawson conducted hydraulic analysis for S Walnut Ave and Klein Road to determine if Phase 2 drainage improvements could alleviate offsite flooding.

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An existing drainage cross culvert, consisting of two corrugated metal arch pipes, exists just north of the intersection of Klein Road and S Walnut Ave. The cross culvert conveys drainage from the east heading northwest through a ditch parallel to S Walnut Ave, then turns through a private homestead and the Ranch Estates community until reaching an existing concrete-lined drainage channel, Tributary 22 (see **Figure 6**).



Figure 6: Flooding Location Map

Resizing or replacing the cross culvert at Klein Road and S Walnut Ave will not resolve the flooding issue noted at Bonnies Way – any increased capacity at the Klein Road cross culvert could allow drainage to reach Tributary 22 more quickly via the existing drainage path through the Ranch Estates community; decreased capacity will restrict drainage conveyance and possibly shift the flooding

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upstream of Klein Road. Drainage must be conveyed to Tributary 22 by a different route so that the overall drainage conveyed through Bonnies Way is reduced. Pape-Dawson considered two potential solutions to address flooding at Bonnies Way by conveying drainage along Klein Road north to Tributary 22:

- Utilize roadside ditches and driveway culverts
- Utilize a storm sewer system

Both alternatives divert water north through the Project to reach Tributary 22 at a different location than utilized today. This would alleviate flooding at Bonnies Way, conveying drainage further downstream along Tributary 22, but possibly create a similar flooding issue at the low water crossing. The new design to replace the existing low water crossing, whether bridge class multi-box culverts or a span bridge on drilled shafts, must account for the additional drainage to ensure no flooding will occur.

Roadside ditches and driveway culverts

The first proposed alternative is to convey drainage north using roadside ditches and driveway culverts along the east side of Klein Road until reaching Tributary 22 near the existing low water crossing. Hydraulic analysis was conducted to determine the required driveway culvert sizes to handle the 4% AEP event flow (as mandated by the DECDM). Using existing slopes, Pape-Dawson determined that driveway box culverts ranging in size from a 5'x4' box to a 6'x5' box would be required. Drainage velocities through the 5'x4' box culverts, however, would be greater than 12 fps. Per the TxDOT Hydraulic Manual, velocities should be maintained between 3 fps to 12 fps. To reduce velocities to acceptable levels, adjustments can be made to the slope of these culverts.

Roadside ditches were also hydraulically analyzed for this alternative. To provide enough capacity for the 4% AEP event, a ditch with minimum 3:1 side slopes and bottom width of 6' is required. Drainage would be conveyed at a depth of 3.4' and would require a slope of 0.008 ft/ft to provide a shear stress below 1 lb/sf. If shear stress rises above this level, due to an increased drainage velocity from using a

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differing ditch section than that described above, soil retention blankets, riprap, or gabion mattresses will be needed to prevent erosion of the ditch.

Under this alternative, drainage would be conveyed at a higher velocity than drainage under existing conditions. This increase in velocity is anticipated to result in a rise in WSEL directly downstream of the existing low water crossing location. To prevent this rise in WSEL, drainage detention would need to be considered in the design, such as a detention pond. This alternative is not feasible for multiple reasons. Klein Road lacks the ROW to fit the proposed roadside ditches (as described in **Section 4.2 Storm Sewer System**) and to fit a proposed detention pond. ROW acquisition for the detention pond would not be feasible due to the adjacent residential developments (as described in **Section 2.1 Existing Land Use and Right Of Way Acquisition**). In addition, the driveway culvert sizes are too large to maintain the same flowline as the 3.4' deep roadside ditches.

Storm sewer improvements

The second proposed alternative is to convey drainage north using a proposed underground storm sewer system parallel to Klein Road until reaching Tributary 22 near the existing low water crossing. Pape-Dawson conducted hydraulic analysis for this alternative and concluded that the proposed storm sewer is anticipated to be an 8'x4' size box culvert. This box culvert could also serve as the trunkline for the proposed storm sewer system already envisioned for the Project (see **Section 4.2 Storm Sewer System**). The benefit of using a storm drain system rather than a ditch is that a storm drain's trunkline size and slope can be modified to reduce drainage velocities, whereas a ditch slope cannot be heavily modified and increasing the size uses more of the available ROW. Adjusting the slope of the storm sewer system allows the velocity to be better controlled, and in-line detention measures are available, meaning a substantial rise in the WSEL downstream of the low water crossing is not anticipated.

Pape-Dawson concluded this alternative is feasible but would involve a large cost due to the size of pipe and the amount of soil excavation needed. It would, however, reduce flooding reported at Bonnies Way.

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5 TRAFFIC OPERATIONS

The schematic developed for the Project limits under Klein Road Phase 1 proposed a three-lane typical section including 40' of pavement for 2~14' lanes, a 12' center two-way left-turn lane, a 6' sidewalk to the west and a 10' shared use path to the east. One important observation is that the typical section prepared during Phase 1 does not meet the Minor Arterial requirements for 48' of pavement, or 4 travel lanes, and violates the AASHTO PDOBF for separation of side paths from the back of curb. The Project schematic will be an update to the Phase 1 schematic based on AASHTO and PROWAG criteria, new traffic counts, projections, and alternatives not previously examined.

5.1 Existing Conditions

Klein Road is a primary access roadway to the Dove Crossing, White Wing, Whispering Valley, and Ranch Estates residential communities. Klein Road is referred to as a north-south roadway in this analysis. The posted speed limit on Klein Road is 30 miles per hour.

Turning Movement Counts (TMC) were collected along the Project limits at the intersections of Klein Road at Walnut Ave, Klein Road at Roadrunner Ave/Stoeger Dr, Klein Road at Dove Crossing Dr, and Klein Road at FM 725 from 7:00 AM to 9:00 AM, 11:00 AM to 1:00 PM, and 4:00 PM to 6:00 PM on Tuesday, May 22nd, 2018 (see **Appendices C1 and C2**). The existing intersection geometries are shown in **Table 9**.

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Table 9: Intersection Geometry - Existing Conditions (2018)

| <u>Intersection</u> | <u>Approach</u> | <u>Lane Designation*</u> | <u>Traffic Control</u> |
|--|----------------------|-------------------------------|--------------------------------|
| Klein at Walnut | NB SB EB | L-T TR L-R | One-Way Stop-Controlled |
| Klein at Roadrunner/Stoeger | NB SB EB WB | LTR LTR LTR | Two-Way Stop-Controlled (TWSC) |
| Klein at Dove Crossing | NB SB EB | LT TR L-R | One-Way Stop-Controlled |
| Klein at FM 725 | NB SB EB WB | L-TR L-TR L-T-R L-TR | Traffic Signal |
| *L = Left-turn lane; T = Through lane; R = Right-turn lane; LT = Shared Left/Thru lane; TR = Shared Thru/Right lane; LTR = Shared Left/Through/Right-turn lane; U = Turn around Lane | | | |

The TMC data confirms that AM, Midday, and PM peak hours on the corridor are 7:15 AM – 8:15 AM, 12:00 PM to 1:00 PM, and 5:00 PM to 6:00 PM, respectively. An existing conditions model was developed using Synchro traffic analysis software Version 9.2. Existing Measures of Effectiveness for each peak hour, including level of service (LOS), delays, and queueing along the project limits, are reported in **Appendix C3**. A summary of the levels of service and delays is shown in **Table 10** and **Table 11**.

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Table 10: Signalized Intersection Capacity - Existing Conditions (2018)

| Intersection | Condition | <u>AM Peak Hour</u> | | <u>MID Peak Hour</u> | | <u>PM Peak Hour</u> | |
|-----------------|-----------|---------------------|-------------------------|----------------------|-------------------------|---------------------|-------------------------|
| | | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) |
| Klein at FM 725 | Existing | C | 24.2 | B | 11.4 | C | 20.5 |

Table 11: Unsignalized Intersection Capacity - Existing Conditions (2018)

| <u>Intersection</u> | | | <u>AM Peak Hour</u> | | <u>MID Peak Hour</u> | | <u>PM Peak Hour</u> | |
|------------------------------------|----------|------|---------------------|--------------------------|----------------------|--------------------------|---------------------|--------------------------|
| Condition | Approach | Mvmt | LOS | Approach Delay (sec/veh) | LOS | Approach Delay (sec/veh) | LOS | Approach Delay (sec/veh) |
| Klein at Walnut | | | | | | | | |
| Existing | NB | LT | A | 3.9 | A | 2.6 | A | 2.5 |
| Existing | SB | TR | A | 0.0 | A | 0.0 | A | 0.0 |
| Existing | EB | LR | C | 23.4 | B | 10.2 | B | 14.1 |
| Klein at Roadrunner/Stoeger | | | | | | | | |
| Existing | NB | LTR | A | 0.3 | A | 0.4 | A | 0.6 |
| Existing | SB | LTR | A | 0.6 | A | 0.7 | A | 0.7 |
| Existing | EB | LTR | C | 22.1 | B | 11.3 | B | 13.5 |
| Existing | WB | LTR | B | 13.5 | A | 9.8 | B | 12.4 |
| Klein at Dove Crossing | | | | | | | | |
| Existing | NB | LT | A | 1.1 | A | 0.6 | A | 0.7 |
| Existing | SB | TR | A | 0.0 | A | 0.0 | A | 0.0 |
| Existing | EB | LR | C | 15.5 | B | 10.9 | B | 13.1 |

The results in **Table 10** and **Table 11** confirm that all intersections operate at LOS C or better, therefore, no traffic improvements are required at this time.

5.2 Traffic Projections

The following is a summary of the data used for traffic analysis and how it was applied to assume growth rates and projected turning movement counts for the Project corridor.

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- Design Years: Base Year is 2018 and Forecasted Year is 2040
- Historic Counts: these relevant historic counts were obtained from the Traffic Count Database System (TCDS)
 - o Four annual Accumulative Count Recorder (ACR) traffic stations, which provide 24-hour axle counts across an entire roadway section, were available outside the project limits:
 - 95H113 – FM 725, just west of Klein Road
 - 95H114 – FM 725, 1.5 miles east of Klein Road
 - 95H112 – FM 1044, 1.5 miles east of Klein Road
 - 46D5 – FM 1044, 2 miles east of Klein Road

These counts all occur in areas of similar development and should reflect the growth on Klein Road.
- Future Projection: Forecasted Year counts were obtained from the San Antonio Bexar County Metropolitan Planning Organization (SABCMPO) 2040 Travel Demand Model. Projections were taken from the locations of the four annual ACR count stations previously listed.
- Growth Rate and Factors: **Table 12** shows the exponential growth rates derived from the SABCMPO 2040 Travel Demand Model projected counts at the pertinent TCDS count locations.

Table 12: Historic Count Growth Rates

| <u>Historic Count</u> | <u>Exponential Growth Rate (%)</u> |
|-----------------------|------------------------------------|
| 95H113 | 4 |
| 95H114 | 5 |
| 95H112 | 5 |
| 46D5 | 6 |

- After reviewing SABCMPO’s 2040 Travel Demand Model assignments and historic growth, an average annual growth rate of 5% was selected for Klein Road. Both the east and west legs on the FM 725 intersection, Stoeger Dr, and Walnut Ave also used a 5% growth rate to reflect

Klein Road Phase 2 Summary of Needs Study

the possibility for adjacent development. Roadrunner Ave and Dove Crossing Dr used a 2% growth rate to reflect the areas already mostly developed. The diagram in **Appendix C4** summarizes the annual growth percentages and the total growth rate factors applied throughout the corridor.

- A single family residential development is currently in the design phase south of the Klein Road at Benelli Dr intersection. A TIA was proposed for this development in 2017. The trips generated from this development were distributed throughout the network and added to the ADT for the forecast year of 2040. In total, the proposed development generates 1038 trips per day (190 peak hour trips) and will obtain access to Klein Road via Benelli Dr.

5.3 Future (No Build) Traffic Model

A future conditions model using the current roadway geometry was developed using existing turning movement counts with the applied growth rate factors and trip generation from future development. Measures of Effectiveness for each peak hour including LOS, delays, and queueing along the project limits are reported in **Appendix C5**. A summary of the levels of service and delays is shown in **Table 13** and **Table 14**.

Table 13: Signalized Intersection Capacity - Future (No Build) Conditions (2040)

| Intersection | Condition | <u>AM Peak Hour</u> | | <u>MID Peak Hour</u> | | <u>PM Peak Hour</u> | |
|-----------------|-----------------|---------------------|-------------------------|----------------------|-------------------------|---------------------|-------------------------|
| | | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) |
| Klein at FM 725 | Fut. (No Build) | F | 476.9 | F | 224.6 | F | 590.1 |

The results in **Table 13** confirm that the intersection of Klein at FM 725 will operate at LOS F under existing conditions by 2040.

Klein Road Phase 2 Summary of Needs Study

Table 14: Unsignalized Intersection Capacity - Future (No Build) Conditions (2040)

| <u>Intersection</u> | | <u>AM Peak Hour</u> | | | <u>MID Peak Hour</u> | | <u>PM Peak Hour</u> | |
|------------------------------------|----------|---------------------|----------|--------------------------------|----------------------|--------------------------------|---------------------|--------------------------------|
| Condition | Approach | Mvmt | LOS | Approach Delay (sec/veh) | LOS | Approach Delay (sec/veh) | LOS | Approach Delay (sec/veh) |
| Klein at Walnut | | | | | | | | |
| Fut. (No Build) | NB | LT | F | 196.2 | A | 3.0 | A | 3.7 |
| Fut. (No Build) | SB | TR | A | 0.0 | A | 0.0 | A | 0.0 |
| Fut. (No Build) | EB | LR | F | ERR | D | 28.0 | F | 4466.4 |
| Klein at Roadrunner/Stoeger | | | | | | | | |
| Fut. (No Build) | NB | LTR | A | 1.7 | A | 0.3 | A | 1.2 |
| Fut. (No Build) | SB | LTR | A | 5.0 | A | 1.1 | A | 3.6 |
| Fut. (No Build) | EB | LTR | F | ERR | D | 27.0 | F | 359.6 |
| Fut. (No Build) | WB | LTR | F | ERR | C | 15.6 | F | 50.8 |
| Klein at Dove Crossing | | | | | | | | |
| Fut. (No Build) | NB | LT | A | 4.7 | A | 0.5 | A | 1.3 |
| Fut. (No Build) | SB | TR | A | 0.0 | A | 0.0 | A | 0.0 |
| Fut. (No Build) | EB | LR | F | ERR | C | 22.4 | F | 120.8 |

The results in **Table 14** confirm that the intersection of Klein Road at S Walnut Ave, Klein Road at Roadrunner Ave/Stoeger Dr, and Klein Road at Dove Crossing Dr will operate at LOS F under existing conditions by 2040. The values displayed as “ERR” indicate approach delays so high, they could not be analyzed.

5.4 Future (Proposed) Traffic Model

A future conditions model was developed using a proposed roadway geometric configuration, existing turning movement counts, applied growth rate factors, and trip generation from future development. The proposed roadway geometry was developed to mitigate the operational issues at the intersections identified in **Table 14**. A four-lane section (two 12-foot lanes each direction) with a 12-foot median for left turn channels and changes to intersection geometry is required to provide acceptable LOS in 2040. Incorporating the same bicycle and pedestrian facilities considered in the schematic developed under Phase 1, with appropriate parkways and buffers as

Klein Road Phase 2 Summary of Needs Study

established in the AASHTO PDOBF, the proposed typical section would require a 90' ROW for the entire Project limits. The proposed changes to intersection geometry are shown in **Table 15**.

Table 15: Intersection Geometry - Future (Proposed) Conditions (2040)

| <u>Intersection</u> | <u>Approach</u> | <u>Lane Designation*</u> | <u>Traffic Control</u> |
|--|----------------------|---|--------------------------------|
| Klein at Walnut | NB SB EB | L-T-T T-T-R L-LR-R | Traffic Signal |
| Klein at Roadrunner/Stoeger | NB SB EB WB | L-T-TR L-T-TR LTR LTR | Two-Way Stop-Controlled (TWSC) |
| Klein at Dove Crossing | NB SB EB | L-T-T T-TR L-R | One-Way Stop-Controlled |
| Klein at FM 725 | NB SB EB WB | L-L-TR-R L-TR L-T-T-T-R L-L-T-T-TR | Traffic Signal |
| *L = Left-turn lane; T = Through lane; R = Right-turn lane; LT = Shared Left/Thru lane; TR = Shared Thru/Right lane; LTR = Shared Left/Through/Right-turn lane; U = Turn around Lane | | | |

Measures of Effectiveness for each peak hour including LOS, delays, and queueing along the project limits are reported in **Appendix C6**. A summary of the levels of service and delays is shown in **Table 16** and **Table 17**.

Klein Road Phase 2 Summary of Needs Study

Table 16: Signalized Intersection Capacity - Future (Proposed) Conditions (2040)

| Intersection | Condition | <u>AM Peak Hour</u> | | <u>MID Peak Hour</u> | | <u>PM Peak Hour</u> | |
|-----------------|-------------------|---------------------|-------------------------|----------------------|-------------------------|---------------------|-------------------------|
| | | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) |
| Klein at Walnut | Future (Proposed) | C | 34.2 | B | 12.7 | B | 16.7 |
| Klein at FM 725 | Future (Proposed) | D | 36.4 | B | 15.8 | D | 45.1 |

Table 17: Unsignalized Intersection Capacity - Future (Proposed) Conditions (2040)

| <u>Intersection</u> | | | <u>AM Peak Hour</u> | | <u>MID Peak Hour</u> | | <u>PM Peak Hour</u> | |
|------------------------------------|----------|----------|---------------------|--------------------------|----------------------|--------------------------|---------------------|--------------------------|
| Condition | Approach | Movement | LOS | Approach Delay (sec/veh) | LOS | Approach Delay (sec/veh) | LOS | Approach Delay (sec/veh) |
| Klein at Roadrunner/Stoeger | | | | | | | | |
| Future (Proposed) | NB | LTR | A | 0.2 | A | 0.2 | A | 0.4 |
| Future (Proposed) | SB | LTR | A | 0.6 | A | 0.8 | A | 0.6 |
| Future (Proposed) | EB | LTR | F | 91.1 | B | 13.6 | C | 23.5 |
| Future (Proposed) | WB | LTR | D | 33.5 | B | 11.4 | C | 16.3 |
| Klein at Dove Crossing | | | | | | | | |
| Future (Proposed) | NB | LT | A | 0.6 | A | 0.3 | A | 0.4 |
| Future (Proposed) | SB | TR | A | 0.0 | A | 0.0 | A | 0.0 |
| Future (Proposed) | EB | LR | C | 22.4 | B | 12.5 | C | 20.7 |

While the intersection of Klein Road at Roadrunner Ave/Stoeger Dr still operates at LOS F at the design year, volumes are not anticipated to warrant a traffic signal. An alternative design option was analyzed for this intersection that included a Flying-T configuration for Roadrunner Ave (thus forcing right-in, right-out movements at Stoeger Dr). However, the system performance was not improved. The proposed geometry minimizes delay at this intersection, maintains volume to capacity ratio < 1 (ie, demand less than capacity), and is therefore still considered viable.

Klein Road Phase 2 Summary of Needs Study

5.5 Alternative Design Options

Due to ROW restrictions (discussed in **Section 2.1 Existing Land Use and Right Of Way Acquisition**) a four-lane section is not attainable throughout the corridor due to existing development restricting feasible ROW acquisition to 70'. If a two-lane section (one 12-foot lane each direction) with a 12-foot median for left turn channels is the only attainable roadway geometry, then the following alternative design configurations should be considered to re-route turns and improve traffic operations:

Alternative 1: Constructing U-turns near the northern and southern project limits would allow for the restriction of left turns from Roadrunner Ave/Stoeger Dr, Dove Crossing Dr, and other stop-controlled intersections, minimizing delay and queue lengths from these minor roads. These trips would be re-routed through the U-turns to return to their desired path with minimal delay. A summary of the levels of service and delays is shown in **Table 18** and **Table 19**.

Table 18: Signalized Intersection Capacity - Future (Alternative 1) Conditions (2040)

| Intersection | Condition | <u>AM Peak Hour</u> | | <u>MID Peak Hour</u> | | <u>PM Peak Hour</u> | |
|-----------------|----------------|---------------------|-------------------------|----------------------|-------------------------|---------------------|-------------------------|
| | | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) |
| Klein at Walnut | Future (Alt 1) | D | 39.7 | B | 14.0 | B | 19.0 |
| Klein at FM 725 | Future (Alt 1) | D | 37.9 | B | 15.8 | D | 45.1 |

Klein Road Phase 2 Summary of Needs Study

Table 19: Unsignalized Intersection Capacity - Future (Alternative 1) Conditions (2040)

| Intersection | Condition | Approach | Mvmt | <u>AM Peak Hour</u> | | <u>MID Peak Hour</u> | | <u>PM Peak Hour</u> | |
|---------------------------------|--------------|----------|------|---------------------|-------------------------|----------------------|-------------------------|---------------------|-------------------------|
| | | | | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) |
| Klein at Roadrunner/ Stoeger | Fut. (Alt 1) | NB | LTR | A | 0.4 | A | 0.2 | A | 0.8 |
| | Fut. (Alt 1) | SB | LTR | A | 1.6 | A | 0.9 | A | 1.5 |
| | Fut. (Alt 1) | EB | R | E | 45.4 | B | 11.0 | D | 27.1 |
| | Fut. (Alt 1) | WB | R | F | 178.6 | B | 13.5 | C | 15.6 |
| Klein at Dove Crossing | Fut. (Alt 1) | NB | LT | A | 1.0 | A | 0.3 | A | 0.9 |
| | Fut. (Alt 1) | SB | TR | A | 0.0 | A | 0.0 | A | 0.0 |
| | Fut. (Alt 1) | EB | R | E | 45.7 | B | 11.9 | E | 47.4 |

Alternative 2: Constructing a Flying-T intersection at Dove Crossing would provide more direct access to and from Klein Road. Left turns from Roadrunner/Stoeger would still be restricted to minimize queue lengths and delays, and therefore, U-turns near the northern and southern limits of the project would have to be constructed. A summary of the levels of service and delays is shown in **Table 20** and **Table 21**.

Table 20: Signalized Intersection Capacity - Future (Alternative 2) Conditions (2040)

| Intersection | Condition | <u>AM Peak Hour</u> | | <u>MID Peak Hour</u> | | <u>PM Peak Hour</u> | |
|-----------------|----------------|---------------------|-------------------------|----------------------|-------------------------|---------------------|-------------------------|
| | | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) |
| Klein at Walnut | Future (Alt 2) | D | 43.2 | B | 14.7 | B | 18.9 |
| Klein at FM 725 | Future (Alt 2) | D | 38.1 | B | 16.1 | D | 45.0 |

Klein Road Phase 2 Summary of Needs Study

Table 21: Unsignalized Intersection Capacity - Future (Alternative 2) Conditions (2040)

| Intersection | Condition | Approach | Mvmt | <u>AM Peak Hour</u> | | <u>MID Peak Hour</u> | | <u>PM Peak Hour</u> | |
|------------------------------|--------------|----------|------|---------------------|-------------------------|----------------------|-------------------------|---------------------|-------------------------|
| | | | | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) | LOS | Control Delay (sec/veh) |
| Klein at Roadrunner /Stoeger | Fut. (Alt 2) | NB | LTR | A | 0.4 | A | 0.2 | A | 0.7 |
| | Fut. (Alt 2) | SB | LTR | A | 1.3 | A | 1.0 | A | 1.4 |
| | Fut. (Alt 2) | EB | R | E | 35.5 | B | 10.7 | C | 23.4 |
| | Fut. (Alt 2) | WB | R | F | 105.7 | B | 12.6 | B | 14.5 |
| Klein at Dove Crossing | Fut. (Alt 2) | NB | LT | A | 2.5 | A | 0.9 | A | 2.5 |
| | Fut. (Alt 2) | SB | TR | A | 1.5 | A | 0.7 | A | 2.8 |
| | Fut. (Alt 2) | EB | R | D | 31.4 | A | 7.6 | F | 87.8 |

Examples of these alternatives are shown in **Appendix C7**. While these alternative methods may be considered in spaces of limited ROW, intersection geometries for the intersections of Klein Road at S Walnut Ave and Klein Road at FM 725 should adhere to the proposed geometries in **Table 15** to address the projected volumes on all approaches.

5.6 Traffic Conclusions

Traffic analysis included evaluations of existing and projected traffic conditions, as well as proposed changes to roadway geometry in response to anticipated future operational issues. Based on traffic projections, the three-lane section developed at Klein Road Phase 1 schematic phase (see **Appendix A5**) will be insufficient to support the projected traffic volumes. A four-lane section (two 12-foot lanes each direction) with a 12-foot median for left turn channels and changes to intersection geometry to provide acceptable LOS in 2040. If this recommended geometry is not attainable due to ROW restrictions, the alternatives provided must be considered to re-route turns and improve traffic operations to the maximum extent feasible.

Klein Road Phase 2 Summary of Needs Study

6 DEFERRED PROFESSIONAL SERVICES

The City deferred conventional survey, environmental assessment, and geotechnical study until PS&E phase pending project funding from the 2019 Proposed Bond Program. Deferring these services imposes some risk of proceeding with specific cost and schedule assumptions that could be adversely impacted if items related to these disciplines are found to be detrimental to the cost or schedule for the Project.

7 SURVEY

Sources of existing feature information supporting schematic design include aerial imagery, LiDAR topography, and field observations. Schematic design will be conducted in state plane grid coordinates as no conventional survey-grade input data was gathered to support the schematic. Design will be converted to surface coordinates at PS&E phase once survey data has been received.

8 ENVIRONMENTAL ASSESSMENT

The Project environmental assessment will identify sensitive environmental areas within project limits. If sensitive environmental areas are located within Phase 2 project limits, PS&E design must be modified to avoid or mitigate any conflicts with sensitive areas.

The 'Phase 1 Environmental Site Assessment' conducted by Raba Kistner in 2014 identified no sensitive environmental areas within Phase 1 project limits. Pape-Dawson identified two potential Phase 2 sensitive environmental areas from field observations:

- Potential wetland southeast of the low water crossing
- Possible soil contamination from underground petroleum storage tanks at the project's northern terminus

The full environmental assessment will fully vet these specific concerns and investigate additional environmental constraints.

Klein Road Phase 2 Summary of Needs Study

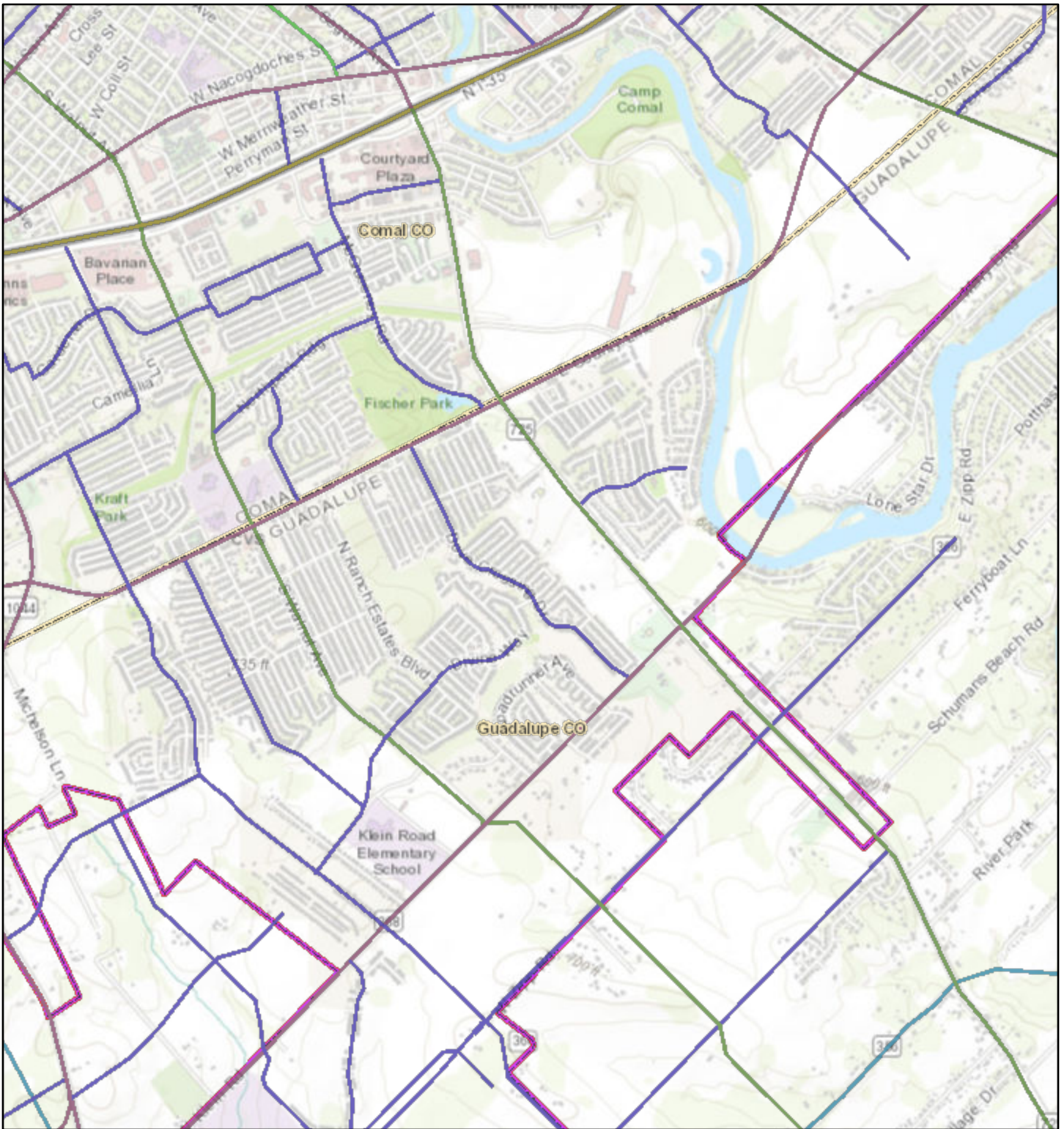
9 GEOTECHNICAL STUDY

The Project geotechnical study will determine soil conditions within project limits and propose pavement section alternatives, similar to the Phase 1 ‘Geotechnical Engineering Study’ conducted by Raba Kistner in 2014. The Phase 1 geotechnical study provides the basis for the Project geotechnical assumptions until more detailed study can be conducted during the PS&E phase.

One concern with the adopted pavement section is that lime treatment requires road closure for several days to allow the subgrade lime-soil mixture to cure. Additionally, the process of mixing the lime can be disruptive to nearby residences and through traffic due to fine dust. Alternatives to lime treatment will be considered at PS&E phase for potential improvements to the traffic control plan or reduction in disruption to nearby residences.

APPENDIX A1

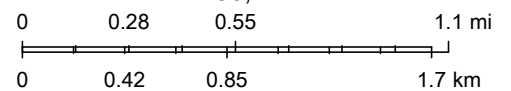
Klein Road Phase 2 Regional Transportation Plan Map



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1:36,112

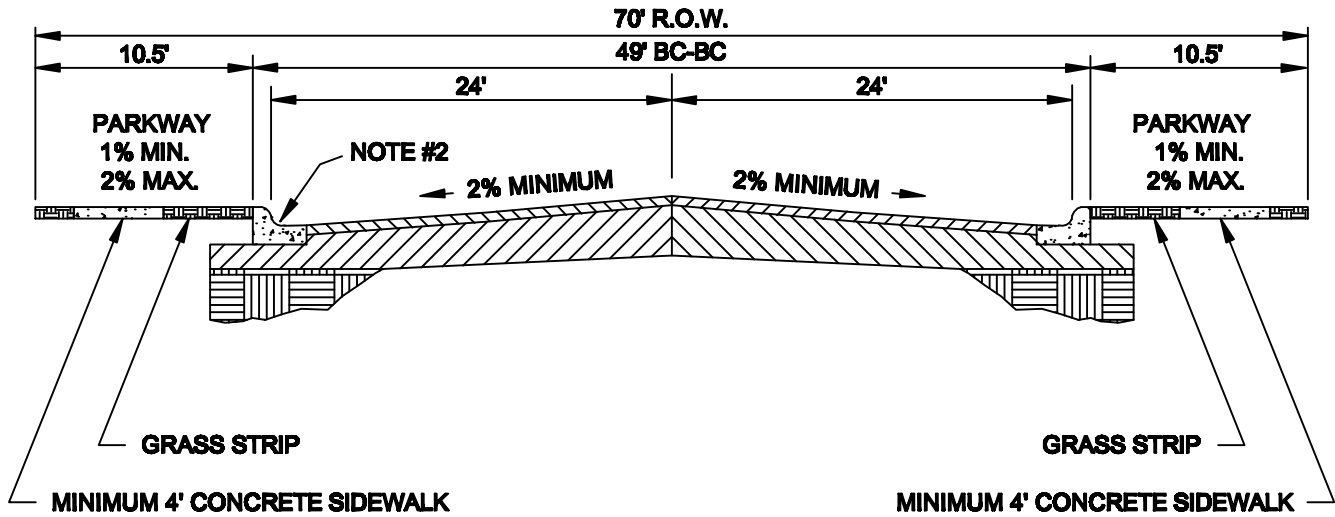
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|------------------------------|-----------------|-----------------------------|
| Regional Transportation Plan | Interstate | Principal Arterial |
| Couplet | Major Collector | ETJ |
| Enhanced Intersection | Minor Arterial | County Boundaries (Outline) |
| Expressway | Minor Collector | City Limits (Outline) |
| Future | Parkway | Addresses |



Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), swisstopo, © OpenStreetMap contributors, and the GIS User Community


APPENDIX A2

MINOR ARTERIAL FOUR LANES - NO PARKING



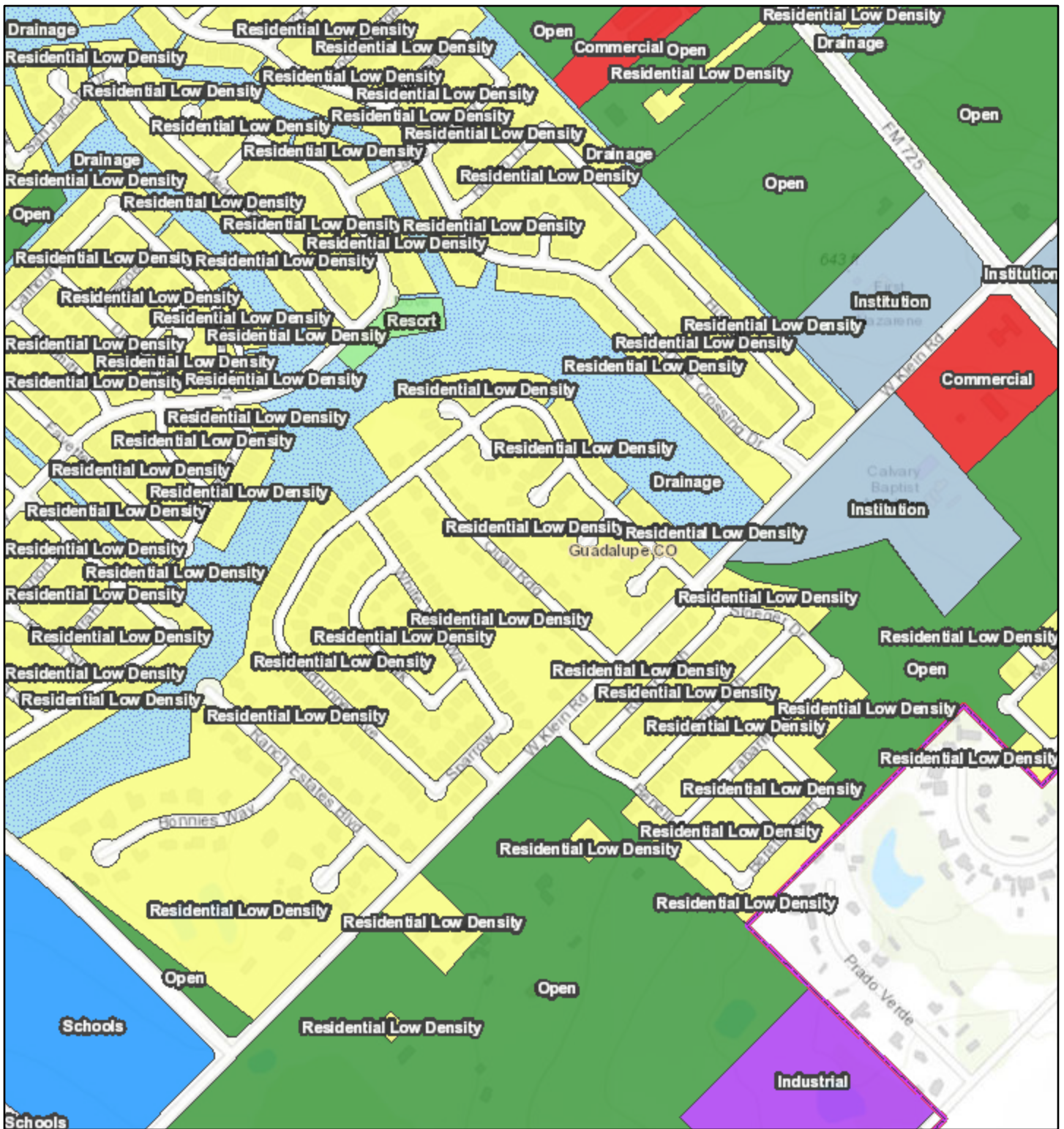
NOTES:

1. STRUCTURAL SECTION REQUIRES DETAILED ENGINEERING DESIGN, SUBJECT TO THE APPROVAL OF THE CITY ENGINEER. CITY WILL ACCEPT DESIGNS THAT INCORPORATE BIAXIAL GEOGRID.
2. SEE CURB DETAIL ST-013.
3. BASE MUST EXTEND 1' BEYOND BACK OF CURB, 6" MINIMUM THICKNESS

| | | | |
|--|-----------------|---------------|--|
| DATE APPROVED: 7/08 | DWG. NO: ST-006 | SCALE: N.T.S. |  |
| DRAWN BY: RAS | SHEET: 1 OF 1 | | |
| FILENAME: Minor Arterial (4) Lanes | | | |
| P:\CURRENT NEW BRAUNFELS DETAILS\2006\ | | | ENGINEERING DEPARTMENT |

APPENDIX A3

Klein Road Phase 2 Existing Land Use Map



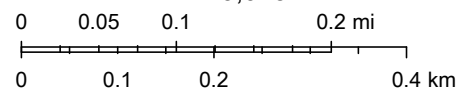
7/31/2018 1:14:13 PM

1:9,028

Existing Land Use (Shaded)

- Residential Low Density (Less than 5 Units/Acre)
- Residential Medium (6-12 Units/Acre)
- Manufactured Homes
- Residential High Density (12+ Units/Acre)
- Mobile Home Park

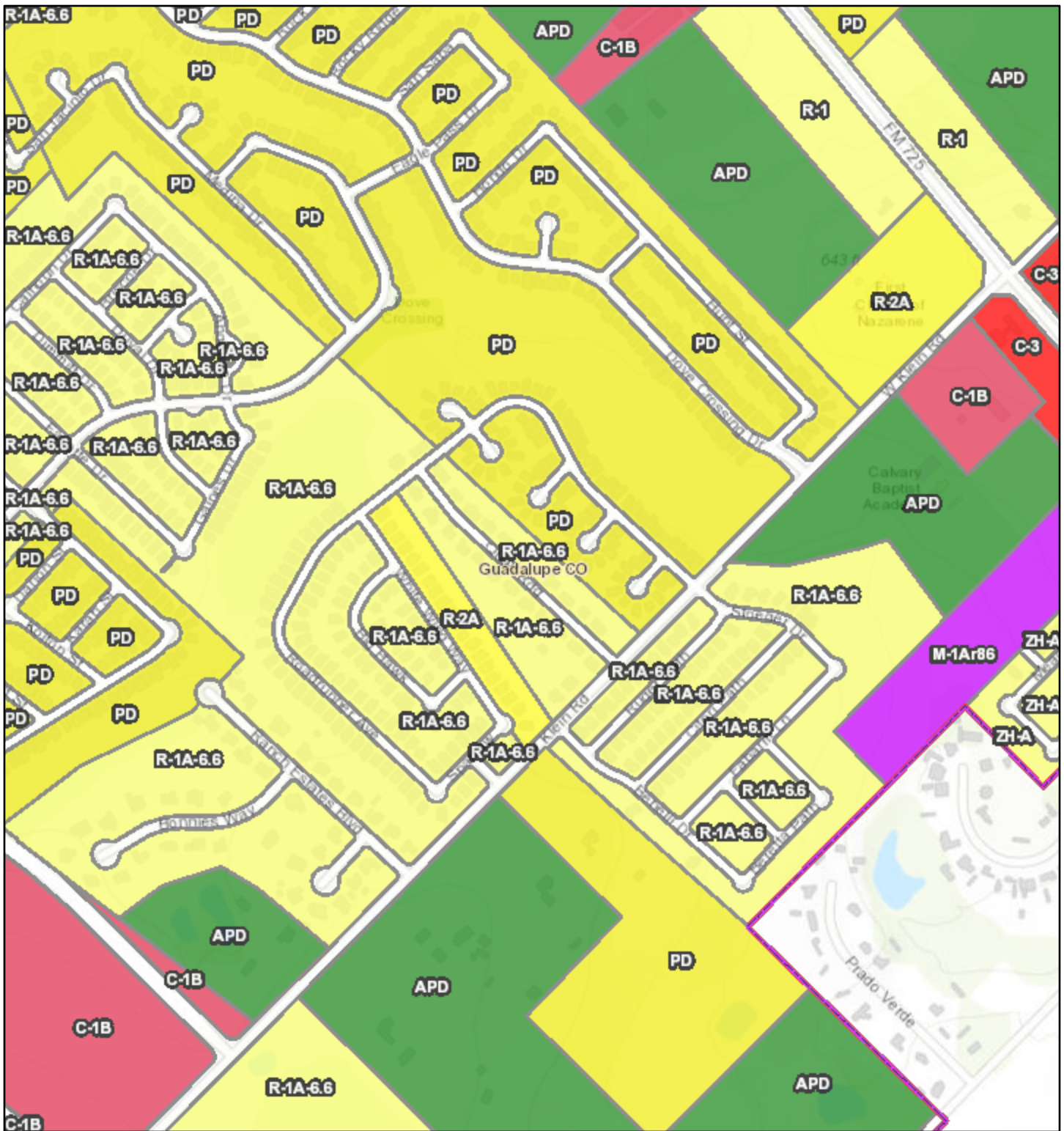
- Commercial
- Industrial
- Schools
- Government
- Institution



Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), swisstopo, © OpenStreetMap contributors, and the GIS User Community

APPENDIX A4

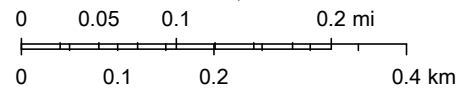
Klein Road Phase 2 Zoning Map



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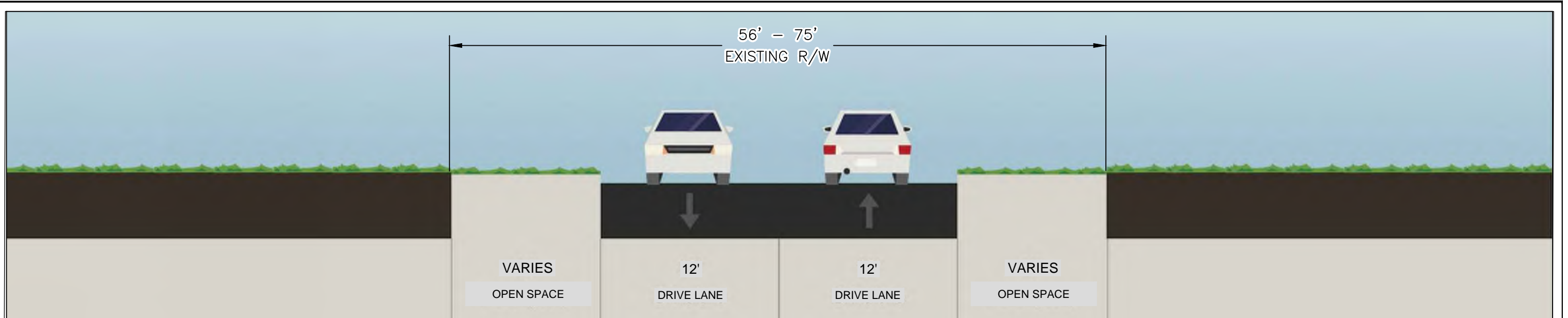
1:9,028

- Zoning (Shaded)
- APD
 - B-1
 - B-1A
 - B-1B
 - C-1
 - C-1A
 - C-1B
 - C-2
 - C-2A
 - C-3

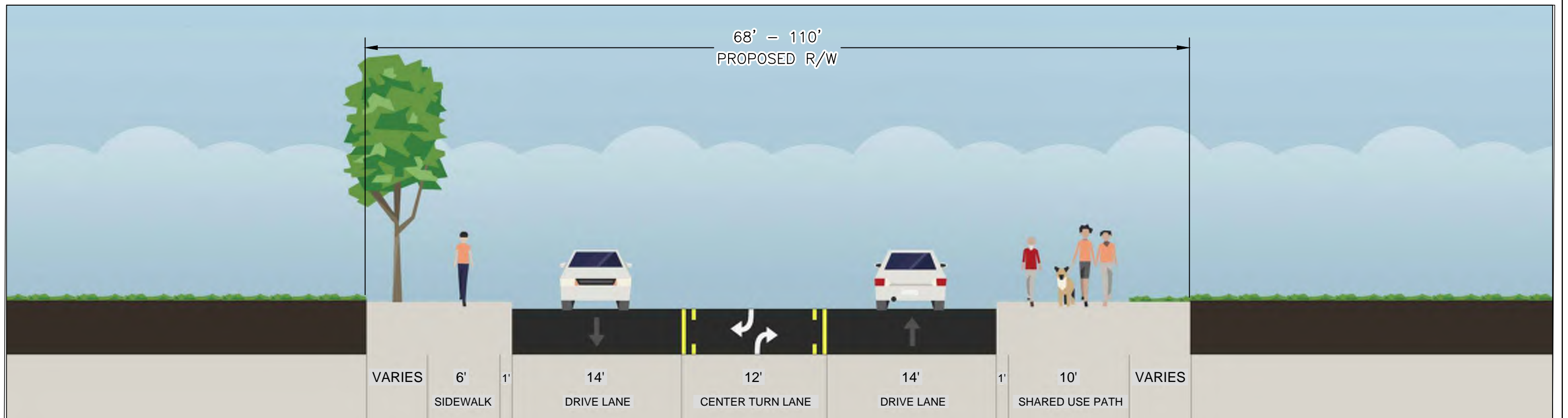


Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), swisstopo, © OpenStreetMap contributors, and the GIS User Community

APPENDIX A5



A EXISTING TYPICAL ROADWAY CROSS SECTION (FACING NORTHEAST)
NOT TO SCALE



B PROPOSED TYPICAL ROADWAY CROSS SECTION (FACING NORTHEAST)
NOT TO SCALE

NOTES:

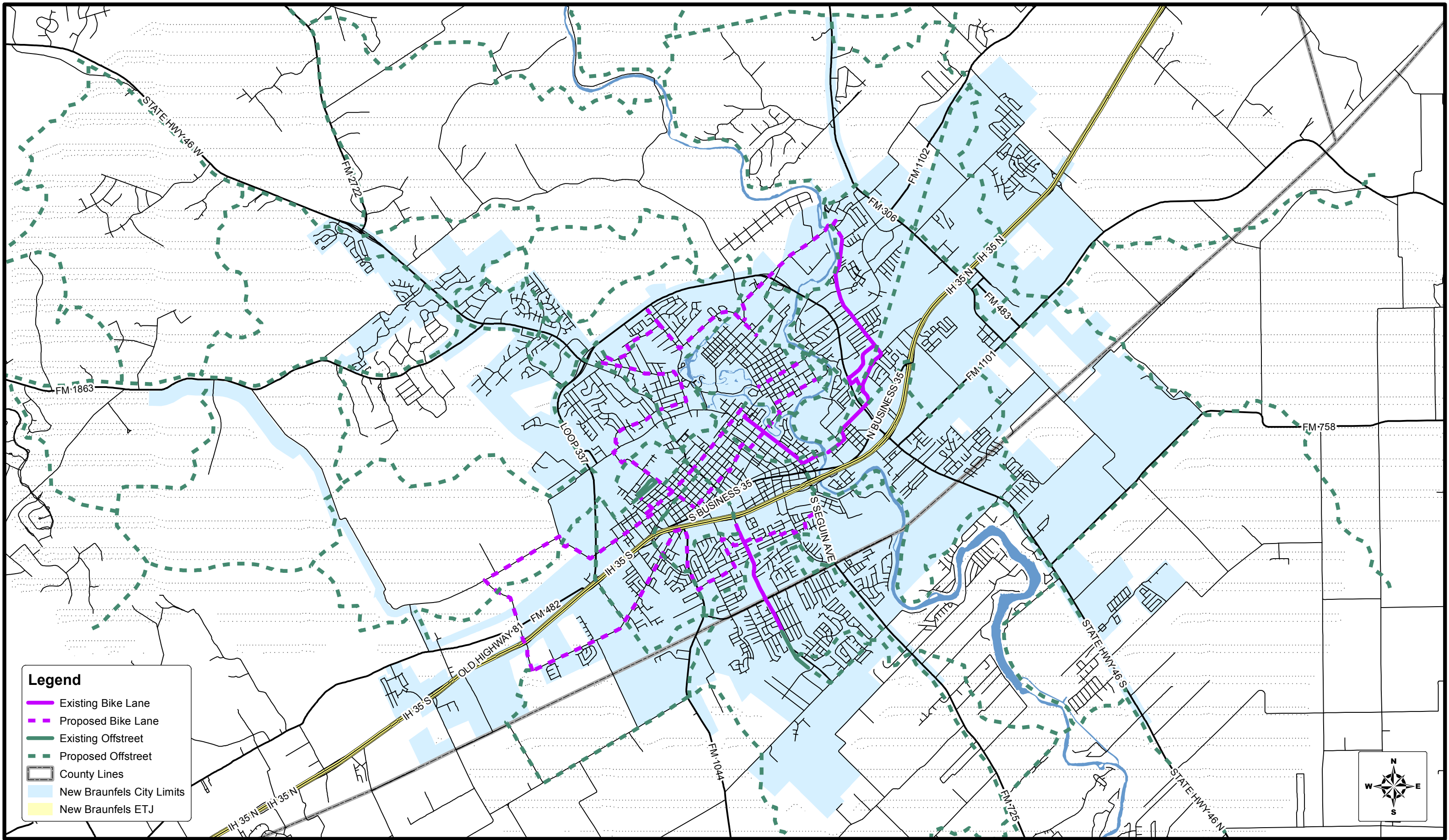
- ASSUMED SURFACING THICKNESS TO MATCH PHASE 1 PAVEMENT SECTION:
- 9" FLEX BASE (CMP IN PLC) (TYPE A GR 1) (FINAL POS)
 - 12" LIME TREATED SUBGRADE
 - 2" HMAC - Type C (PG 70-22 BINDER)
 - 2" HMAC - Type D (PG 76-22 BINDER)
 - TENSAR TX-5 GEOGRID
 - PRIME COAT (MC-30)
 - TACK COAT



| | | | |
|---|----------------|-----------------|------------------|
| SHEET 1 OF 5 | | | |
| EXISTING AND PROPOSED TYPICAL SECTIONS W. KLEIN ROAD - WALNUT AVENUE TO FM 725 CONCEPTUAL DESIGN | | | |
| CITY OF NEW BRAUNFELS NEW BRAUNFELS, TEXAS | | | |
| Drawn By: TM | Checked By: TR | Scale: AS SHOWN | Date: 11/21/2017 |

M:\CTOF\NEWBRAUNFELS\CADD\KLEINRD\H2APP\XREFS\PROPROAD

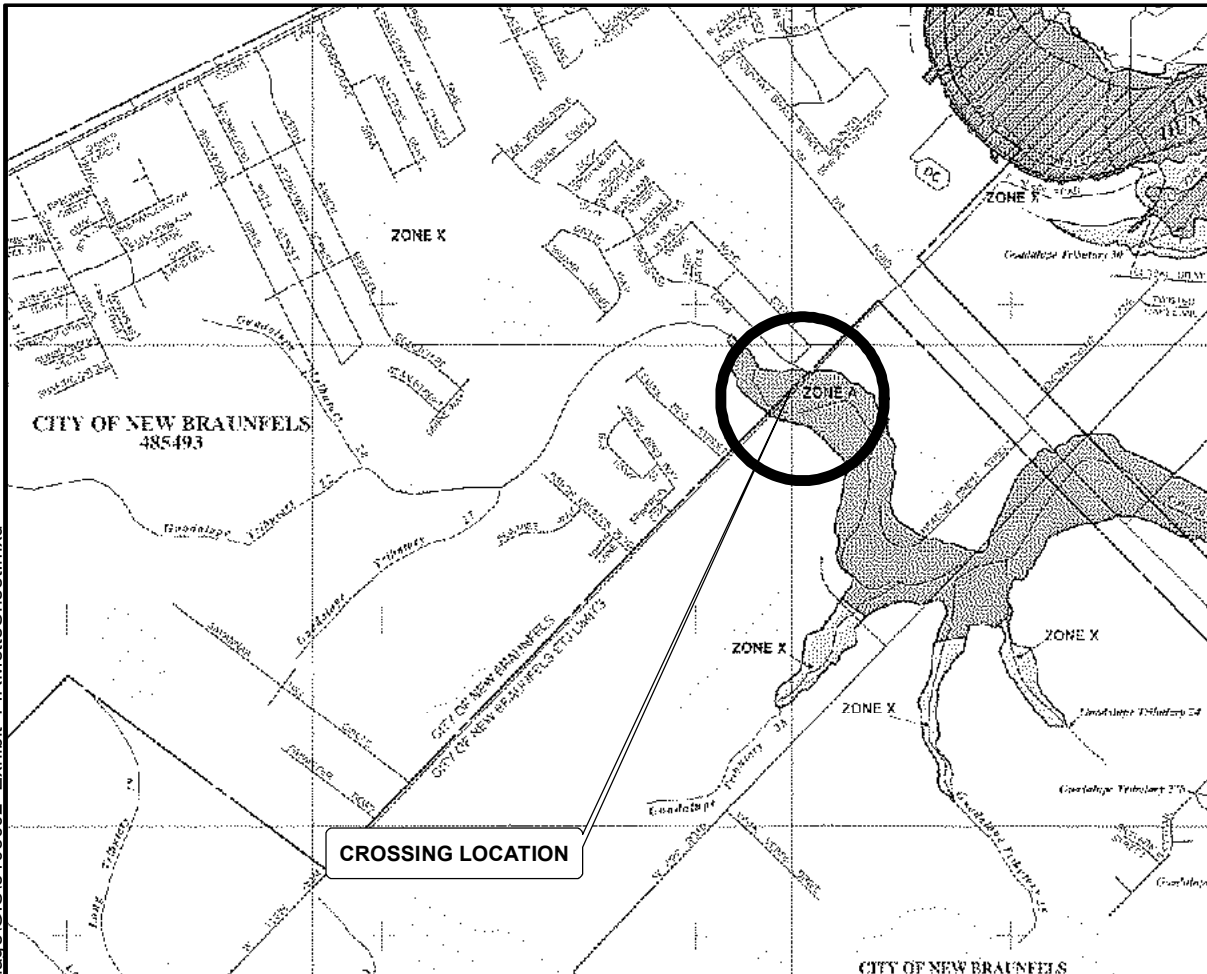
APPENDIX A6



APPENDIX A7

APPENDIX B1

\\pape-dawson\pdt\H\projects\51030\02\design\Civil\Drainage\GIS\5103002 Exhibit FIRMetteSheet.mxd




PANEL 0115F

FIRM
FLOOD INSURANCE RATE MAP
GUADALUPE COUNTY,
TEXAS
AND INCORPORATED AREAS

PANEL 115 OF 480
SEE MAP INDEX FOR 1997 PANEL LAYOUT

| | | | |
|------------------|--------|-------|--------|
| CONTAINS: | NUMBER | PANEL | SHEETS |
| COMMUNITY | 48593 | 011 | 1 |
| WARRANTY EXPIRES | 48593 | 011 | 1 |

Note to User: The Map Number does not refer to the actual printing and order. The Community Number shown above should be used for insurance applications to the proper authority.




MAP NUMBER
48187C0115F

EFFECTIVE DATE
NOVEMBER 2, 2007

Federal Emergency Management Agency





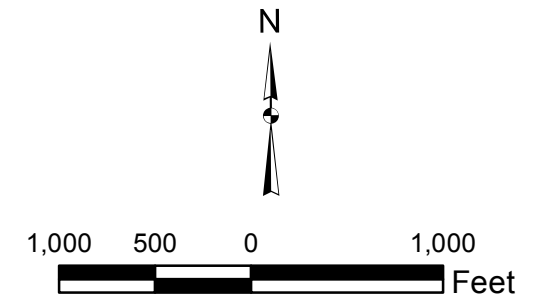
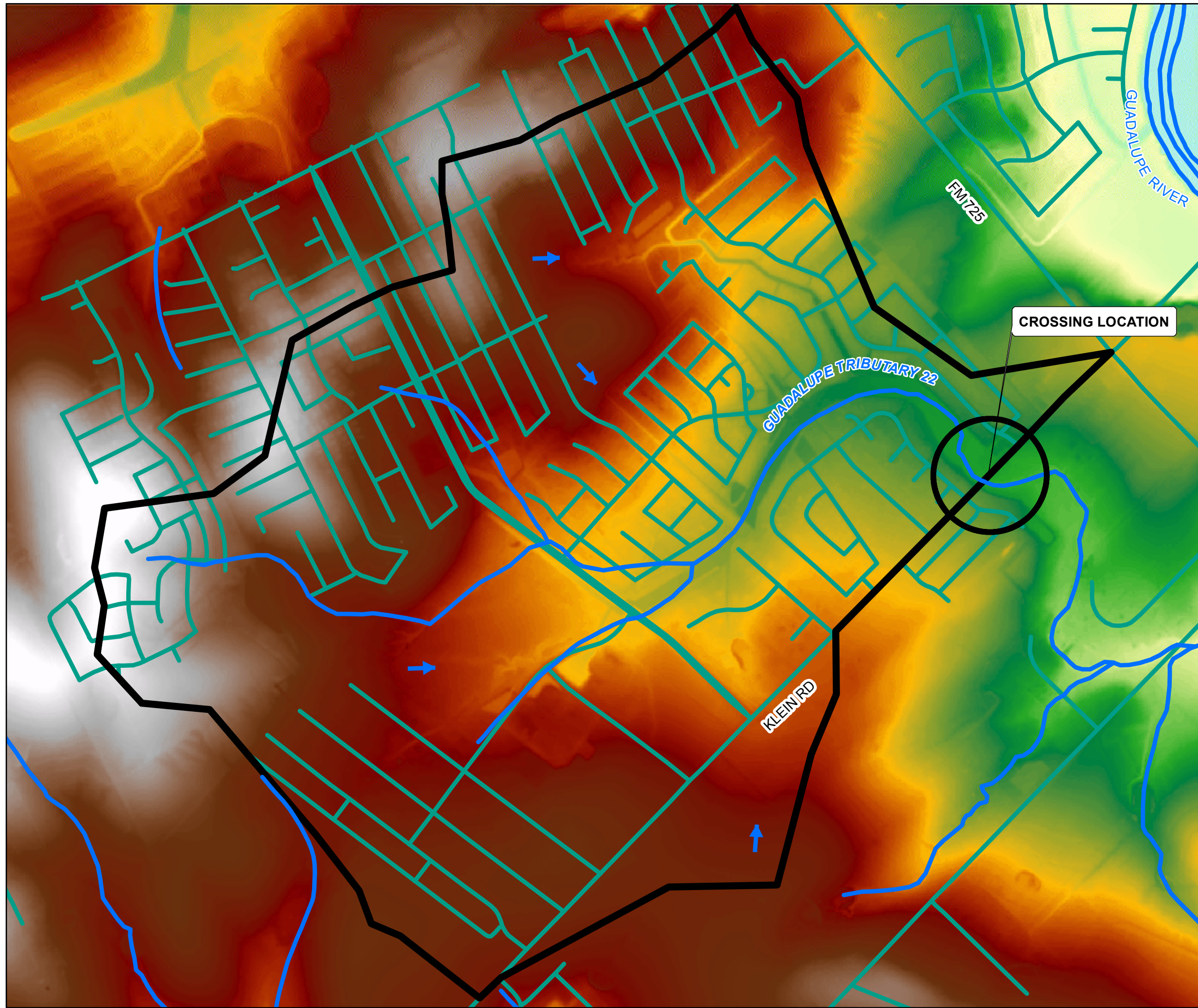
PAPE-DAWSON ENGINEERS
San Antonio | Austin | Houston | Fort Worth | Dallas
TBPE Firm Reg. #470

**KLEIN ROAD
DRAINAGE STUDY
FIRMette**




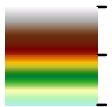

| | | | | | |
|-------------------|-----------|-------------------------|-------------|---------|--------------|
| FED. RD. DIV. NO. | STATE | PAPE-DAWSON PROJECT NO. | | | HIGHWAY NO. |
| - | TEXAS | 51030-02 | | | KLEIN |
| STATE DISTRICT | COUNTY | CONTROL NO. | SECTION NO. | JOB NO. | APPENDIX NO. |
| - | GUADALUPE | - | - | - | - |

APPENDIX B2

\\pape-dawson\pd\H\projects\51030\02\design\Civil\Drainage\GIS\5103002_Exhibit_DrainageAreaMap.mxd



Legend

-  STREAM LINE
-  DRAINAGE AREA BOUNDARY
-  STREETS
- ELEVATION**
- FEET**
-  - High : 755.48
- Low : 574.28
-  FLOW ARROW

SOURCE:
LIDAR DATA OBTAINED FROM FEMA, 2013, NAVD88

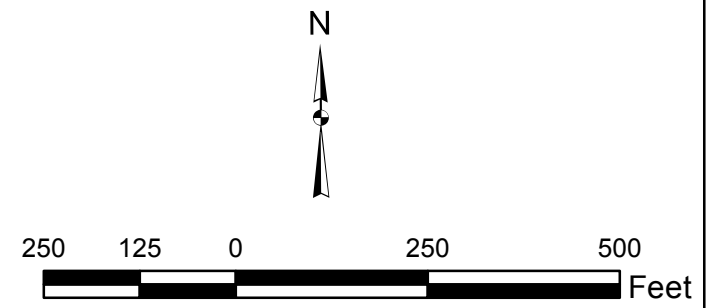
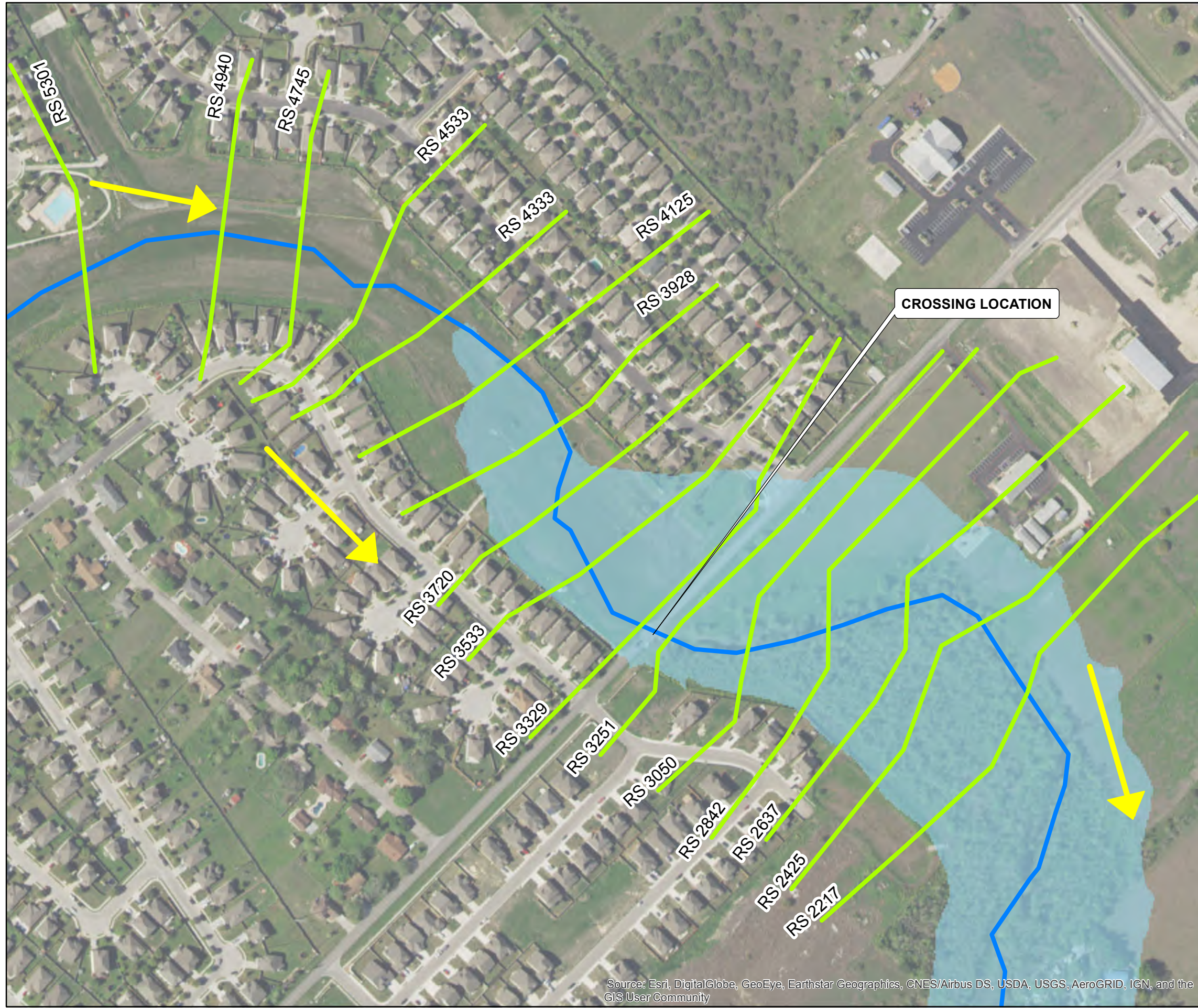
PAPE-DAWSON ENGINEERS
San Antonio | Austin | Houston | Fort Worth | Dallas
TBPE Firm Reg. #470

KLEIN ROAD DRAINAGE STUDY DRAINAGE AREA MAP





| FED. RD. DIV. NO. | STATE | PAPE-DAWSON PROJECT NO. | | | HIGHWAY NO. |
|-------------------|-----------|-------------------------|-------------|---------|--------------|
| - | TEXAS | 51030-02 | | | KLEIN |
| STATE DISTRICT | COUNTY | CONTROL NO. | SECTION NO. | JOB NO. | APPENDIX NO. |
| - | GUADALUPE | - | - | - | |

APPENDIX B3

\\pape-dawson\pd\H\projects\510\30\02\design\Civil\Drainage\GIS\5103002_ Exhibit_CrossSectionLayout.mxd



Legend

-  STREAM LINE
- FLOOD HAZARD ZONE**
-  A
-  HEC-RAS CROSS SECTIONS
-  FLOW ARROW

PAPE-DAWSON ENGINEERS
 San Antonio | Austin | Houston | Fort Worth | Dallas
 TBPE Firm Reg. #470

**KLEIN ROAD DRAINAGE STUDY
 HEC-RAS CROSS SECTION LAYOUT**

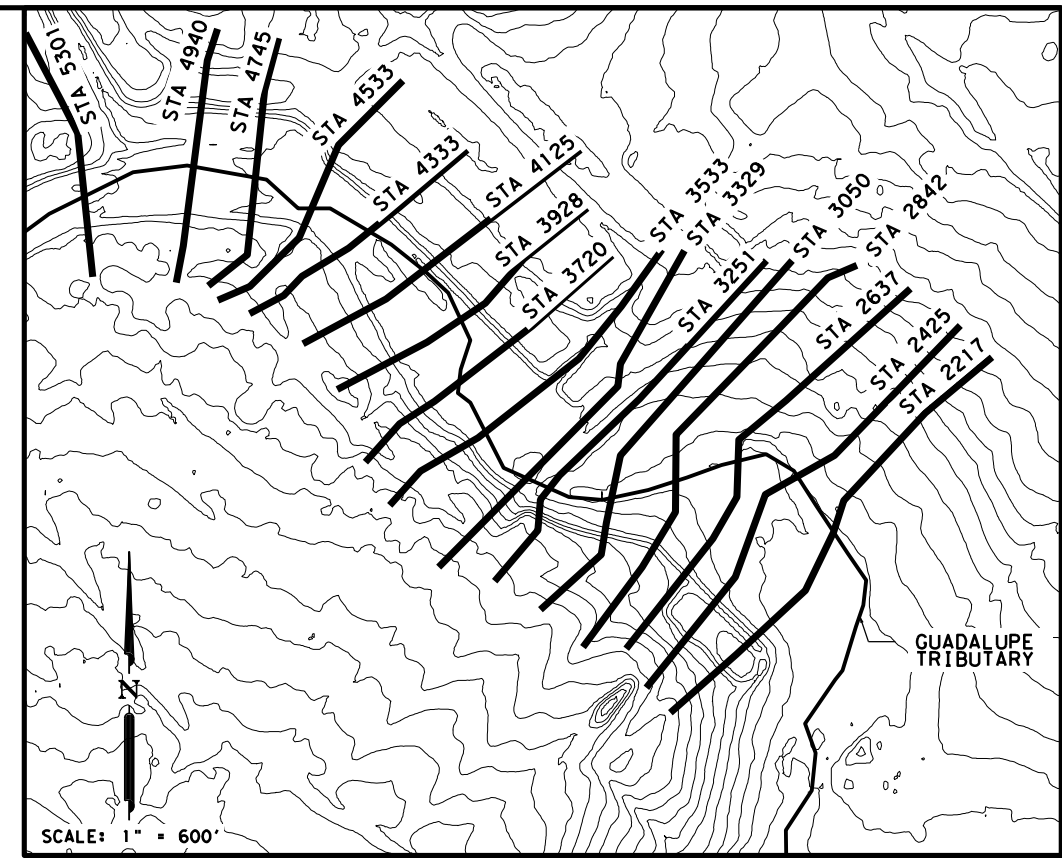
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|-------------------|-----------|-------------------------|-------------|---------|--------------|
| - | TEXAS | 51030-02 | | | KLEIN |
| STATE DISTRICT | COUNTY | CONTROL NO. | SECTION NO. | JOB NO. | APPENDIX NO. |
| - | GUADALUPE | - | - | - | |

Source: Esri, DigitalGlobe, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community

APPENDIX B4

CULVERT HYDRAULIC DATA

| Reach | River Sta | Profile | Plan | Q Total (cfs) | Min Ch El (ft) | W.S. Elev (ft) | Crit W.S. (ft) | E.G. Elev (ft) | E.G. (ft/ft) | Vel Chnl (ft/s) | Flow Area (sq ft) | Top Width (ft) | Froude # |
|-------|-----------|---------|-------|---------------|----------------|----------------|----------------|----------------|--------------|-----------------|-------------------|----------------|----------|
| Trib | 5301 | 50-YR | EX | 5021 | 628.00 | 631.27 | 631.26 | 632.69 | 0.011795 | 9.64 | 536.40 | 198.35 | 0.98 |
| Trib | 5301 | 50-YR | PR CV | 5021 | 628.00 | 631.27 | 631.26 | 632.69 | 0.011799 | 9.64 | 536.33 | 198.34 | 0.98 |
| Trib | 5301 | 100-YR | EX | 6260 | 628.00 | 631.75 | 631.75 | 633.36 | 0.011068 | 10.30 | 634.11 | 211.17 | 0.97 |
| Trib | 5301 | 100-YR | PR CV | 6260 | 628.00 | 631.75 | 631.75 | 633.36 | 0.011068 | 10.30 | 634.11 | 211.17 | 0.97 |
| Trib | 4940 | 50-YR | EX | 5021 | 626.40 | 630.09 | | 630.47 | 0.003000 | 4.92 | 1038.13 | 377.08 | 0.49 |
| Trib | 4940 | 50-YR | PR CV | 5021 | 626.40 | 630.09 | | 630.47 | 0.002997 | 4.92 | 1038.43 | 377.18 | 0.49 |
| Trib | 4940 | 100-YR | EX | 6260 | 626.40 | 630.55 | | 630.98 | 0.002908 | 5.30 | 1221.85 | 433.34 | 0.50 |
| Trib | 4940 | 100-YR | PR CV | 6260 | 626.40 | 630.55 | | 630.98 | 0.002901 | 5.30 | 1222.88 | 433.57 | 0.50 |
| Trib | 4745 | 50-YR | EX | 5021 | 625.80 | 629.62 | | 629.94 | 0.002302 | 4.54 | 1142.97 | 438.47 | 0.44 |
| Trib | 4745 | 50-YR | PR CV | 5021 | 625.80 | 629.62 | | 629.94 | 0.002299 | 4.53 | 1143.64 | 438.65 | 0.44 |
| Trib | 4745 | 100-YR | EX | 6260 | 625.80 | 630.10 | | 630.46 | 0.002217 | 4.87 | 1366.59 | 495.39 | 0.44 |
| Trib | 4745 | 100-YR | PR CV | 6260 | 625.80 | 630.11 | | 630.46 | 0.002208 | 4.86 | 1368.68 | 495.94 | 0.44 |
| Trib | 4533 | 50-YR | EX | 5021 | 624.89 | 629.15 | | 629.47 | 0.002156 | 4.79 | 1242.52 | 483.23 | 0.43 |
| Trib | 4533 | 50-YR | PR CV | 5021 | 624.89 | 629.16 | | 629.47 | 0.002149 | 4.79 | 1243.88 | 483.32 | 0.43 |
| Trib | 4533 | 100-YR | EX | 6260 | 624.89 | 629.68 | | 630.01 | 0.001965 | 4.99 | 1502.04 | 499.12 | 0.42 |
| Trib | 4533 | 100-YR | PR CV | 6260 | 624.89 | 629.69 | | 630.02 | 0.001952 | 4.98 | 1505.51 | 499.32 | 0.42 |
| Trib | 4333 | 50-YR | EX | 5021 | 624.21 | 628.14 | | 628.81 | 0.004762 | 6.58 | 777.79 | 268.30 | 0.63 |
| Trib | 4333 | 50-YR | PR CV | 5021 | 624.21 | 628.16 | | 628.82 | 0.004708 | 6.56 | 780.84 | 268.69 | 0.63 |
| Trib | 4333 | 100-YR | EX | 6260 | 624.21 | 628.58 | | 629.38 | 0.004866 | 7.21 | 897.49 | 283.31 | 0.65 |
| Trib | 4333 | 100-YR | PR CV | 6260 | 624.21 | 628.61 | | 629.39 | 0.004748 | 7.16 | 905.15 | 284.24 | 0.64 |
| Trib | 4125 | 50-YR | EX | 5021 | 623.44 | 627.50 | | 627.96 | 0.003104 | 5.46 | 937.44 | 300.44 | 0.51 |
| Trib | 4125 | 50-YR | PR CV | 5021 | 623.44 | 627.53 | | 627.98 | 0.003013 | 5.41 | 946.75 | 302.23 | 0.51 |
| Trib | 4125 | 100-YR | EX | 6260 | 623.44 | 627.92 | | 628.48 | 0.003259 | 6.04 | 1070.26 | 324.35 | 0.54 |
| Trib | 4125 | 100-YR | PR CV | 6260 | 623.44 | 627.99 | | 628.53 | 0.003070 | 5.93 | 1092.52 | 328.00 | 0.52 |
| Trib | 3928 | 50-YR | EX | 5021 | 623.23 | 627.03 | | 627.38 | 0.002479 | 4.80 | 1061.52 | 332.55 | 0.46 |
| Trib | 3928 | 50-YR | PR CV | 5021 | 623.23 | 627.08 | | 627.43 | 0.002345 | 4.72 | 1080.35 | 333.73 | 0.45 |
| Trib | 3928 | 100-YR | EX | 6260 | 623.23 | 627.43 | | 627.87 | 0.002630 | 5.33 | 1198.65 | 341.02 | 0.48 |
| Trib | 3928 | 100-YR | PR CV | 6260 | 623.23 | 627.55 | | 627.96 | 0.002369 | 5.16 | 1239.41 | 343.50 | 0.46 |
| Trib | 3720 | 50-YR | EX | 5021 | 622.63 | 626.63 | | 626.91 | 0.001902 | 4.30 | 1188.94 | 360.67 | 0.40 |
| Trib | 3720 | 50-YR | PR CV | 5021 | 622.63 | 626.72 | | 626.99 | 0.001748 | 4.19 | 1221.17 | 362.20 | 0.39 |
| Trib | 3720 | 100-YR | EX | 6260 | 622.63 | 627.00 | | 627.36 | 0.002099 | 4.83 | 1325.56 | 367.96 | 0.43 |
| Trib | 3720 | 100-YR | PR CV | 6260 | 622.63 | 627.18 | | 627.51 | 0.001796 | 4.61 | 1393.34 | 372.08 | 0.40 |
| Trib | 3533 | 50-YR | EX | 5021 | 622.42 | 626.38 | | 626.58 | 0.001407 | 3.83 | 1512.73 | 559.00 | 0.35 |
| Trib | 3533 | 50-YR | PR CV | 5021 | 622.42 | 626.50 | | 626.69 | 0.001242 | 3.67 | 1580.84 | 565.38 | 0.33 |
| Trib | 3533 | 100-YR | EX | 6260 | 622.42 | 626.75 | | 627.00 | 0.001510 | 4.23 | 1724.12 | 577.78 | 0.37 |
| Trib | 3533 | 100-YR | PR CV | 6260 | 622.42 | 627.00 | | 627.20 | 0.001207 | 3.93 | 1865.82 | 590.17 | 0.33 |
| Trib | 3329 | 50-YR | EX | 5021 | 621.25 | 625.99 | 624.54 | 626.28 | 0.001515 | 4.45 | 1270.68 | 543.66 | 0.42 |
| Trib | 3329 | 50-YR | PR CV | 5021 | 621.25 | 624.62 | 624.62 | 625.83 | 0.009621 | 8.82 | 570.20 | 336.92 | 0.99 |
| Trib | 3329 | 100-YR | EX | 6260 | 621.25 | 626.30 | 624.90 | 626.66 | 0.001701 | 4.99 | 1446.38 | 589.76 | 0.45 |
| Trib | 3329 | 100-YR | PR CV | 6260 | 621.25 | 625.37 | 625.02 | 626.46 | 0.006122 | 8.41 | 748.89 | 484.89 | 0.83 |
| Trib | 3296 | | | | | | | | | | | | |
| Trib | | | | Culvert | | | | | | | | | |
| Trib | 3251 | 50-YR | EX | 5021 | 619.25 | 624.15 | | 624.69 | 0.004690 | 7.12 | 999.54 | 570.09 | 0.72 |
| Trib | 3251 | 50-YR | PR CV | 5021 | 619.25 | 624.38 | 624.38 | 625.67 | 0.007827 | 9.65 | 584.96 | 592.38 | 0.94 |
| Trib | 3251 | 100-YR | EX | 6260 | 619.25 | 624.49 | | 625.06 | 0.004430 | 7.43 | 1199.76 | 601.56 | 0.71 |
| Trib | 3251 | 100-YR | PR CV | 6260 | 619.25 | 624.79 | 624.79 | 626.28 | 0.007763 | 10.40 | 678.59 | 627.92 | 0.95 |
| Trib | 3050 | 50-YR | EX | 5021 | 619.11 | 623.61 | | 623.95 | 0.002560 | 5.82 | 1227.97 | 569.90 | 0.55 |
| Trib | 3050 | 50-YR | PR CV | 5021 | 619.11 | 623.61 | | 623.95 | 0.002560 | 5.82 | 1227.97 | 569.90 | 0.55 |
| Trib | 3050 | 100-YR | EX | 6260 | 619.11 | 623.95 | | 624.33 | 0.002604 | 6.24 | 1426.26 | 594.31 | 0.56 |
| Trib | 3050 | 100-YR | PR CV | 6260 | 619.11 | 623.95 | | 624.33 | 0.002604 | 6.24 | 1426.26 | 594.31 | 0.56 |
| Trib | 2842 | 50-YR | EX | 5021 | 618.69 | 622.21 | 622.20 | 623.04 | 0.007879 | 8.20 | 788.35 | 486.92 | 0.91 |
| Trib | 2842 | 50-YR | PR CV | 5021 | 618.69 | 622.21 | 622.20 | 623.04 | 0.007879 | 8.20 | 788.35 | 486.92 | 0.91 |
| Trib | 2842 | 100-YR | EX | 6260 | 618.69 | 622.51 | 622.49 | 623.42 | 0.007676 | 8.72 | 939.36 | 522.44 | 0.91 |
| Trib | 2842 | 100-YR | PR CV | 6260 | 618.69 | 622.51 | 622.49 | 623.42 | 0.007676 | 8.72 | 939.36 | 522.44 | 0.91 |
| Trib | 2637 | 50-YR | EX | 5021 | 618.12 | 621.41 | | 621.81 | 0.003859 | 6.09 | 1069.82 | 541.42 | 0.64 |
| Trib | 2637 | 50-YR | PR CV | 5021 | 618.12 | 621.41 | | 621.81 | 0.003859 | 6.09 | 1069.82 | 541.42 | 0.64 |
| Trib | 2637 | 100-YR | EX | 6260 | 618.12 | 621.71 | | 622.18 | 0.004004 | 6.64 | 1233.78 | 564.70 | 0.67 |
| Trib | 2637 | 100-YR | PR CV | 6260 | 618.12 | 621.71 | | 622.18 | 0.004004 | 6.64 | 1233.78 | 564.70 | 0.67 |
| Trib | 2425 | 50-YR | EX | 5021 | 617.81 | 620.61 | | 621.00 | 0.003778 | 5.13 | 1060.32 | 605.39 | 0.61 |
| Trib | 2425 | 50-YR | PR CV | 5021 | 617.81 | 620.61 | | 621.00 | 0.003778 | 5.13 | 1060.32 | 605.39 | 0.61 |
| Trib | 2425 | 100-YR | EX | 6260 | 617.81 | 620.95 | | 621.37 | 0.003492 | 5.42 | 1268.73 | 635.13 | 0.60 |
| Trib | 2425 | 100-YR | PR CV | 6260 | 617.81 | 620.95 | | 621.37 | 0.003492 | 5.42 | 1268.73 | 635.13 | 0.60 |
| Trib | 2217 | 50-YR | EX | 5021 | 616.95 | 619.99 | 619.10 | 620.34 | 0.002602 | 4.83 | 1097.70 | 524.03 | 0.52 |
| Trib | 2217 | 50-YR | PR CV | 5021 | 616.95 | 619.99 | 619.10 | 620.34 | 0.002602 | 4.83 | 1097.70 | 524.03 | 0.52 |
| Trib | 2217 | 100-YR | EX | 6260 | 616.95 | 620.34 | 619.37 | 620.75 | 0.002600 | 5.24 | 1282.59 | 548.21 | 0.53 |
| Trib | 2217 | 100-YR | PR CV | 6260 | 616.95 | 620.34 | 619.37 | 620.75 | 0.002600 | 5.24 | 1282.59 | 548.21 | 0.53 |



NOTES:
 1. DATA PRESENTED FROM DRAINAGE SUMMARY FOR KLEIN ROAD PREPARED BY PAPE-DAWSON ENGINEERS. DATED JULY 2018.
 2. GUADALUPE TRIBUTARY 22 IS IDENTIFIED ON FEMA FIRM PANEL 48187C0115F, DATED NOVEMBER 2, 2007. THE UPSTREAM/DOWNSTREAM AREA AND EXISTING CROSSING ARE WITHIN A ZONE "A".

HYDRAULIC METHOD
 WATER SURFACE ELEVATIONS COMPUTED USING A HEC-RAS (V.5.0.3) MODEL CREATED FOR GUADALUPE TRIBUTARY 22.
 FILE NAME: "5103002_KLEINRD.PRJ"
 EFFECTIVE AND PROPOSED MODELS WERE DEVELOPED USING LIDAR DATA AND FIELD DATA.
 EFFECTIVE CONDITION WATER SURFACE ELEVATIONS COMPUTED FROM HEC-RAS MODEL PLAN "EXISTING" NAMED "5103002_KLEINRD.P01".
 PROPOSED CONDITION WATER SURFACE ELEVATIONS COMPUTED FROM HEC-RAS MODEL PLAN "PROP CULVERT" NAMED "5103002_KLEINRD.P03".

HYDROLOGIC METHOD
 FLOWS USED FOR MODELS WERE CALCULATED FROM THE SCS HYDROGRAPH METHOD AND INFORMATION FROM THE CITY OF NEW BRAUNFELS - DRAINAGE AND EROSION CONTROL DESIGN MANUAL.

| REV. NO. | DATE | DESCRIPTION | BY |
|----------|------|-------------|----|
| | | | |

SAN ANTONIO | AUSTIN | HOUSTON | FORT WORTH | DALLAS
 2000 NW LOOP 410 | SAN ANTONIO, TX 78213 | 210.375.9000
 TBPE FIRM REGISTRATION #470 | TPLS FIRM REGISTRATION #10028800

**KLEIN ROAD
 PROPOSED CULVERT
 HYDRAULIC DATA
 SHEET**

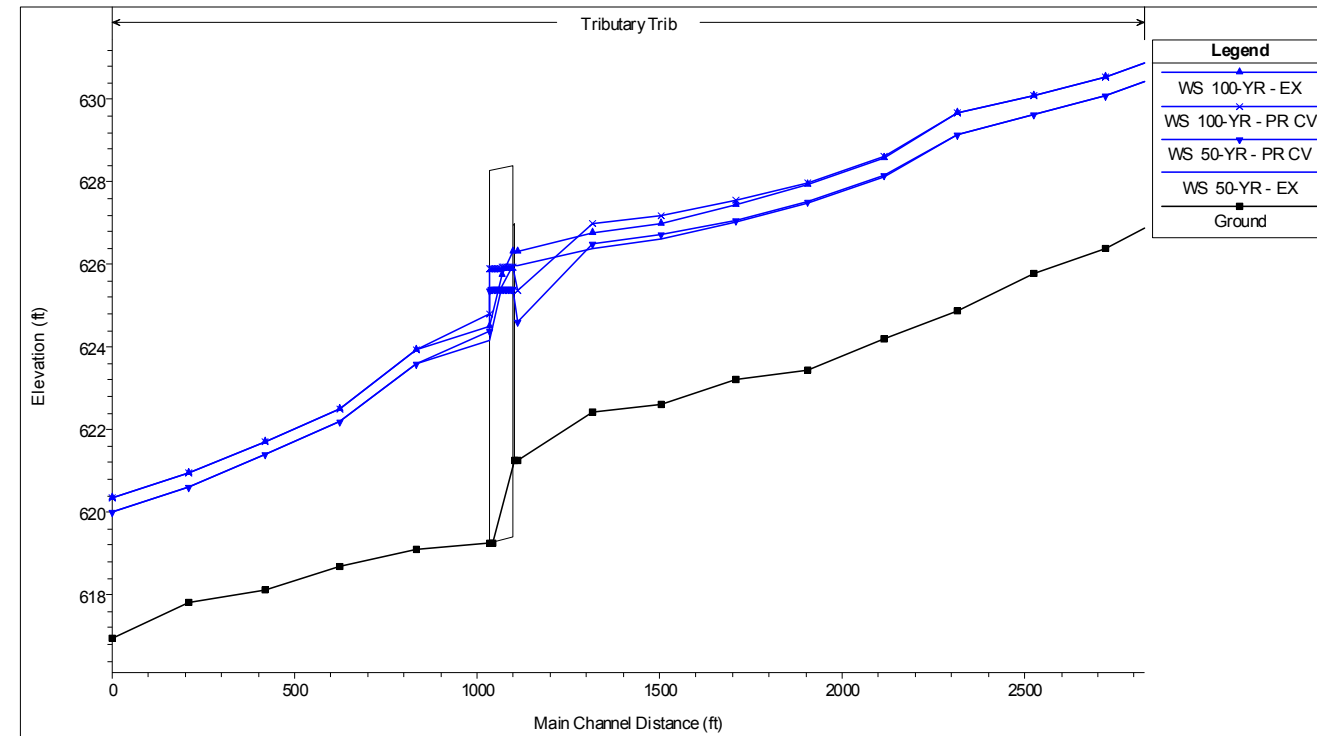
SHEET 1 OF 4

Plotted on: 7/30/2018
 Design File name: \\pape-dawson\pd\h\projects\5103002\des\civ\Drainage\5103002\hds01.dgn

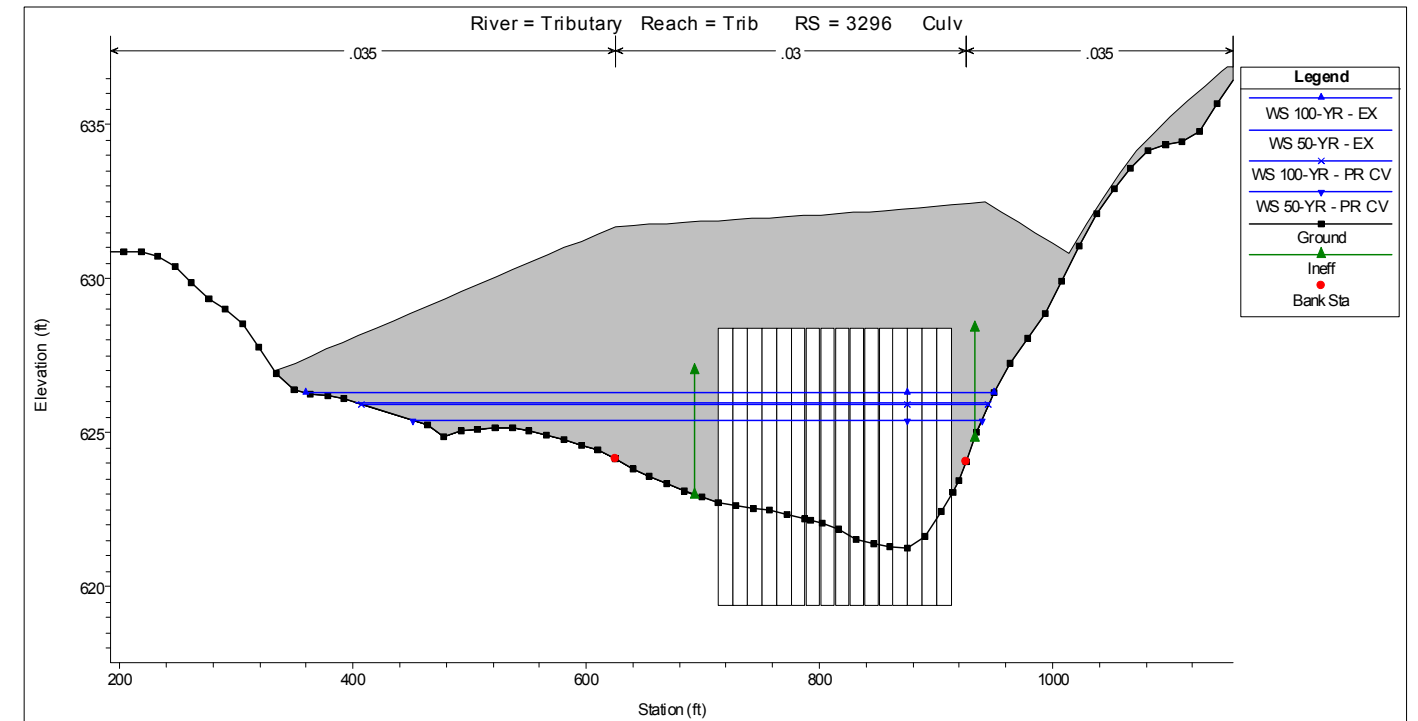
Plotted on: 7/30/2018

Design File Name: \\pape-dawson\pd\h\projects\10\30\02\design\Civil\Drainage\5103002\hds02.dgn

HEC-RAS CHANNEL PROFILE



HEC-RAS CULVERT UPSTREAM



HEC-RAS CULVERT OUTPUT

| Trib RS: 3296 Culv Group: Culvert #1 Profile: 50-YR | | | | | | |
|---|--------|---------|------------------------|---------|--------|--|
| Plan | EX | PR CV | | EX | PR CV | |
| Q Culv Group (cfs) | 63.97 | 5021.00 | Culv Full Len (ft) | 30.00 | 60.00 | |
| # Barrels | 3 | 16 | Culv Vel US (ft/s) | 6.79 | 4.36 | |
| Q Barrel (cfs) | 21.32 | 313.81 | Culv Vel DS (ft/s) | 6.79 | 4.27 | |
| E.G. US. (ft) | 626.28 | 625.81 | Culv Inv El Up (ft) | 619.40 | 619.40 | |
| W.S. US. (ft) | 625.99 | 624.62 | Culv Inv El Dn (ft) | 619.26 | 619.26 | |
| E.G. DS (ft) | 624.69 | 625.67 | Culv Frctn Ls (ft) | 0.91 | 0.00 | |
| W.S. DS (ft) | 624.15 | 624.38 | Culv Exit Loss (ft) | 0.18 | 0.00 | |
| Delta EG (ft) | 1.59 | 0.14 | Culv Entr Loss (ft) | 0.50 | 0.12 | |
| Delta WS (ft) | 1.84 | 0.25 | Q Weir (cfs) | 4961.35 | | |
| E.G. IC (ft) | 626.26 | 623.77 | Weir Sta Lft (ft) | 361.67 | | |
| E.G. OC (ft) | 626.28 | 625.81 | Weir Sta Rgt (ft) | 947.24 | | |
| Culvert Control | Outlet | Outlet | Weir Submerg | 0.26 | | |
| Culv WS Inlet (ft) | 621.40 | 625.40 | Weir Max Depth (ft) | 4.01 | | |
| Culv WS Outlet (ft) | 621.26 | 625.39 | Weir Avg Depth (ft) | 2.03 | | |
| Culv Nml Depth (ft) | | 3.31 | Weir Flow Area (sq ft) | 1188.40 | | |
| Culv Crt Depth (ft) | 1.65 | 2.77 | Min El Weir Flow (ft) | 622.27 | 627.01 | |

| Trib RS: 3296 Culv Group: Culvert #1 Profile: 100-YR | | | | | | |
|--|--------|---------|------------------------|---------|--------|--|
| Plan | EX | PR CV | | EX | PR CV | |
| Q Culv Group (cfs) | 64.56 | 6260.00 | Culv Full Len (ft) | 30.00 | 60.00 | |
| # Barrels | 3 | 16 | Culv Vel US (ft/s) | 6.85 | 5.00 | |
| Q Barrel (cfs) | 21.52 | 391.25 | Culv Vel DS (ft/s) | 6.85 | 4.90 | |
| E.G. US. (ft) | 626.66 | 626.47 | Culv Inv El Up (ft) | 619.40 | 619.40 | |
| W.S. US. (ft) | 626.30 | 625.37 | Culv Inv El Dn (ft) | 619.26 | 619.26 | |
| E.G. DS (ft) | 625.06 | 626.28 | Culv Frctn Ls (ft) | 0.93 | 0.00 | |
| W.S. DS (ft) | 624.49 | 624.79 | Culv Exit Loss (ft) | 0.16 | 0.00 | |
| Delta EG (ft) | 1.60 | 0.19 | Culv Entr Loss (ft) | 0.51 | 0.16 | |
| Delta WS (ft) | 1.81 | 0.58 | Q Weir (cfs) | 6195.44 | | |
| E.G. IC (ft) | 626.64 | 624.49 | Weir Sta Lft (ft) | 341.77 | | |
| E.G. OC (ft) | 626.66 | 626.47 | Weir Sta Rgt (ft) | 952.74 | | |
| Culvert Control | Outlet | Outlet | Weir Submerg | 0.30 | | |
| Culv WS Inlet (ft) | 621.40 | 625.93 | Weir Max Depth (ft) | 4.39 | | |
| Culv WS Outlet (ft) | 621.26 | 625.91 | Weir Avg Depth (ft) | 2.32 | | |
| Culv Nml Depth (ft) | | 3.86 | Weir Flow Area (sq ft) | 1415.00 | | |
| Culv Crt Depth (ft) | 1.66 | 3.21 | Min El Weir Flow (ft) | 622.27 | 627.01 | |

NOTES:

1. DATA PRESENTED FROM DRAINAGE SUMMARY FOR KLEIN ROAD PREPARED BY PAPE-DAWSON ENGINEERS. DATED JULY 2018.

2. GUADALUPE TRIBUTARY 22 IS IDENTIFIED ON FEMA FIRM PANEL 48187C0115F, DATED NOVEMBER 2, 2007. THE UPSTREAM/DOWNSTREAM AREA AND EXISTING CROSSING ARE WITHIN A ZONE "A".

HYDRAULIC METHOD

WATER SURFACE ELEVATIONS COMPUTED USING A HEC-RAS (V.5.0.3) MODEL CREATED FOR GUADALUPE TRIBUTARY 22. FILE NAME: "5103002_KLEINRD.PRJ"

EFFECTIVE AND PROPOSED MODELS WERE DEVELOPED USING LIDAR DATA AND FIELD DATA.

EFFECTIVE CONDITION WATER SURFACE ELEVATIONS COMPUTED FROM HEC-RAS MODEL PLAN "EXISTING" NAMED "5103002_KLEINRD.P01".

PROPOSED CONDITION WATER SURFACE ELEVATIONS COMPUTED FROM HEC-RAS MODEL PLAN "PROP CULVERT" NAMED "5103002_KLEINRD.P03".

HYDROLOGIC METHOD

FLows USED FOR MODELS WERE CALCULATED FROM THE SCS HYDROGRAPH METHOD AND INFORMATION FROM THE CITY OF NEW BRAUNFELS - DRAINAGE AND EROSION CONTROL DESIGN MANUAL.

| REV. NO. | DATE | DESCRIPTION | BY |
|----------|------|-------------|----|
| | | | |
| | | | |
| | | | |

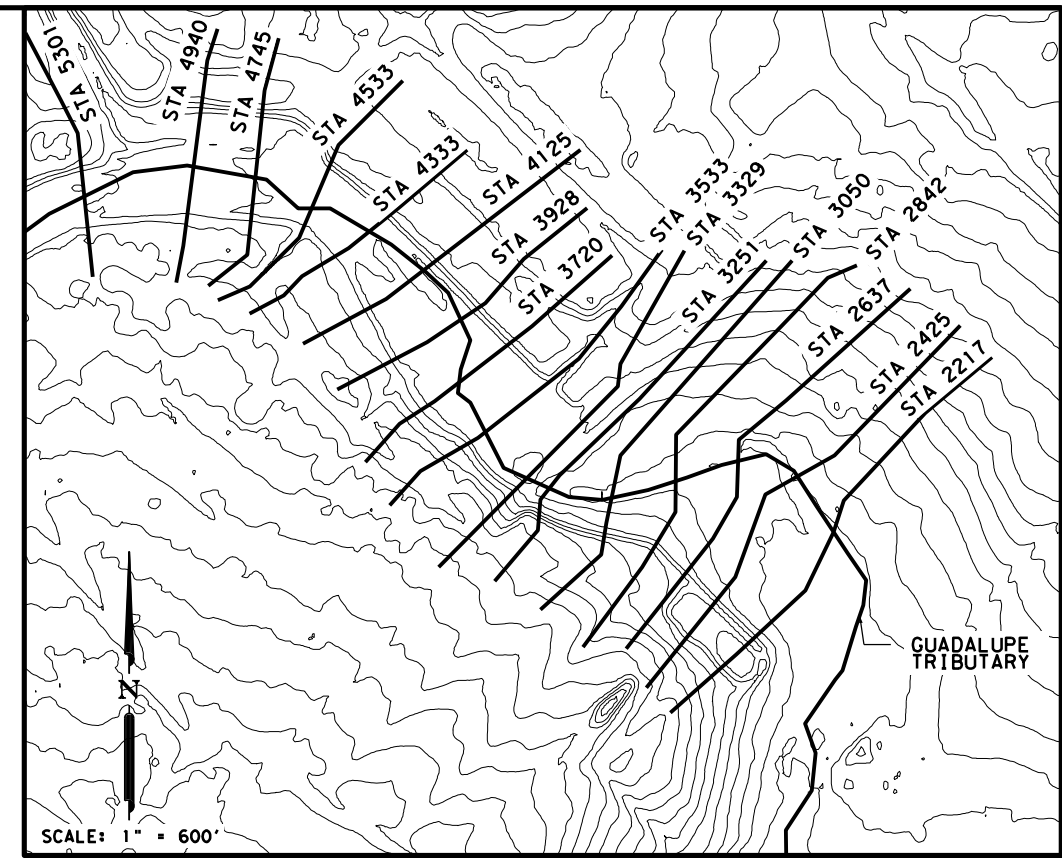
SAN ANTONIO | AUSTIN | HOUSTON | FORT WORTH | DALLAS
2000 NW LOOP 410 | SAN ANTONIO, TX 78213 | 210.375.9000
TBP E FIRM REGISTRATION #470 | TBP L S FIRM REGISTRATION #10028800

KLEIN ROAD PROPOSED CULVERT HYDRAULIC DATA SHEET

SHEET 2 OF 4

BRIDGE HYDRAULIC DATA

| Reach | River Sta | Profile | Plan | Q Total (cfs) | Min Ch El (ft) | W.S. Elev (ft) | Crit W.S. (ft) | E.G. Elev (ft) | E.G. (ft/ft) | Vel Chnl (ft/s) | Flow Area (sq ft) | Top Width (ft) | Froude # |
|-------|-----------|---------|------|---------------|----------------|----------------|----------------|----------------|--------------|-----------------|-------------------|----------------|----------|
| Trib | 5301 | 50-YR | EX | 5021 | 628.00 | 631.27 | 631.26 | 632.69 | 0.011795 | 9.64 | 536.40 | 198.35 | 0.98 |
| Trib | 5301 | 50-YR | PRBR | 5021 | 628.00 | 631.27 | 631.26 | 632.69 | 0.011790 | 9.64 | 536.48 | 198.36 | 0.98 |
| Trib | 5301 | 100-YR | EX | 6260 | 628.00 | 631.75 | 631.75 | 633.36 | 0.011068 | 10.30 | 634.11 | 211.17 | 0.97 |
| Trib | 5301 | 100-YR | PRBR | 6260 | 628.00 | 631.75 | 631.75 | 633.36 | 0.011068 | 10.30 | 634.11 | 211.17 | 0.97 |
| Trib | 4940 | 50-YR | EX | 5021 | 626.40 | 630.09 | | 630.47 | 0.003000 | 4.92 | 1038.13 | 377.08 | 0.49 |
| Trib | 4940 | 50-YR | PRBR | 5021 | 626.40 | 630.09 | | 630.47 | 0.003002 | 4.92 | 1037.90 | 377.01 | 0.49 |
| Trib | 4940 | 100-YR | EX | 6260 | 626.40 | 630.55 | | 630.98 | 0.002908 | 5.30 | 1221.85 | 433.34 | 0.50 |
| Trib | 4940 | 100-YR | PRBR | 6260 | 626.40 | 630.55 | | 630.98 | 0.002908 | 5.30 | 1221.80 | 433.33 | 0.50 |
| Trib | 4745 | 50-YR | EX | 5021 | 625.80 | 629.62 | | 629.94 | 0.002302 | 4.54 | 1142.97 | 438.47 | 0.44 |
| Trib | 4745 | 50-YR | PRBR | 5021 | 625.80 | 629.62 | | 629.94 | 0.002305 | 4.54 | 1142.46 | 438.34 | 0.44 |
| Trib | 4745 | 100-YR | EX | 6260 | 625.80 | 630.10 | | 630.46 | 0.002217 | 4.87 | 1366.59 | 495.39 | 0.44 |
| Trib | 4745 | 100-YR | PRBR | 6260 | 625.80 | 630.10 | | 630.46 | 0.002217 | 4.87 | 1366.47 | 495.36 | 0.44 |
| Trib | 4533 | 50-YR | EX | 5021 | 624.89 | 629.15 | | 629.47 | 0.002156 | 4.79 | 1242.52 | 483.23 | 0.43 |
| Trib | 4533 | 50-YR | PRBR | 5021 | 624.89 | 629.15 | | 629.46 | 0.002161 | 4.79 | 1241.46 | 483.16 | 0.43 |
| Trib | 4533 | 100-YR | EX | 6260 | 624.89 | 629.68 | | 630.01 | 0.001965 | 4.99 | 1502.04 | 499.12 | 0.42 |
| Trib | 4533 | 100-YR | PRBR | 6260 | 624.89 | 629.68 | | 630.01 | 0.001966 | 4.99 | 1501.85 | 499.11 | 0.42 |
| Trib | 4333 | 50-YR | EX | 5021 | 624.21 | 628.14 | | 628.81 | 0.004762 | 6.58 | 777.79 | 268.30 | 0.63 |
| Trib | 4333 | 50-YR | PRBR | 5021 | 624.21 | 628.14 | | 628.81 | 0.004806 | 6.60 | 775.40 | 267.99 | 0.63 |
| Trib | 4333 | 100-YR | EX | 6260 | 624.21 | 628.58 | | 629.38 | 0.004866 | 7.21 | 897.49 | 283.31 | 0.65 |
| Trib | 4333 | 100-YR | PRBR | 6260 | 624.21 | 628.58 | | 629.38 | 0.004872 | 7.22 | 897.13 | 283.26 | 0.65 |
| Trib | 4125 | 50-YR | EX | 5021 | 623.44 | 627.50 | | 627.96 | 0.003104 | 5.46 | 937.44 | 300.44 | 0.51 |
| Trib | 4125 | 50-YR | PRBR | 5021 | 623.44 | 627.47 | | 627.94 | 0.003180 | 5.50 | 929.92 | 298.98 | 0.52 |
| Trib | 4125 | 100-YR | EX | 6260 | 623.44 | 627.92 | | 628.48 | 0.003259 | 6.04 | 1070.26 | 324.35 | 0.54 |
| Trib | 4125 | 100-YR | PRBR | 6260 | 623.44 | 627.92 | | 628.48 | 0.003268 | 6.04 | 1069.23 | 324.18 | 0.54 |
| Trib | 3928 | 50-YR | EX | 5021 | 623.23 | 627.03 | | 627.38 | 0.002479 | 4.80 | 1061.52 | 332.55 | 0.46 |
| Trib | 3928 | 50-YR | PRBR | 5021 | 623.23 | 626.98 | | 627.34 | 0.002600 | 4.87 | 1045.59 | 331.56 | 0.47 |
| Trib | 3928 | 100-YR | EX | 6260 | 623.23 | 627.43 | | 627.87 | 0.002630 | 5.33 | 1198.65 | 341.02 | 0.48 |
| Trib | 3928 | 100-YR | PRBR | 6260 | 623.23 | 627.43 | | 627.87 | 0.002643 | 5.34 | 1196.71 | 340.90 | 0.48 |
| Trib | 3720 | 50-YR | EX | 5021 | 622.63 | 626.63 | | 626.91 | 0.001902 | 4.30 | 1188.94 | 360.67 | 0.40 |
| Trib | 3720 | 50-YR | PRBR | 5021 | 622.63 | 626.55 | | 626.85 | 0.002056 | 4.40 | 1160.23 | 359.31 | 0.42 |
| Trib | 3720 | 100-YR | EX | 6260 | 622.63 | 627.00 | | 627.36 | 0.002099 | 4.83 | 1325.56 | 367.96 | 0.43 |
| Trib | 3720 | 100-YR | PRBR | 6260 | 622.63 | 626.99 | | 627.35 | 0.002116 | 4.84 | 1322.17 | 367.76 | 0.43 |
| Trib | 3533 | 50-YR | EX | 5021 | 622.42 | 626.38 | | 626.58 | 0.001407 | 3.83 | 1512.73 | 559.00 | 0.35 |
| Trib | 3533 | 50-YR | PRBR | 5021 | 622.42 | 626.27 | | 626.49 | 0.001588 | 3.98 | 1448.83 | 552.62 | 0.37 |
| Trib | 3533 | 100-YR | EX | 6260 | 622.42 | 626.75 | | 627.00 | 0.001510 | 4.23 | 1724.12 | 577.78 | 0.37 |
| Trib | 3533 | 100-YR | PRBR | 6260 | 622.42 | 626.74 | | 626.99 | 0.001529 | 4.24 | 1716.65 | 577.17 | 0.37 |
| Trib | 3329 | 50-YR | EX | 5021 | 621.25 | 625.99 | 624.54 | 626.28 | 0.001515 | 4.45 | 1270.68 | 543.66 | 0.42 |
| Trib | 3329 | 50-YR | PRBR | 5021 | 621.25 | 625.60 | 624.55 | 626.02 | 0.002492 | 5.27 | 973.07 | 506.60 | 0.53 |
| Trib | 3329 | 100-YR | EX | 6260 | 621.25 | 626.30 | 624.90 | 626.66 | 0.001701 | 4.99 | 1446.38 | 589.76 | 0.45 |
| Trib | 3329 | 100-YR | PRBR | 6260 | 621.25 | 626.23 | 624.89 | 626.60 | 0.001824 | 5.10 | 1405.46 | 575.85 | 0.46 |
| Trib | 3296 | | | Bridge | | | | | | | | | |
| Trib | 3251 | 50-YR | EX | 5021 | 619.25 | 624.15 | | 624.69 | 0.004690 | 7.12 | 999.54 | 570.09 | 0.72 |
| Trib | 3251 | 50-YR | PRBR | 5021 | 619.25 | 624.19 | 624.19 | 625.24 | 0.007480 | 9.07 | 666.98 | 576.02 | 0.91 |
| Trib | 3251 | 100-YR | EX | 6260 | 619.25 | 624.49 | | 625.06 | 0.004430 | 7.43 | 1199.76 | 601.56 | 0.71 |
| Trib | 3251 | 100-YR | PRBR | 6260 | 619.25 | 624.53 | 624.53 | 625.75 | 0.007548 | 9.78 | 770.12 | 604.87 | 0.93 |
| Trib | 3050 | 50-YR | EX | 5021 | 619.11 | 623.61 | | 623.95 | 0.002560 | 5.82 | 1227.97 | 569.90 | 0.55 |
| Trib | 3050 | 50-YR | PRBR | 5021 | 619.11 | 623.61 | | 623.95 | 0.002560 | 5.82 | 1227.97 | 569.90 | 0.55 |
| Trib | 3050 | 100-YR | EX | 6260 | 619.11 | 623.95 | | 624.33 | 0.002604 | 6.24 | 1426.26 | 594.31 | 0.56 |
| Trib | 3050 | 100-YR | PRBR | 6260 | 619.11 | 623.95 | | 624.33 | 0.002604 | 6.24 | 1426.26 | 594.31 | 0.56 |
| Trib | 2842 | 50-YR | EX | 5021 | 618.69 | 622.21 | 622.20 | 623.04 | 0.007879 | 8.20 | 788.35 | 486.92 | 0.91 |
| Trib | 2842 | 50-YR | PRBR | 5021 | 618.69 | 622.21 | 622.20 | 623.04 | 0.007879 | 8.20 | 788.35 | 486.92 | 0.91 |
| Trib | 2842 | 100-YR | EX | 6260 | 618.69 | 622.51 | 622.49 | 623.42 | 0.007676 | 8.72 | 939.36 | 522.44 | 0.91 |
| Trib | 2842 | 100-YR | PRBR | 6260 | 618.69 | 622.51 | 622.49 | 623.42 | 0.007676 | 8.72 | 939.36 | 522.44 | 0.91 |
| Trib | 2637 | 50-YR | EX | 5021 | 618.12 | 621.41 | | 621.81 | 0.003859 | 6.09 | 1069.82 | 541.42 | 0.64 |
| Trib | 2637 | 50-YR | PRBR | 5021 | 618.12 | 621.41 | | 621.81 | 0.003859 | 6.09 | 1069.82 | 541.42 | 0.64 |
| Trib | 2637 | 100-YR | EX | 6260 | 618.12 | 621.71 | | 622.18 | 0.004004 | 6.64 | 1233.78 | 564.70 | 0.67 |
| Trib | 2637 | 100-YR | PRBR | 6260 | 618.12 | 621.71 | | 622.18 | 0.004004 | 6.64 | 1233.78 | 564.70 | 0.67 |
| Trib | 2425 | 50-YR | EX | 5021 | 617.81 | 620.61 | | 621.00 | 0.003778 | 5.13 | 1060.32 | 605.39 | 0.61 |
| Trib | 2425 | 50-YR | PRBR | 5021 | 617.81 | 620.61 | | 621.00 | 0.003778 | 5.13 | 1060.32 | 605.39 | 0.61 |
| Trib | 2425 | 100-YR | EX | 6260 | 617.81 | 620.95 | | 621.37 | 0.003492 | 5.42 | 1268.73 | 635.13 | 0.60 |
| Trib | 2425 | 100-YR | PRBR | 6260 | 617.81 | 620.95 | | 621.37 | 0.003493 | 5.42 | 1268.69 | 635.13 | 0.60 |
| Trib | 2217 | 50-YR | EX | 5021 | 616.95 | 619.99 | 619.10 | 620.34 | 0.002602 | 4.83 | 1097.70 | 524.03 | 0.52 |
| Trib | 2217 | 50-YR | PRBR | 5021 | 616.95 | 619.99 | 619.10 | 620.34 | 0.002602 | 4.83 | 1097.70 | 524.03 | 0.52 |
| Trib | 2217 | 100-YR | EX | 6260 | 616.95 | 620.34 | 619.37 | 620.75 | 0.002600 | 5.24 | 1282.59 | 548.21 | 0.53 |
| Trib | 2217 | 100-YR | PRBR | 6260 | 616.95 | 620.34 | 619.37 | 620.75 | 0.002600 | 5.24 | 1282.59 | 548.21 | 0.53 |



NOTES:
 1. DATA PRESENTED FROM DRAINAGE SUMMARY FOR KLEIN ROAD PREPARED BY PAPE-DAWSON ENGINEERS. DATED JULY 2018.
 2. GUADALUPE TRIBUTARY 22 IS IDENTIFIED ON FEMA FIRM PANEL 48187C0115F, DATED NOVEMBER 2, 2007. THE UPSTREAM/DOWNSTREAM AREA AND EXISTING CROSSING ARE WITHIN A ZONE "A".

HYDRAULIC METHOD
 WATER SURFACE ELEVATIONS COMPUTED USING A HEC-RAS (V.5.0.3) MODEL CREATED FOR GUADALUPE TRIBUTARY 22.
 FILE NAME: "5103002_KLEINRD.PRJ"
 EFFECTIVE AND PROPOSED MODELS WERE DEVELOPED USING LIDAR DATA AND FIELD DATA.
 EFFECTIVE CONDITION WATER SURFACE ELEVATIONS COMPUTED FROM HEC-RAS MODEL PLAN "EXISTING" NAMED "5103002_KLEINRD.P01".
 PROPOSED CONDITION WATER SURFACE ELEVATIONS COMPUTED FROM HEC-RAS MODEL PLAN "PROP BRIDGE" NAMED "5103002_KLEINRD.P02".

HYDROLOGIC METHOD
 FLOWS USED FOR MODELS WERE CALCULATED FROM THE SCS HYDROGRAPH METHOD AND INFORMATION FROM THE CITY OF NEW BRAUNFELS - DRAINAGE AND EROSION CONTROL DESIGN MANUAL.

| REV. NO. | DATE | DESCRIPTION | BY |
|----------|------|-------------|----|
| | | | |
| | | | |

PAPE-DAWSON ENGINEERS
 SAN ANTONIO | AUSTIN | HOUSTON | FORT WORTH | DALLAS
 2000 NW LOOP 410 | SAN ANTONIO, TX 78213 | 210.375.9000
 TBPE FIRM REGISTRATION #470 | TPLS FIRM REGISTRATION #10028800

**KLEIN ROAD
 PROPOSED BRIDGE
 HYDRAULIC DATA
 SHEET**

SHEET 3 OF 4

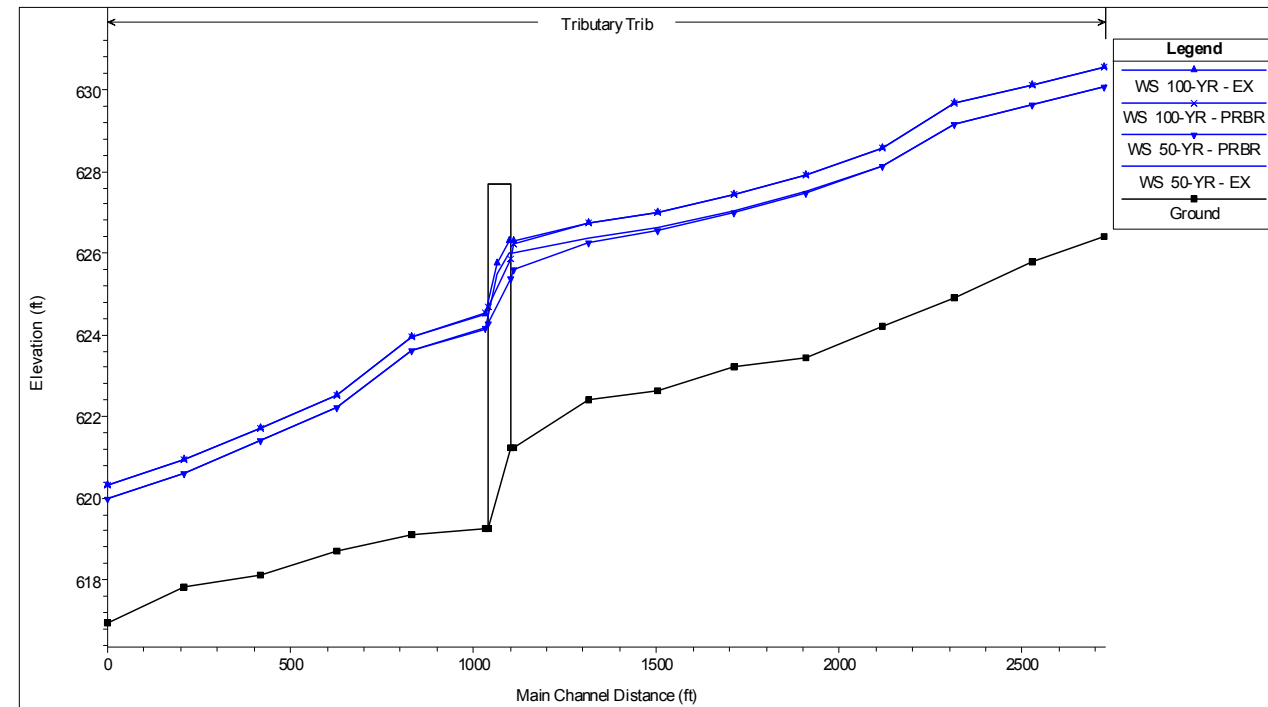
Plotted on: 7/30/2018

Design File name: \\pape-dawson\pd\h\projects\5103002\des\civil\Drainage\5103002\hds03.dgn

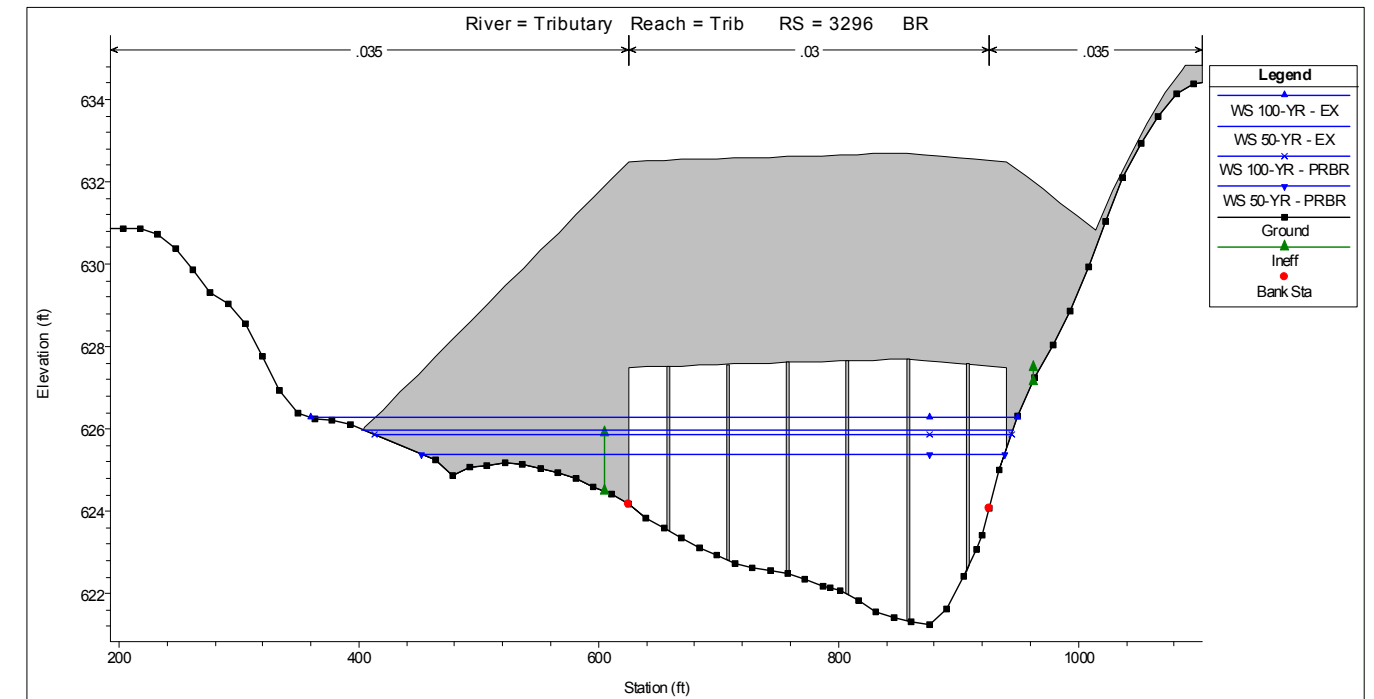
Plotted on: 7/30/2018

Design File Name: \\pape-dawson\pd\h\projects\10\30\02\des\civi\Drainage\5103002\hds04.dgn

HEC-RAS CHANNEL PROFILE



HEC-RAS BRIDGE UPSTREAM



HEC-RAS BRIDGE OUTPUT

| Plan: PRBR Tributary Trib RS: 3296 Profile: 50-YR | | Element | | |
|---|-------------|------------------------|--------------|----------|
| E.G. US. (ft) | 626.02 | Inside BR US | Inside BR DS | |
| W.S. US. (ft) | 625.60 | E.G. Elev (ft) | 625.95 | 625.42 |
| Q Total (cfs) | 5021.00 | W.S. Elev (ft) | 625.38 | 624.29 |
| Q Bridge (cfs) | 5021.00 | Crit W.S. (ft) | 624.61 | 624.29 |
| Q Weir (cfs) | | Max Chl Dpth (ft) | 4.13 | 5.04 |
| Weir Sta Lft (ft) | | Vel Total (ft/s) | 6.00 | 7.94 |
| Weir Sta Rgt (ft) | | Flow Area (sq ft) | 837.34 | 632.67 |
| Weir Submerg | | Froude # Chl | 0.52 | 0.67 |
| Weir Max Depth (ft) | | Specif Force (cu ft) | 2238.57 | 2216.99 |
| Min El Weir Flow (ft) | 625.98 | Hydr Depth (ft) | 2.80 | 2.38 |
| Min El Prs (ft) | 627.70 | W.P. Total (ft) | 335.09 | 293.46 |
| Delta EG (ft) | 0.78 | Conv. Total (cfs) | 77412.00 | 52759.20 |
| Delta WS (ft) | 1.41 | Top Width (ft) | 298.62 | 266.07 |
| BR Open Area (sq ft) | 1501.84 | Frctn Loss (ft) | 0.36 | |
| BR Open Vel (ft/s) | 7.94 | C & E Loss (ft) | 0.17 | |
| BR Sluice Coef | | Shear Total (lb/sq ft) | 0.66 | 1.22 |
| BR Sel Method | Energy only | Power Total (lb/ft s) | 3.94 | 9.67 |

| Plan: PRBR Tributary Trib RS: 3296 Profile: 100-YR | | Element | | |
|--|-------------|------------------------|--------------|----------|
| E.G. US. (ft) | 626.60 | Inside BR US | Inside BR DS | |
| W.S. US. (ft) | 626.23 | E.G. Elev (ft) | 626.50 | 625.96 |
| Q Total (cfs) | 6260.00 | W.S. Elev (ft) | 625.85 | 624.67 |
| Q Bridge (cfs) | 6260.00 | Crit W.S. (ft) | 624.95 | 624.67 |
| Q Weir (cfs) | | Max Chl Dpth (ft) | 4.60 | 5.42 |
| Weir Sta Lft (ft) | | Vel Total (ft/s) | 6.40 | 8.52 |
| Weir Sta Rgt (ft) | | Flow Area (sq ft) | 978.15 | 735.07 |
| Weir Submerg | | Froude # Chl | 0.53 | 0.69 |
| Weir Max Depth (ft) | | Specif Force (cu ft) | 2976.60 | 2909.61 |
| Min El Weir Flow (ft) | 625.98 | Hydr Depth (ft) | 3.26 | 2.71 |
| Min El Prs (ft) | 627.70 | W.P. Total (ft) | 342.96 | 302.41 |
| Delta EG (ft) | 0.86 | Conv. Total (cfs) | 98459.00 | 65547.20 |
| Delta WS (ft) | 1.70 | Top Width (ft) | 300.03 | 270.81 |
| BR Open Area (sq ft) | 1501.84 | Frctn Loss (ft) | 0.35 | |
| BR Open Vel (ft/s) | 8.52 | C & E Loss (ft) | 0.19 | |
| BR Sluice Coef | | Shear Total (lb/sq ft) | 0.72 | 1.38 |
| BR Sel Method | Energy only | Power Total (lb/ft s) | 4.61 | 11.79 |

NOTES:

1. DATA PRESENTED FROM DRAINAGE SUMMARY FOR KLEIN ROAD PREPARED BY PAPE-DAWSON ENGINEERS. DATED JULY 2018.

2. GUADALUPE TRIBUTARY 22 IS IDENTIFIED ON FEMA FIRM PANEL 48187C0115F, DATED NOVEMBER 2, 2007. THE UPSTREAM/DOWNSTREAM AREA AND EXISTING CROSSING ARE WITHIN A ZONE "A".

HYDRAULIC METHOD

WATER SURFACE ELEVATIONS COMPUTED USING A HEC-RAS (V.5.0.3) MODEL CREATED FOR GUADALUPE TRIBUTARY 22. FILE NAME: "5103002_KLEINRD.PRJ"

EFFECTIVE AND PROPOSED MODELS WERE DEVELOPED USING LIDAR DATA AND FIELD DATA.


EFFECTIVE CONDITION WATER SURFACE ELEVATIONS COMPUTED FROM HEC-RAS MODEL PLAN "EXISTING" NAMED "5103002_KLEINRD.P01".

PROPOSED CONDITION WATER SURFACE ELEVATIONS COMPUTED FROM HEC-RAS MODEL PLAN "PROP BRIDGE" NAMED "5103002_KLEINRD.P02".

HYDROLOGIC METHOD

FLows USED FOR MODELS WERE CALCULATED FROM THE SCS HYDROGRAPH METHOD AND INFORMATION FROM THE CITY OF NEW BRAUNFELS - DRAINAGE AND EROSION CONTROL DESIGN MANUAL.

| REV. NO. | DATE | DESCRIPTION | BY |
|----------|------|-------------|----|
| | | | |
| | | | |
| | | | |



SAN ANTONIO | AUSTIN | HOUSTON | FORT WORTH | DALLAS
2000 NW LOOP 410 | SAN ANTONIO, TX 78213 | 210.375.9000
TBPE FIRM REGISTRATION #470 | TBPLS FIRM REGISTRATION #10028800

KLEIN ROAD PROPOSED BRIDGE HYDRAULIC DATA SHEET

SHEET 4 OF 4

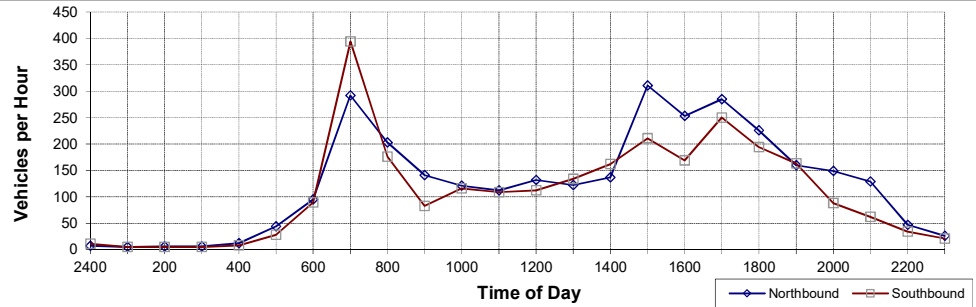
APPENDIX C1

Average Daily Traffic

Project No. : 51030-01
 Station No. :
 Counter No. : 1

Location: Klein Rd, N of Walnut Ave
 City/State: New Braunfels, TX
 Date: May 22, 2018
 Day of Week: Tuesday

Site:



| Time | Peak | Northbound | Southbound | Time | Peak | Northbound | Southbound |
|--------------|------|-------------|------------|---------------------|------|-----------------------|------------|
| | | TMC | TMC | | | TMC | TMC |
| 24:00 | | 1 | 2 | 12:00 | | 35 | 29 |
| 0:15 | | 4 | 4 | 12:15 | | 37 | 27 |
| 0:30 | | 0 | 2 | 12:30 | | 22 | 22 |
| 0:45 | | 2 | 3 | 12:45 | | 38 | 34 |
| 1:00 | | 4 | 1 | 13:00 | | 28 | 34 |
| 1:15 | | 1 | 0 | 13:15 | | 33 | 23 |
| 1:30 | | 0 | 0 | 13:30 | | 28 | 33 |
| 1:45 | | 0 | 4 | 13:45 | | 33 | 44 |
| 2:00 | | 3 | 0 | 14:00 | * | 24 | 29 |
| 2:15 | | 1 | 2 | 14:15 | * | 32 | 29 |
| 2:30 | | 2 | 3 | 14:30 | * | 30 | 38 |
| 2:45 | | 0 | 0 | 14:45 | * | 51 | 66 |
| 3:00 | | 2 | 1 | 15:00 | | 100 | 59 |
| 3:15 | | 1 | 1 | 15:15 | | 47 | 51 |
| 3:30 | | 3 | 1 | 15:30 | | 53 | 50 |
| 3:45 | | 0 | 2 | 15:45 | | 111 | 51 |
| 4:00 | | 3 | 1 | 16:00 | | 70 | 62 |
| 4:15 | | 1 | 3 | 16:15 | | 66 | 30 |
| 4:30 | | 2 | 2 | 16:30 | | 58 | 47 |
| 4:45 | | 6 | 2 | 16:45 | | 59 | 30 |
| 5:00 | | 4 | 5 | 17:00 | | 68 | 47 |
| 5:15 | | 11 | 3 | 17:15 | * | 85 | 60 |
| 5:30 | | 18 | 11 | 17:30 | * | 56 | 57 |
| 5:45 | | 11 | 9 | 17:45 | * | 76 | 86 |
| 6:00 | | 16 | 13 | 18:00 | * | 60 | 74 |
| 6:15 | | 20 | 11 | 18:15 | | 69 | 45 |
| 6:30 | | 25 | 23 | 18:30 | | 47 | 39 |
| 6:45 | | 34 | 42 | 18:45 | | 50 | 36 |
| 7:00 | | 45 | 57 | 19:00 | | 48 | 51 |
| 7:15 | * | 72 | 136 | 19:15 | | 42 | 42 |
| 7:30 | * | 110 | 131 | 19:30 | | 31 | 38 |
| 7:45 | * | 65 | 70 | 19:45 | | 39 | 32 |
| 8:00 | * | 75 | 86 | 20:00 | | 24 | 21 |
| 8:15 | | 64 | 30 | 20:15 | | 32 | 21 |
| 8:30 | | 29 | 29 | 20:30 | | 32 | 25 |
| 8:45 | | 35 | 31 | 20:45 | | 61 | 21 |
| 9:00 | | 37 | 20 | 21:00 | | 71 | 17 |
| 9:15 | | 32 | 25 | 21:15 | | 16 | 16 |
| 9:30 | | 46 | 18 | 21:30 | | 23 | 17 |
| 9:45 | | 26 | 20 | 21:45 | | 19 | 12 |
| 10:00 | | 19 | 28 | 22:00 | | 12 | 11 |
| 10:15 | | 42 | 23 | 22:15 | | 18 | 10 |
| 10:30 | | 35 | 36 | 22:30 | | 8 | 8 |
| 10:45 | | 25 | 29 | 22:45 | | 9 | 5 |
| 11:00 | | 26 | 25 | 23:00 | | 9 | 6 |
| 11:15 | | 24 | 30 | 23:15 | | 10 | 5 |
| 11:30 | | 32 | 27 | 23:30 | | 2 | 4 |
| 11:45 | | 30 | 27 | 23:45 | | 5 | 6 |
| AM Peak Hour | | 7:15-8:15 | | Directional Volumes | | 3,021 | 2,629 |
| % of ADT | | 13.2% | | | | 24-Hour Volume | 5,650 |
| PM Peak Hour | | 17:15-18:15 | | | | | |
| % of ADT | | 9.8% | | | | | |

APPENDIX C2

| | | | | | | | | | | | | |
|---------------------------------------|-------------------|----------------|--------------|----------------------|----------------|------------------|--|----------------|--------------|------------------|----------------|--------------|
| North/South Street: Klein Rd | | | | | | | | | | | | |
| East/West Street: Walnut Ave / | | | | | | | | | | | | |
| TOD: | AM | Date: | 22-May-18 | Synchro Node: | 1 | Raw Data: | H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | Walnut Ave | | | | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 7:00 AM | 9 | 45 | 0 | 0 | 56 | 8 | 8 | 0 | 13 | 0 | 0 | 0 |
| 7:15 AM | 25 | 69 | 0 | 0 | 124 | 32 | 13 | 0 | 26 | 0 | 0 | 0 |
| 7:30 AM | 40 | 86 | 0 | 0 | 83 | 25 | 11 | 0 | 45 | 0 | 0 | 0 |
| 7:45 AM | 55 | 43 | 0 | 0 | 62 | 22 | 10 | 0 | 48 | 0 | 0 | 0 |
| 8:00 AM | 48 | 70 | 0 | 0 | 49 | 9 | 4 | 0 | 40 | 0 | 0 | 0 |
| 8:15 AM | 29 | 46 | 0 | 0 | 12 | 8 | 5 | 0 | 14 | 0 | 0 | 0 |
| 8:30 AM | 13 | 18 | 0 | 0 | 14 | 13 | 8 | 0 | 8 | 0 | 0 | 0 |
| 8:45 AM | 8 | 26 | 0 | 0 | 13 | 7 | 9 | 0 | 10 | 0 | 0 | 0 |
| Total | 227 | 403 | 0 | 0 | 413 | 124 | 68 | 0 | 204 | 0 | 0 | 0 |
| Peak Hour | 168 | 268 | 0 | 0 | 318 | 88 | 38 | 0 | 159 | 0 | 0 | 0 |

| Pedestrians | | | | |
|--------------------|-----------|-----------|-----------|-----------|
| | NB | SB | EB | WB |
| 7:00 AM | | | | |
| 7:15 AM | | | | |
| 7:30 AM | | | | |
| 7:45 AM | | | | |
| 8:00 AM | | | | |
| 8:15 AM | | | | |
| 8:30 AM | | | | |
| 8:45 AM | | | | |

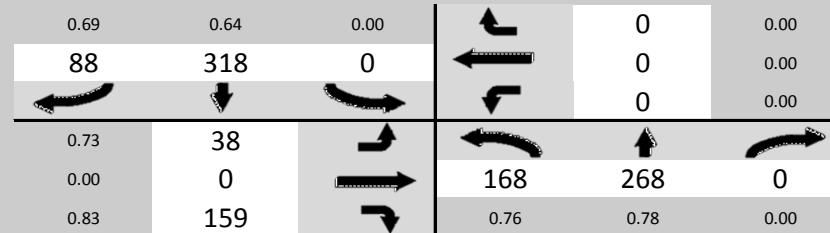


Diagram for: Peak Hour
Peak Hour: 07:15 AM-08:15 AM



| | | | | | | | | | | | | |
|---------------------------------------|---------------|----------------|--------------|-------------|----------------------|--|-------------|----------------|--------------|-------------|----------------|--------------|
| North/South Street: Klein Rd | | | | | | | | | | | | |
| East/West Street: Walnut Ave / | | | | | | | | | | | | |
| TOD: | Midday | Date: | 22-May-18 | | Synchro Node: | 1 Raw Data: H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | Walnut Ave | | | | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 11:00 AM | 15 | 14 | 0 | 0 | 18 | 6 | 8 | 0 | 8 | 0 | 0 | 0 |
| 11:15 AM | 9 | 14 | 0 | 0 | 16 | 3 | 15 | 0 | 17 | 0 | 0 | 0 |
| 11:30 AM | 13 | 13 | 0 | 0 | 13 | 12 | 9 | 0 | 16 | 0 | 0 | 0 |
| 11:45 AM | 17 | 21 | 0 | 0 | 13 | 8 | 10 | 0 | 6 | 0 | 0 | 0 |
| 12:00 PM | 13 | 22 | 0 | 0 | 19 | 14 | 10 | 0 | 12 | 0 | 0 | 0 |
| 12:15 PM | 8 | 17 | 0 | 0 | 11 | 11 | 13 | 0 | 8 | 0 | 0 | 0 |
| 12:30 PM | 9 | 18 | 0 | 0 | 12 | 10 | 4 | 0 | 11 | 0 | 0 | 0 |
| 12:45 PM | 4 | 25 | 0 | 0 | 26 | 5 | 10 | 0 | 14 | 0 | 0 | 0 |
| Total | 88 | 144 | 0 | 0 | 128 | 69 | 79 | 0 | 92 | 0 | 0 | 0 |
| Peak Hour | 52 | 70 | 0 | 0 | 61 | 37 | 44 | 0 | 51 | 0 | 0 | 0 |

| Pedestrians | | | | |
|-------------|----|----|----|----|
| | NB | SB | EB | WB |
| 11:00 AM | | | | |
| 11:15 AM | | | | |
| 11:30 AM | | | | |
| 11:45 AM | | | | |
| 12:00 PM | | | | |
| 12:15 PM | | | | |
| 12:30 PM | | | | |
| 12:45 PM | | | | |

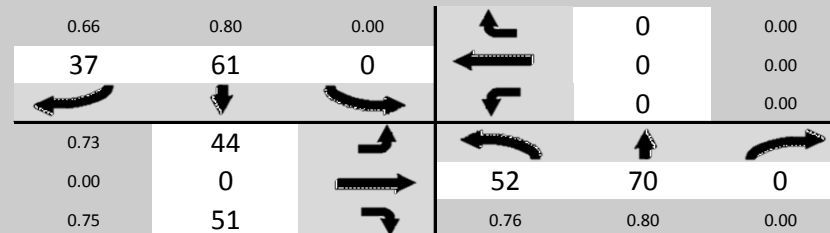


Diagram for: Peak Hour
Peak Hour: 11:15 AM-12:15 PM



| | | | | | | | | | | | | |
|---------------------------------------|-------------------|----------------|--------------|----------------------|----------------|------------------|--|----------------|--------------|------------------|----------------|--------------|
| North/South Street: Klein Rd | | | | | | | | | | | | |
| East/West Street: Walnut Ave / | | | | | | | | | | | | |
| TOD: | PM | Date: | 22-May-18 | Synchro Node: | 1 | Raw Data: | H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | Walnut Ave | | | | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 4:00 PM | 31 | 40 | 0 | 0 | 37 | 16 | 25 | 0 | 28 | 0 | 0 | 0 |
| 4:15 PM | 19 | 28 | 0 | 0 | 24 | 12 | 26 | 0 | 16 | 0 | 0 | 0 |
| 4:30 PM | 16 | 26 | 0 | 0 | 23 | 12 | 34 | 0 | 30 | 0 | 0 | 0 |
| 4:45 PM | 12 | 29 | 0 | 0 | 19 | 13 | 23 | 0 | 16 | 0 | 0 | 0 |
| 5:00 PM | 15 | 34 | 0 | 0 | 30 | 16 | 41 | 0 | 19 | 0 | 0 | 0 |
| 5:15 PM | 11 | 32 | 0 | 0 | 35 | 22 | 32 | 0 | 23 | 0 | 0 | 0 |
| 5:30 PM | 15 | 28 | 0 | 0 | 45 | 22 | 30 | 0 | 27 | 0 | 0 | 0 |
| 5:45 PM | 13 | 33 | 0 | 0 | 64 | 13 | 35 | 0 | 62 | 0 | 0 | 0 |
| Total | 132 | 250 | 0 | 0 | 277 | 126 | 246 | 0 | 221 | 0 | 0 | 0 |
| Peak Hour | 54 | 127 | 0 | 0 | 174 | 73 | 138 | 0 | 131 | 0 | 0 | 0 |

| Pedestrians | | | | |
|--------------------|-----------|-----------|-----------|-----------|
| | NB | SB | EB | WB |
| 4:00 PM | | | | |
| 4:15 PM | | | | |
| 4:30 PM | | | | |
| 4:45 PM | | | | |
| 5:00 PM | | | | |
| 5:15 PM | | | | |
| 5:30 PM | | | | |
| 5:45 PM | | | | |

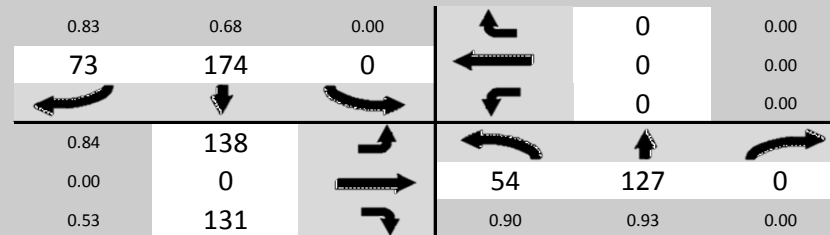


Diagram for: Peak Hour
Peak Hour: 05:00 PM-06:00 PM



| | | | | | | | | | | | | |
|--|-------------------|----------------|--------------|----------------------|----------------|------------------|--|----------------|--------------|------------------|----------------|--------------|
| North/South Street: Klein Rd | | | | | | | | | | | | |
| East/West Street: Roadrunner Ave / Stoeger Dr | | | | | | | | | | | | |
| TOD: | AM | Date: | 22-May-18 | Synchro Node: | 2 | Raw Data: | H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | Roadrunner Ave | | | Stoeger Dr | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 7:00 AM | 0 | 59 | 0 | 1 | 47 | 0 | 8 | 0 | 2 | 0 | 0 | 10 |
| 7:15 AM | 1 | 68 | 1 | 0 | 93 | 0 | 9 | 0 | 4 | 3 | 0 | 12 |
| 7:30 AM | 1 | 104 | 2 | 1 | 99 | 1 | 4 | 0 | 3 | 1 | 0 | 6 |
| 7:45 AM | 2 | 76 | 0 | 5 | 62 | 2 | 12 | 0 | 5 | 3 | 0 | 4 |
| 8:00 AM | 3 | 79 | 1 | 3 | 61 | 2 | 8 | 0 | 1 | 0 | 0 | 2 |
| 8:15 AM | 1 | 76 | 0 | 4 | 25 | 4 | 8 | 0 | 0 | 0 | 0 | 2 |
| 8:30 AM | 0 | 35 | 0 | 1 | 24 | 3 | 3 | 0 | 1 | 0 | 0 | 6 |
| 8:45 AM | 0 | 34 | 0 | 3 | 26 | 2 | 7 | 0 | 0 | 0 | 0 | 1 |
| Total | 8 | 531 | 4 | 18 | 437 | 14 | 59 | 0 | 16 | 7 | 0 | 43 |
| Peak Hour | 7 | 327 | 4 | 9 | 315 | 5 | 33 | 0 | 13 | 7 | 0 | 24 |

| Pedestrians | | | | |
|--------------------|-----------|-----------|-----------|-----------|
| | NB | SB | EB | WB |
| 7:00 AM | | | | |
| 7:15 AM | | | | |
| 7:30 AM | | | | |
| 7:45 AM | | | | |
| 8:00 AM | | | | |
| 8:15 AM | | | | |
| 8:30 AM | | | | |
| 8:45 AM | | | | |

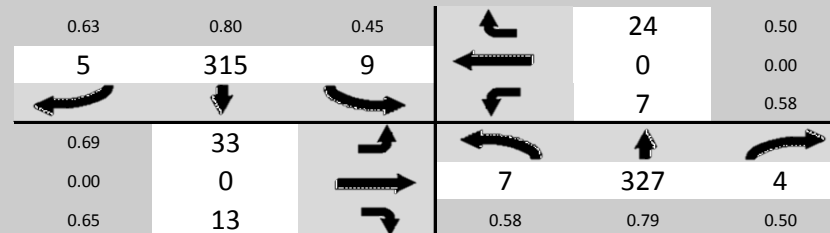


Diagram for: Peak Hour
Peak Hour: 07:15 AM-08:15 AM



| | | | | | | | | | | | | |
|--|-------------------|----------------|--------------|----------------------|----------------|------------------|--|----------------|--------------|------------------|----------------|--------------|
| North/South Street: Klein Rd | | | | | | | | | | | | |
| East/West Street: Roadrunner Ave / Stoeger Dr | | | | | | | | | | | | |
| TOD: | Midday | Date: | 22-May-18 | Synchro Node: | 2 | Raw Data: | H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | Roadrunner Ave | | | Stoeger Dr | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 11:00 AM | 0 | 33 | 0 | 2 | 19 | 0 | 4 | 0 | 0 | 0 | 0 | 2 |
| 11:15 AM | 0 | 24 | 1 | 0 | 18 | 1 | 3 | 0 | 0 | 0 | 0 | 1 |
| 11:30 AM | 0 | 29 | 0 | 2 | 23 | 4 | 2 | 0 | 1 | 2 | 0 | 6 |
| 11:45 AM | 1 | 28 | 1 | 1 | 28 | 1 | 3 | 0 | 0 | 0 | 0 | 2 |
| 12:00 PM | 2 | 25 | 0 | 2 | 30 | 1 | 3 | 1 | 0 | 0 | 0 | 3 |
| 12:15 PM | 1 | 29 | 1 | 2 | 26 | 3 | 1 | 0 | 1 | 0 | 0 | 6 |
| 12:30 PM | 0 | 21 | 0 | 3 | 17 | 0 | 5 | 0 | 1 | 0 | 0 | 3 |
| 12:45 PM | 0 | 42 | 1 | 1 | 29 | 2 | 2 | 0 | 0 | 1 | 1 | 2 |
| Total | 4 | 231 | 4 | 13 | 190 | 12 | 23 | 1 | 3 | 3 | 1 | 25 |
| Peak Hour | 4 | 111 | 2 | 7 | 107 | 9 | 9 | 1 | 2 | 2 | 0 | 17 |

| Pedestrians | | | | |
|--------------------|-----------|-----------|-----------|-----------|
| | NB | SB | EB | WB |
| 11:00 AM | | | | |
| 11:15 AM | | | | |
| 11:30 AM | | | | |
| 11:45 AM | | | | |
| 12:00 PM | | | | |
| 12:15 PM | | | | |
| 12:30 PM | | | | |
| 12:45 PM | | | | |

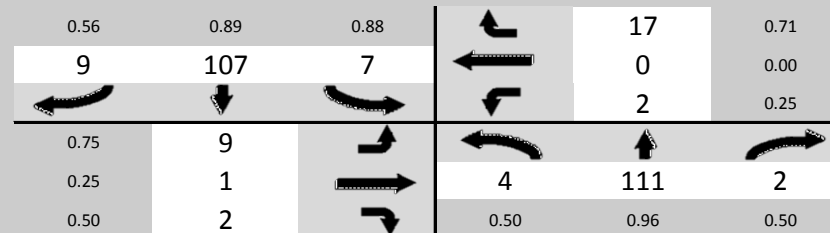


Diagram for: Peak Hour
Peak Hour: 11:30 AM-12:30 PM



| | | | | | | | | | | | | | |
|----------------------------|-------------------|------------------------------------|--------------|-------------------|----------------|----------------------|------------------|----------------|------------------|--|----------------|--------------|--|
| North/South Street: | | Klein Rd | | | | | | | | | | | |
| East/West Street: | | Roadrunner Ave / Stoeger Dr | | | | | | | | | | | |
| TOD: | PM | Date: | 22-May-18 | | | Synchro Node: | 2 | | Raw Data: | H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | | |
| | Klein Rd | | | Klein Rd | | | Roadrunner Ave | | | Stoeger Dr | | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right | |
| 4:00 PM | 0 | 67 | 2 | 3 | 47 | 6 | 6 | 0 | 1 | 2 | 0 | 4 | |
| 4:15 PM | 5 | 61 | 0 | 5 | 40 | 6 | 5 | 0 | 0 | 1 | 0 | 1 | |
| 4:30 PM | 1 | 45 | 0 | 7 | 45 | 6 | 7 | 0 | 2 | 1 | 0 | 4 | |
| 4:45 PM | 1 | 47 | 0 | 6 | 40 | 6 | 5 | 0 | 1 | 0 | 0 | 2 | |
| 5:00 PM | 3 | 55 | 1 | 4 | 50 | 8 | 2 | 0 | 0 | 0 | 2 | 1 | |
| 5:15 PM | 4 | 61 | 0 | 6 | 68 | 3 | 3 | 0 | 1 | 0 | 0 | 2 | |
| 5:30 PM | 1 | 48 | 1 | 7 | 59 | 14 | 2 | 0 | 0 | 0 | 0 | 1 | |
| 5:45 PM | 1 | 55 | 1 | 5 | 92 | 11 | 4 | 0 | 7 | 0 | 0 | 3 | |
| Total | 16 | 439 | 5 | 43 | 441 | 60 | 34 | 0 | 12 | 4 | 2 | 18 | |
| Peak Hour | 9 | 219 | 3 | 22 | 269 | 36 | 11 | 0 | 8 | 0 | 2 | 7 | |

| Pedestrians | | | | |
|--------------------|-----------|-----------|-----------|-----------|
| | NB | SB | EB | WB |
| 4:00 PM | | | | |
| 4:15 PM | | | | |
| 4:30 PM | | | | |
| 4:45 PM | | | | |
| 5:00 PM | | | | |
| 5:15 PM | | | | |
| 5:30 PM | | | | |
| 5:45 PM | | | | |

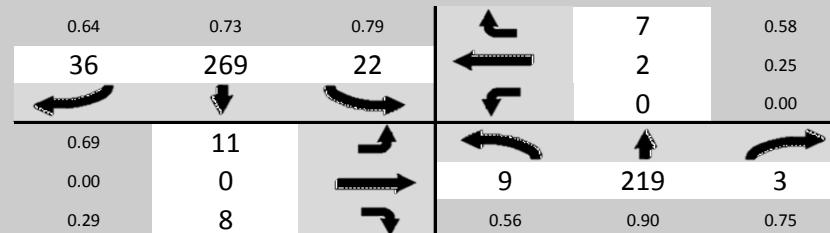


Diagram for: Peak Hour
Peak Hour: 05:00 PM-06:00 PM



| | | | | | | | | | | | | |
|---|-------------------|----------------|--------------|----------------------|----------------|------------------|--|----------------|--------------|------------------|----------------|--------------|
| North/South Street: Klein Rd | | | | | | | | | | | | |
| East/West Street: Dove Crossing Dr / | | | | | | | | | | | | |
| TOD: | AM | Date: | 22-May-18 | Synchro Node: | 3 | Raw Data: | H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | Dove Crossing Dr | | | | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 7:00 AM | 3 | 76 | 0 | 0 | 49 | 4 | 11 | 0 | 3 | 0 | 0 | 0 |
| 7:15 AM | 3 | 93 | 0 | 0 | 84 | 4 | 13 | 0 | 10 | 0 | 0 | 0 |
| 7:30 AM | 5 | 108 | 0 | 0 | 83 | 3 | 16 | 0 | 16 | 0 | 0 | 0 |
| 7:45 AM | 11 | 76 | 0 | 0 | 55 | 9 | 10 | 0 | 15 | 0 | 0 | 0 |
| 8:00 AM | 10 | 72 | 0 | 0 | 47 | 3 | 17 | 0 | 13 | 0 | 0 | 0 |
| 8:15 AM | 15 | 72 | 0 | 0 | 27 | 3 | 10 | 0 | 3 | 0 | 0 | 0 |
| 8:30 AM | 4 | 37 | 0 | 0 | 30 | 6 | 7 | 0 | 2 | 0 | 0 | 0 |
| 8:45 AM | 2 | 40 | 0 | 0 | 24 | 7 | 3 | 0 | 4 | 0 | 0 | 0 |
| Total | 53 | 574 | 0 | 0 | 399 | 39 | 87 | 0 | 66 | 0 | 0 | 0 |
| Peak Hour | 29 | 349 | 0 | 0 | 269 | 19 | 56 | 0 | 54 | 0 | 0 | 0 |

| Pedestrians | | | | |
|--------------------|-----------|-----------|-----------|-----------|
| | NB | SB | EB | WB |
| 7:00 AM | | | | |
| 7:15 AM | | | | |
| 7:30 AM | | | | |
| 7:45 AM | | | | |
| 8:00 AM | | | | |
| 8:15 AM | | | | |
| 8:30 AM | | | | |
| 8:45 AM | | | | |

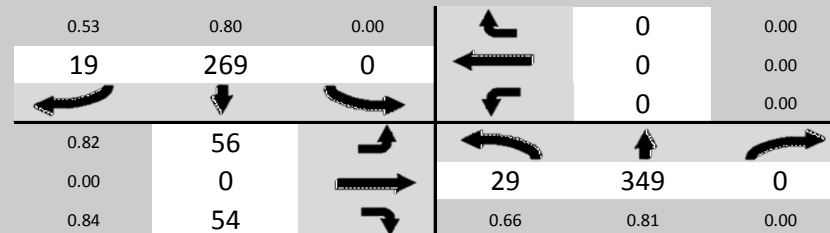


Diagram for: Peak Hour
Peak Hour: 07:15 AM-08:15 AM



| | | | | | | | | | | | | |
|----------------------------|-------------------|---------------------------|--------------|-------------------|----------------|----------------------|--|----------------|--------------|------------------|----------------|--------------|
| North/South Street: | | Klein Rd | | | | | | | | | | |
| East/West Street: | | Dove Crossing Dr / | | | | | | | | | | |
| TOD: | Midday | Date: | 22-May-18 | | | Synchro Node: | 3 Raw Data: H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | Dove Crossing Dr | | | | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 11:00 AM | 3 | 34 | 0 | 0 | 25 | 2 | 6 | 0 | 0 | 0 | 0 | 0 |
| 11:15 AM | 0 | 29 | 0 | 0 | 17 | 2 | 2 | 0 | 2 | 0 | 0 | 0 |
| 11:30 AM | 0 | 38 | 0 | 0 | 30 | 5 | 5 | 0 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 32 | 0 | 0 | 25 | 6 | 6 | 0 | 1 | 0 | 0 | 0 |
| 12:00 PM | 1 | 33 | 0 | 0 | 34 | 4 | 5 | 0 | 1 | 0 | 0 | 0 |
| 12:15 PM | 1 | 38 | 0 | 0 | 29 | 6 | 3 | 0 | 1 | 0 | 0 | 0 |
| 12:30 PM | 0 | 30 | 0 | 0 | 22 | 3 | 14 | 0 | 0 | 0 | 0 | 0 |
| 12:45 PM | 3 | 42 | 0 | 0 | 28 | 13 | 4 | 0 | 2 | 0 | 0 | 0 |
| Total | 8 | 276 | 0 | 0 | 210 | 41 | 45 | 0 | 7 | 0 | 0 | 0 |
| Peak Hour | 5 | 143 | 0 | 0 | 113 | 26 | 26 | 0 | 4 | 0 | 0 | 0 |

| Pedestrians | | | | |
|--------------------|-----------|-----------|-----------|-----------|
| | NB | SB | EB | WB |
| 11:00 AM | | | | |
| 11:15 AM | | | | |
| 11:30 AM | | | | |
| 11:45 AM | | | | |
| 12:00 PM | | | | |
| 12:15 PM | | | | |
| 12:30 PM | | | | |
| 12:45 PM | | | | |

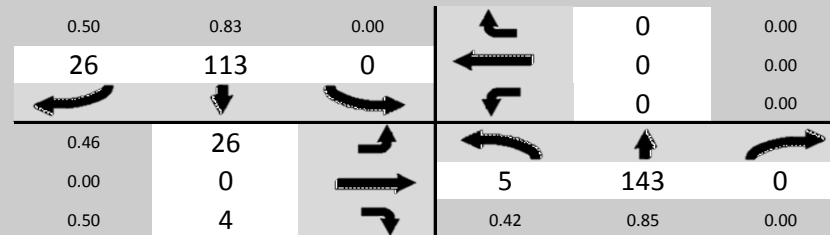


Diagram for: Peak Hour
Peak Hour: 12:00 PM-01:00 PM



| | | | | | | | | | | | | |
|----------------------------|-------------------|---------------------------|--------------|-------------------|----------------------|--|------------------|----------------|--------------|------------------|----------------|--------------|
| North/South Street: | | Klein Rd | | | | | | | | | | |
| East/West Street: | | Dove Crossing Dr / | | | | | | | | | | |
| TOD: | PM | Date: | 22-May-18 | | Synchro Node: | 3 Raw Data: H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | Dove Crossing Dr | | | | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 4:00 PM | 5 | 64 | 0 | 0 | 55 | 3 | 5 | 0 | 2 | 0 | 0 | 0 |
| 4:15 PM | 6 | 57 | 0 | 0 | 54 | 9 | 4 | 0 | 6 | 0 | 0 | 0 |
| 4:30 PM | 4 | 51 | 0 | 0 | 46 | 13 | 15 | 0 | 7 | 0 | 0 | 0 |
| 4:45 PM | 5 | 54 | 0 | 0 | 50 | 16 | 10 | 0 | 4 | 0 | 0 | 0 |
| 5:00 PM | 4 | 56 | 0 | 0 | 56 | 12 | 12 | 0 | 4 | 0 | 0 | 0 |
| 5:15 PM | 4 | 59 | 0 | 0 | 73 | 18 | 7 | 0 | 8 | 0 | 0 | 0 |
| 5:30 PM | 2 | 49 | 0 | 0 | 76 | 16 | 12 | 0 | 9 | 0 | 0 | 0 |
| 5:45 PM | 4 | 54 | 0 | 0 | 91 | 27 | 11 | 0 | 12 | 0 | 0 | 0 |
| Total | 34 | 444 | 0 | 0 | 501 | 114 | 76 | 0 | 52 | 0 | 0 | 0 |
| Peak Hour | 14 | 218 | 0 | 0 | 296 | 73 | 42 | 0 | 33 | 0 | 0 | 0 |

| Pedestrians | | | | |
|--------------------|-----------|-----------|-----------|-----------|
| | NB | SB | EB | WB |
| 4:00 PM | | | | |
| 4:15 PM | | | | |
| 4:30 PM | | | | |
| 4:45 PM | | | | |
| 5:00 PM | | | | |
| 5:15 PM | | | | |
| 5:30 PM | | | | |
| 5:45 PM | | | | |

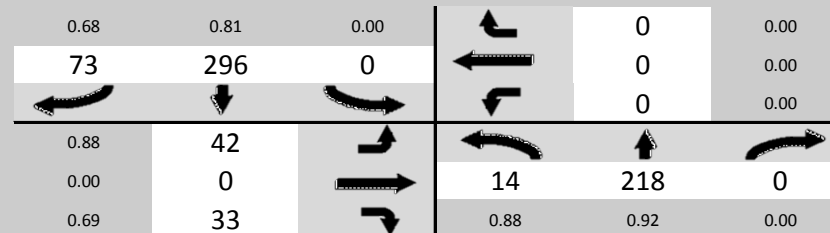


Diagram for: Peak Hour
Peak Hour: 05:00 PM-06:00 PM



| | | | | | | | | | | | | |
|-------------------------------------|-------------|----------------|--------------|----------------------|--|--------------|-------------|----------------|--------------|-------------|----------------|--------------|
| North/South Street: Klein Rd | | | | | | | | | | | | |
| East/West Street: FM 725 | | | | | | | | | | | | |
| TOD: | AM | Date: | 22-May-18 | Synchro Node: | 4 Raw Data: H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | | | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | FM 725 | | | FM 725 | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 7:00 AM | 53 | 0 | 32 | 0 | 1 | 3 | 1 | 65 | 20 | 45 | 158 | 0 |
| 7:15 AM | 59 | 1 | 54 | 0 | 1 | 3 | 0 | 67 | 23 | 67 | 181 | 0 |
| 7:30 AM | 63 | 0 | 43 | 1 | 0 | 2 | 1 | 81 | 29 | 32 | 201 | 1 |
| 7:45 AM | 53 | 0 | 32 | 0 | 0 | 3 | 1 | 82 | 33 | 33 | 161 | 1 |
| 8:00 AM | 55 | 1 | 26 | 0 | 1 | 0 | 0 | 67 | 29 | 11 | 105 | 0 |
| 8:15 AM | 60 | 0 | 17 | 0 | 0 | 3 | 0 | 71 | 13 | 5 | 157 | 1 |
| 8:30 AM | 30 | 0 | 13 | 0 | 0 | 1 | 1 | 78 | 16 | 17 | 122 | 0 |
| 8:45 AM | 20 | 0 | 4 | 1 | 0 | 1 | 1 | 75 | 20 | 9 | 137 | 0 |
| Total | 393 | 2 | 221 | 2 | 3 | 16 | 5 | 586 | 183 | 219 | 1222 | 3 |
| Peak Hour | 228 | 1 | 161 | 1 | 2 | 11 | 3 | 295 | 105 | 177 | 701 | 2 |

| Pedestrians | | | | |
|-------------|----|----|----|----|
| | NB | SB | EB | WB |
| 7:00 AM | | | | |
| 7:15 AM | | | | |
| 7:30 AM | | | | |
| 7:45 AM | | | | |
| 8:00 AM | | | | |
| 8:15 AM | | | | |
| 8:30 AM | | | | |
| 8:45 AM | | | | |

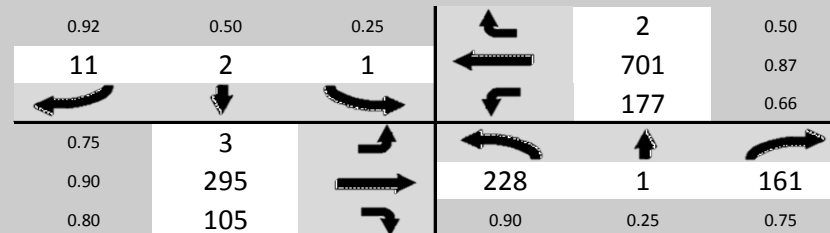


Diagram for: Peak Hour
Peak Hour: 07:00 AM-08:00 AM



| | | | | | | | | | | | | |
|-------------------------------------|-------------------|----------------|--------------|----------------------|----------------|------------------|--|----------------|--------------|------------------|----------------|--------------|
| North/South Street: Klein Rd | | | | | | | | | | | | |
| East/West Street: FM 725 | | | | | | | | | | | | |
| TOD: | Midday | Date: | 22-May-18 | Synchro Node: | 4 | Raw Data: | H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | FM 725 | | | FM 725 | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 11:00 AM | 27 | 1 | 11 | 0 | 0 | 0 | 4 | 83 | 13 | 6 | 113 | 2 |
| 11:15 AM | 22 | 0 | 9 | 0 | 0 | 4 | 1 | 88 | 17 | 8 | 116 | 0 |
| 11:30 AM | 26 | 1 | 11 | 2 | 1 | 0 | 0 | 106 | 19 | 6 | 100 | 0 |
| 11:45 AM | 24 | 0 | 11 | 1 | 0 | 2 | 1 | 114 | 25 | 9 | 87 | 1 |
| 12:00 PM | 28 | 0 | 9 | 0 | 0 | 0 | 1 | 108 | 26 | 8 | 98 | 1 |
| 12:15 PM | 31 | 1 | 12 | 0 | 0 | 2 | 2 | 97 | 23 | 10 | 99 | 1 |
| 12:30 PM | 33 | 0 | 12 | 0 | 0 | 1 | 2 | 97 | 26 | 6 | 121 | 0 |
| 12:45 PM | 28 | 0 | 13 | 1 | 0 | 2 | 4 | 113 | 30 | 6 | 111 | 1 |
| Total | 219 | 3 | 88 | 4 | 1 | 11 | 15 | 806 | 179 | 59 | 845 | 6 |
| Peak Hour | 120 | 1 | 46 | 1 | 0 | 5 | 9 | 415 | 105 | 30 | 429 | 3 |

| Pedestrians | | | | |
|--------------------|-----------|-----------|-----------|-----------|
| | NB | SB | EB | WB |
| 11:00 AM | | | | |
| 11:15 AM | | | | |
| 11:30 AM | | | | |
| 11:45 AM | | | | |
| 12:00 PM | | | | |
| 12:15 PM | | | | |
| 12:30 PM | | | | |
| 12:45 PM | | | | |

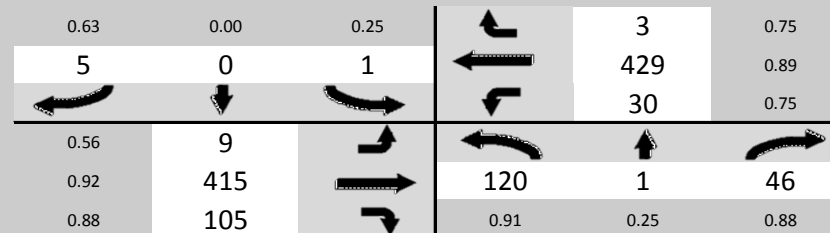


Diagram for: Peak Hour
Peak Hour: 12:00 PM-01:00 PM



| | | | | | | | | | | | | |
|-------------------------------------|-------------|----------------|--------------|-------------|----------------------|--------------|-------------|------------------|--|-------------|----------------|--------------|
| North/South Street: Klein Rd | | | | | | | | | | | | |
| East/West Street: FM 725 | | | | | | | | | | | | |
| TOD: | PM | Date: | 22-May-18 | | Synchro Node: | 4 | | Raw Data: | H:\projects\510\30\01\Traffic\Data\RAW\Sit | | | |
| | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
| | Klein Rd | | | Klein Rd | | | FM 725 | | | FM 725 | | |
| Time | Left | Through | Right | Left | Through | Right | Left | Through | Right | Left | Through | Right |
| 4:00 PM | 46 | 0 | 22 | 0 | 0 | 1 | 2 | 144 | 26 | 15 | 132 | 0 |
| 4:15 PM | 34 | 0 | 18 | 0 | 0 | 0 | 4 | 150 | 43 | 15 | 130 | 0 |
| 4:30 PM | 34 | 2 | 33 | 0 | 1 | 1 | 2 | 179 | 37 | 21 | 129 | 0 |
| 4:45 PM | 22 | 0 | 21 | 0 | 0 | 0 | 0 | 178 | 46 | 16 | 114 | 1 |
| 5:00 PM | 39 | 2 | 32 | 2 | 0 | 3 | 4 | 162 | 41 | 32 | 153 | 1 |
| 5:15 PM | 24 | 1 | 28 | 1 | 0 | 2 | 6 | 195 | 55 | 33 | 162 | 2 |
| 5:30 PM | 28 | 0 | 33 | 0 | 1 | 1 | 3 | 158 | 54 | 42 | 147 | 1 |
| 5:45 PM | 33 | 1 | 29 | 0 | 0 | 0 | 1 | 163 | 54 | 41 | 141 | 0 |
| Total | 260 | 6 | 216 | 3 | 2 | 8 | 22 | 1329 | 356 | 215 | 1108 | 5 |
| Peak Hour | 124 | 4 | 122 | 3 | 1 | 6 | 14 | 678 | 204 | 148 | 603 | 4 |

| Pedestrians | | | | |
|-------------|----|----|----|----|
| | NB | SB | EB | WB |
| 4:00 PM | | | | |
| 4:15 PM | | | | |
| 4:30 PM | | | | |
| 4:45 PM | | | | |
| 5:00 PM | | | | |
| 5:15 PM | | | | |
| 5:30 PM | | | | |
| 5:45 PM | | | | |

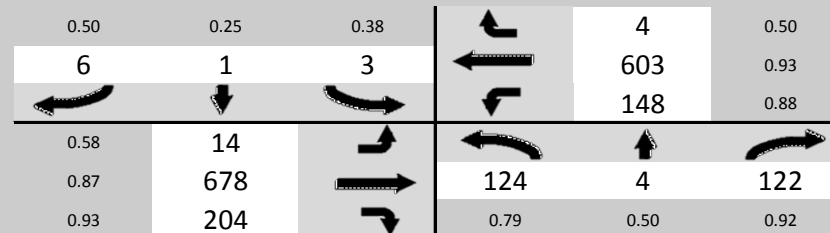


Diagram for: Peak Hour
Peak Hour: 05:00 PM-06:00 PM



APPENDIX C3

HCM Unsignalized Intersection Capacity Analysis
3: Klein & Walnut

Existing AM
07/24/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|------|------|-------|------|----------------------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 38 | 159 | 168 | 268 | 318 | 88 |
| Future Volume (Veh/h) | 38 | 159 | 168 | 268 | 318 | 88 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.73 | 0.83 | 0.76 | 0.78 | 0.64 | 0.69 |
| Hourly flow rate (vph) | 52 | 192 | 221 | 344 | 497 | 128 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 1347 | 561 | 625 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 1347 | 561 | 625 | | | |
| tC, single (s) | 6.4 | 6.2 | 4.1 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | |
| p0 queue free % | 59 | 63 | 77 | | | |
| cM capacity (veh/h) | 127 | 525 | 947 | | | |
| Direction, Lane # | EB 1 | EB 2 | NB 1 | NB 2 | SB 1 | |
| Volume Total | 52 | 192 | 221 | 344 | 625 | |
| Volume Left | 52 | 0 | 221 | 0 | 0 | |
| Volume Right | 0 | 192 | 0 | 0 | 128 | |
| cSH | 127 | 525 | 947 | 1700 | 1700 | |
| Volume to Capacity | 0.41 | 0.37 | 0.23 | 0.20 | 0.37 | |
| Queue Length 95th (ft) | 44 | 42 | 23 | 0 | 0 | |
| Control Delay (s) | 51.7 | 15.8 | 10.0 | 0.0 | 0.0 | |
| Lane LOS | F | C | A | | | |
| Approach Delay (s) | 23.4 | | 3.9 | | 0.0 | |
| Approach LOS | C | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 5.5 | | | |
| Intersection Capacity Utilization | | | 44.7% | | ICU Level of Service | A |
| Analysis Period (min) | | | 15 | | | |

HCM Unsignalized Intersection Capacity Analysis
5: Klein & Roadrunner/Stoeger

Existing AM
07/24/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------------|-------------|-------------|-------------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Volume (veh/h) | 33 | 0 | 13 | 7 | 0 | 24 | 7 | 327 | 4 | 9 | 315 | 5 |
| Future Volume (Veh/h) | 33 | 0 | 13 | 7 | 0 | 24 | 7 | 327 | 4 | 9 | 315 | 5 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.69 | 1.00 | 0.65 | 0.58 | 1.00 | 0.50 | 0.58 | 0.79 | 0.50 | 0.45 | 0.80 | 0.63 |
| Hourly flow rate (vph) | 48 | 0 | 20 | 12 | 0 | 48 | 12 | 414 | 8 | 20 | 394 | 8 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | None | | | None | |
| Median storage (veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 928 | 884 | 398 | 900 | 884 | 418 | 402 | | | 422 | | |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 928 | 884 | 398 | 900 | 884 | 418 | 402 | | | 422 | | |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 79 | 100 | 97 | 95 | 100 | 92 | 99 | | | 98 | | |
| cM capacity (veh/h) | 225 | 276 | 652 | 246 | 276 | 635 | 1157 | | | 1137 | | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 68 | 60 | 434 | 422 | | | | | | | | |
| Volume Left | 48 | 12 | 12 | 20 | | | | | | | | |
| Volume Right | 20 | 48 | 8 | 8 | | | | | | | | |
| cSH | 278 | 483 | 1157 | 1137 | | | | | | | | |
| Volume to Capacity | 0.24 | 0.12 | 0.01 | 0.02 | | | | | | | | |
| Queue Length 95th (ft) | 23 | 11 | 1 | 1 | | | | | | | | |
| Control Delay (s) | 22.1 | 13.5 | 0.3 | 0.6 | | | | | | | | |
| Lane LOS | C | B | A | A | | | | | | | | |
| Approach Delay (s) | 22.1 | 13.5 | 0.3 | 0.6 | | | | | | | | |
| Approach LOS | C | B | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 2.7 | | | | | | | | | |
| Intersection Capacity Utilization | | | 34.9% | | ICU Level of Service | | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

8: Klein & Dove Crossing

Existing AM
07/24/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|-------------|-------------|-------------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 56 | 54 | 29 | 349 | 269 | 19 |
| Future Volume (Veh/h) | 56 | 54 | 29 | 349 | 269 | 19 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.82 | 0.84 | 0.66 | 0.81 | 0.80 | 0.53 |
| Hourly flow rate (vph) | 68 | 64 | 44 | 431 | 336 | 36 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | 6 | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 873 | 354 | 372 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 873 | 354 | 372 | | | |
| tC, single (s) | 6.4 | 6.2 | 4.1 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | |
| p0 queue free % | 78 | 91 | 96 | | | |
| cM capacity (veh/h) | 309 | 690 | 1186 | | | |
| Direction, Lane # | EB 1 | NB 1 | SB 1 | | | |
| Volume Total | 132 | 475 | 372 | | | |
| Volume Left | 68 | 44 | 0 | | | |
| Volume Right | 64 | 0 | 36 | | | |
| cSH | 599 | 1186 | 1700 | | | |
| Volume to Capacity | 0.22 | 0.04 | 0.22 | | | |
| Queue Length 95th (ft) | 21 | 3 | 0 | | | |
| Control Delay (s) | 15.5 | 1.1 | 0.0 | | | |
| Lane LOS | C | A | | | | |
| Approach Delay (s) | 15.5 | 1.1 | 0.0 | | | |
| Approach LOS | C | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 2.6 | | | |
| Intersection Capacity Utilization | | | 48.6% | ICU Level of Service | A | |
| Analysis Period (min) | | | 15 | | | |

HCM Signalized Intersection Capacity Analysis
 10: Klein & FM 725/FM725

Existing AM
 07/24/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|-------|-------|------|-------|------|------|------|------|------|
| Lane Configurations | ↖ | ↑ | ↗ | ↖ | ↗ | | ↖ | ↗ | | ↖ | ↗ | |
| Traffic Volume (vph) | 2 | 297 | 114 | 143 | 648 | 2 | 230 | 2 | 155 | 1 | 2 | 8 |
| Future Volume (vph) | 2 | 297 | 114 | 143 | 648 | 2 | 230 | 2 | 155 | 1 | 2 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.85 | | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1776 | 1482 | 1719 | 1775 | | 1752 | 1573 | | 1770 | 1653 | |
| Flt Permitted | 0.28 | 1.00 | 1.00 | 0.43 | 1.00 | | 0.75 | 1.00 | | 0.47 | 1.00 | |
| Satd. Flow (perm) | 514 | 1776 | 1482 | 770 | 1775 | | 1378 | 1573 | | 880 | 1653 | |
| Peak-hour factor, PHF | 0.50 | 0.91 | 0.86 | 0.53 | 0.81 | 0.50 | 0.91 | 0.50 | 0.72 | 0.25 | 0.50 | 0.67 |
| Adj. Flow (vph) | 4 | 326 | 133 | 270 | 800 | 4 | 253 | 4 | 215 | 4 | 4 | 12 |
| RTOR Reduction (vph) | 0 | 0 | 69 | 0 | 0 | 0 | 0 | 169 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 4 | 326 | 64 | 270 | 804 | 0 | 253 | 50 | 0 | 4 | 7 | 0 |
| Heavy Vehicles (%) | 2% | 7% | 9% | 5% | 7% | 2% | 3% | 2% | 3% | 2% | 2% | 2% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | 4 |
| Permitted Phases | 2 | | 2 | 6 | | | 8 | 8 | | 4 | 4 | |
| Actuated Green, G (s) | 44.1 | 43.6 | 43.6 | 50.9 | 50.9 | | 19.2 | 19.2 | | 19.2 | 19.2 | |
| Effective Green, g (s) | 44.1 | 43.6 | 43.6 | 50.9 | 50.9 | | 19.2 | 19.2 | | 19.2 | 19.2 | |
| Actuated g/C Ratio | 0.49 | 0.48 | 0.48 | 0.57 | 0.57 | | 0.21 | 0.21 | | 0.21 | 0.21 | |
| Clearance Time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 304 | 860 | 717 | 552 | 1003 | | 293 | 335 | | 187 | 352 | |
| v/s Ratio Prot | 0.00 | c0.18 | | 0.06 | c0.45 | | | 0.03 | | | 0.00 | |
| v/s Ratio Perm | 0.01 | | 0.04 | 0.22 | | | c0.18 | | | 0.00 | | |
| v/c Ratio | 0.01 | 0.38 | 0.09 | 0.49 | 0.80 | | 0.86 | 0.15 | | 0.02 | 0.02 | |
| Uniform Delay, d1 | 17.2 | 14.7 | 12.5 | 10.8 | 15.5 | | 34.1 | 28.8 | | 28.0 | 28.0 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 1.3 | 0.2 | 0.7 | 6.7 | | 22.2 | 0.2 | | 0.0 | 0.0 | |
| Delay (s) | 17.2 | 15.9 | 12.8 | 11.5 | 22.3 | | 56.3 | 29.0 | | 28.0 | 28.0 | |
| Level of Service | B | B | B | B | C | | E | C | | C | C | |
| Approach Delay (s) | | 15.0 | | | 19.6 | | | 43.6 | | | 28.0 | |
| Approach LOS | | B | | | B | | | D | | | C | |

| Intersection Summary | | |
|-----------------------------------|-------|-----------------------------|
| HCM 2000 Control Delay | 24.2 | HCM 2000 Level of Service C |
| HCM 2000 Volume to Capacity ratio | 0.80 | |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) 16.1 |
| Intersection Capacity Utilization | 70.4% | ICU Level of Service C |
| Analysis Period (min) | 15 | |
| c Critical Lane Group | | |

Intersection: 3: Klein & Walnut

| Movement | EB | EB | NB |
|-----------------------|-----|-----|-----|
| Directions Served | L | R | L |
| Maximum Queue (ft) | 50 | 68 | 160 |
| Average Queue (ft) | 23 | 42 | 38 |
| 95th Queue (ft) | 45 | 63 | 81 |
| Link Distance (ft) | 336 | 336 | |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | | 260 |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: Klein & Roadrunner/Stoeger

| Movement | EB | WB | NB | SB |
|-----------------------|-----|-----|------|-----|
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 56 | 31 | 29 | 50 |
| Average Queue (ft) | 24 | 14 | 1 | 5 |
| 95th Queue (ft) | 49 | 38 | 10 | 28 |
| Link Distance (ft) | 532 | 456 | 2995 | 665 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 8: Klein & Dove Crossing

| Movement | EB | EB | NB |
|-----------------------|-----|-----|-----|
| Directions Served | L | R | LT |
| Maximum Queue (ft) | 71 | 68 | 77 |
| Average Queue (ft) | 31 | 30 | 7 |
| 95th Queue (ft) | 54 | 56 | 34 |
| Link Distance (ft) | 556 | | 665 |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | 150 | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 10: Klein & FM 725/FM725

| Movement | EB | EB | WB | WB | NB | NB | SB |
|-----------------------|-----|-----|----|-----|-----|------|-----|
| Directions Served | T | R | L | TR | L | TR | TR |
| Maximum Queue (ft) | 162 | 72 | 95 | 407 | 224 | 289 | 51 |
| Average Queue (ft) | 72 | 25 | 58 | 139 | 142 | 58 | 8 |
| 95th Queue (ft) | 143 | 55 | 96 | 308 | 231 | 145 | 32 |
| Link Distance (ft) | 508 | | | 545 | | 1243 | 403 |
| Upstream Blk Time (%) | | | | | | | |
| Queuing Penalty (veh) | | | | | | | |
| Storage Bay Dist (ft) | | 150 | 70 | | 200 | | |
| Storage Blk Time (%) | 2 | | 4 | 14 | 4 | | |
| Queuing Penalty (veh) | 2 | | 26 | 20 | 7 | | |

Network Summary

Network wide Queuing Penalty: 54

HCM Unsignalized Intersection Capacity Analysis
3: Klein & Walnut

Existing MID
07/24/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|------|------|-------|------|----------------------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 37 | 45 | 34 | 82 | 68 | 40 |
| Future Volume (Veh/h) | 37 | 45 | 34 | 82 | 68 | 40 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.71 | 0.80 | 0.65 | 0.82 | 0.65 | 0.71 |
| Hourly flow rate (vph) | 52 | 56 | 52 | 100 | 105 | 56 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 337 | 133 | 161 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 337 | 133 | 161 | | | |
| tC, single (s) | 6.4 | 6.2 | 4.1 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | |
| p0 queue free % | 92 | 94 | 96 | | | |
| cM capacity (veh/h) | 630 | 911 | 1412 | | | |
| Direction, Lane # | EB 1 | EB 2 | NB 1 | NB 2 | SB 1 | |
| Volume Total | 52 | 56 | 52 | 100 | 161 | |
| Volume Left | 52 | 0 | 52 | 0 | 0 | |
| Volume Right | 0 | 56 | 0 | 0 | 56 | |
| cSH | 630 | 911 | 1412 | 1700 | 1700 | |
| Volume to Capacity | 0.08 | 0.06 | 0.04 | 0.06 | 0.09 | |
| Queue Length 95th (ft) | 7 | 5 | 3 | 0 | 0 | |
| Control Delay (s) | 11.2 | 9.2 | 7.6 | 0.0 | 0.0 | |
| Lane LOS | B | A | A | | | |
| Approach Delay (s) | 10.2 | | 2.6 | | 0.0 | |
| Approach LOS | B | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 3.6 | | | |
| Intersection Capacity Utilization | | | 18.6% | | ICU Level of Service | A |
| Analysis Period (min) | | | 15 | | | |

HCM Unsignalized Intersection Capacity Analysis

5: Klein & Roadrunner/Stoeger

Existing MID
07/24/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------------|-------------|-------------|-------------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Volume (veh/h) | 11 | 1 | 2 | 1 | 1 | 14 | 3 | 117 | 2 | 8 | 102 | 6 |
| Future Volume (Veh/h) | 11 | 1 | 2 | 1 | 1 | 14 | 3 | 117 | 2 | 8 | 102 | 6 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.55 | 0.25 | 0.50 | 0.25 | 0.25 | 0.58 | 0.38 | 0.70 | 0.50 | 0.67 | 0.85 | 0.50 |
| Hourly flow rate (vph) | 20 | 4 | 4 | 4 | 4 | 24 | 8 | 167 | 4 | 12 | 120 | 12 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | None | | | None | |
| Median storage (veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 361 | 337 | 126 | 341 | 341 | 169 | 132 | | | 171 | | |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 361 | 337 | 126 | 341 | 341 | 169 | 132 | | | 171 | | |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 96 | 99 | 100 | 99 | 99 | 97 | 99 | | | 99 | | |
| cM capacity (veh/h) | 569 | 576 | 924 | 601 | 573 | 875 | 1453 | | | 1406 | | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 28 | 32 | 179 | 144 | | | | | | | | |
| Volume Left | 20 | 4 | 8 | 12 | | | | | | | | |
| Volume Right | 4 | 24 | 4 | 12 | | | | | | | | |
| cSH | 603 | 779 | 1453 | 1406 | | | | | | | | |
| Volume to Capacity | 0.05 | 0.04 | 0.01 | 0.01 | | | | | | | | |
| Queue Length 95th (ft) | 4 | 3 | 0 | 1 | | | | | | | | |
| Control Delay (s) | 11.3 | 9.8 | 0.4 | 0.7 | | | | | | | | |
| Lane LOS | B | A | A | A | | | | | | | | |
| Approach Delay (s) | 11.3 | 9.8 | 0.4 | 0.7 | | | | | | | | |
| Approach LOS | B | A | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 2.1 | | | | | | | | | |
| Intersection Capacity Utilization | | | 21.3% | | ICU Level of Service | | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

8: Klein & Dove Crossing

Existing MID
07/24/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|-------------|-------------|-------------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 26 | 4 | 5 | 143 | 113 | 26 |
| Future Volume (Veh/h) | 26 | 4 | 5 | 143 | 113 | 26 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.46 | 0.50 | 0.42 | 0.85 | 0.83 | 0.50 |
| Hourly flow rate (vph) | 57 | 8 | 12 | 168 | 136 | 52 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | 6 | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 354 | 162 | 188 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 354 | 162 | 188 | | | |
| tC, single (s) | 6.4 | 6.2 | 4.1 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | |
| p0 queue free % | 91 | 99 | 99 | | | |
| cM capacity (veh/h) | 638 | 883 | 1386 | | | |
| Direction, Lane # | EB 1 | NB 1 | SB 1 | | | |
| Volume Total | 65 | 180 | 188 | | | |
| Volume Left | 57 | 12 | 0 | | | |
| Volume Right | 8 | 0 | 52 | | | |
| cSH | 728 | 1386 | 1700 | | | |
| Volume to Capacity | 0.09 | 0.01 | 0.11 | | | |
| Queue Length 95th (ft) | 7 | 1 | 0 | | | |
| Control Delay (s) | 10.9 | 0.6 | 0.0 | | | |
| Lane LOS | B | A | | | | |
| Approach Delay (s) | 10.9 | 0.6 | 0.0 | | | |
| Approach LOS | B | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 1.9 | | | |
| Intersection Capacity Utilization | | | 21.6% | ICU Level of Service | A | |
| Analysis Period (min) | | | 15 | | | |

HCM Signalized Intersection Capacity Analysis
 10: Klein & FM 725/FM725

Existing MID
 07/24/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|-------|-------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 9 | 415 | 105 | 30 | 429 | 3 | 120 | 1 | 46 | 1 | 0 | 5 |
| Future Volume (vph) | 9 | 415 | 105 | 30 | 429 | 3 | 120 | 1 | 46 | 1 | 0 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.86 | | 1.00 | 0.85 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1687 | 1792 | 1524 | 1671 | 1758 | | 1703 | 1589 | | 1770 | 1583 | |
| Flt Permitted | 0.43 | 1.00 | 1.00 | 0.41 | 1.00 | | 0.75 | 1.00 | | 0.72 | 1.00 | |
| Satd. Flow (perm) | 759 | 1792 | 1524 | 727 | 1758 | | 1349 | 1589 | | 1342 | 1583 | |
| Peak-hour factor, PHF | 0.56 | 0.92 | 0.88 | 0.75 | 0.89 | 0.75 | 0.91 | 0.25 | 0.88 | 0.25 | 1.00 | 0.63 |
| Adj. Flow (vph) | 16 | 451 | 119 | 40 | 482 | 4 | 132 | 4 | 52 | 4 | 0 | 8 |
| RTOR Reduction (vph) | 0 | 0 | 62 | 0 | 1 | 0 | 0 | 43 | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 16 | 451 | 57 | 40 | 485 | 0 | 132 | 13 | 0 | 4 | 1 | 0 |
| Heavy Vehicles (%) | 7% | 6% | 6% | 8% | 8% | 2% | 6% | 2% | 3% | 2% | 2% | 2% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | 4 |
| Permitted Phases | 2 | | 2 | 6 | | | 8 | 8 | | 4 | 4 | |
| Actuated Green, G (s) | 26.3 | 25.4 | 25.4 | 28.5 | 26.5 | | 9.7 | 9.7 | | 9.7 | 9.7 | |
| Effective Green, g (s) | 26.3 | 25.4 | 25.4 | 28.5 | 26.5 | | 9.7 | 9.7 | | 9.7 | 9.7 | |
| Actuated g/C Ratio | 0.49 | 0.48 | 0.48 | 0.54 | 0.50 | | 0.18 | 0.18 | | 0.18 | 0.18 | |
| Clearance Time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 390 | 855 | 727 | 424 | 875 | | 245 | 289 | | 244 | 288 | |
| v/s Ratio Prot | 0.00 | 0.25 | | c0.00 | c0.28 | | | 0.01 | | | 0.00 | |
| v/s Ratio Perm | 0.02 | | 0.04 | 0.05 | | | c0.10 | | | 0.00 | | |
| v/c Ratio | 0.04 | 0.53 | 0.08 | 0.09 | 0.55 | | 0.54 | 0.05 | | 0.02 | 0.01 | |
| Uniform Delay, d1 | 7.0 | 9.7 | 7.5 | 6.1 | 9.3 | | 19.7 | 17.9 | | 17.8 | 17.8 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 0.6 | 0.0 | 0.1 | 0.8 | | 2.3 | 0.1 | | 0.0 | 0.0 | |
| Delay (s) | 7.0 | 10.3 | 7.6 | 6.2 | 10.0 | | 22.0 | 18.0 | | 17.9 | 17.8 | |
| Level of Service | A | B | A | A | B | | C | B | | B | B | |
| Approach Delay (s) | | 9.7 | | | 9.7 | | | 20.8 | | | 17.8 | |
| Approach LOS | | A | | | A | | | C | | | B | |

| Intersection Summary | | |
|-----------------------------------|-------|---------------------------|
| HCM 2000 Control Delay | 11.4 | HCM 2000 Level of Service |
| HCM 2000 Volume to Capacity ratio | 0.54 | B |
| Actuated Cycle Length (s) | 53.2 | Sum of lost time (s) |
| Intersection Capacity Utilization | 47.3% | 16.1 |
| Analysis Period (min) | 15 | ICU Level of Service |
| c Critical Lane Group | | A |

Intersection: 3: Klein & Walnut

| Movement | EB | EB | NB |
|-----------------------|-----|-----|-----|
| Directions Served | L | R | L |
| Maximum Queue (ft) | 31 | 77 | 31 |
| Average Queue (ft) | 24 | 29 | 4 |
| 95th Queue (ft) | 43 | 59 | 21 |
| Link Distance (ft) | 336 | 336 | |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | | 260 |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: Klein & Roadrunner/Stoeger

| Movement | EB | WB |
|-----------------------|-----|-----|
| Directions Served | LTR | LTR |
| Maximum Queue (ft) | 54 | 31 |
| Average Queue (ft) | 15 | 11 |
| 95th Queue (ft) | 42 | 35 |
| Link Distance (ft) | 532 | 456 |
| Upstream Blk Time (%) | | |
| Queuing Penalty (veh) | | |
| Storage Bay Dist (ft) | | |
| Storage Blk Time (%) | | |
| Queuing Penalty (veh) | | |

Intersection: 8: Klein & Dove Crossing

| Movement | EB | EB |
|-----------------------|-----|-----|
| Directions Served | L | R |
| Maximum Queue (ft) | 49 | 31 |
| Average Queue (ft) | 21 | 5 |
| 95th Queue (ft) | 45 | 23 |
| Link Distance (ft) | 608 | |
| Upstream Blk Time (%) | | |
| Queuing Penalty (veh) | | |
| Storage Bay Dist (ft) | | 150 |
| Storage Blk Time (%) | | |
| Queuing Penalty (veh) | | |

Intersection: 10: Klein & FM 725/FM725

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB |
|-----------------------|-----|-----|-----|----|-----|-----|------|-----|-----|
| Directions Served | L | T | R | L | TR | L | TR | L | TR |
| Maximum Queue (ft) | 30 | 242 | 174 | 48 | 135 | 152 | 69 | 28 | 30 |
| Average Queue (ft) | 5 | 76 | 23 | 16 | 59 | 57 | 24 | 1 | 6 |
| 95th Queue (ft) | 21 | 174 | 74 | 40 | 116 | 117 | 51 | 9 | 25 |
| Link Distance (ft) | | 381 | | | 374 | | 1243 | | 403 |
| Upstream Blk Time (%) | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | |
| Storage Bay Dist (ft) | 120 | | 150 | 70 | | 200 | | 120 | |
| Storage Blk Time (%) | | 2 | 0 | | 4 | | | | |
| Queuing Penalty (veh) | | 2 | 0 | | 1 | | | | |

Network Summary

Network wide Queuing Penalty: 3

HCM Unsignalized Intersection Capacity Analysis

3: Klein & Walnut

Existing PM
07/24/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|------|------|-------|------|----------------------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 138 | 131 | 54 | 127 | 174 | 73 |
| Future Volume (Veh/h) | 138 | 131 | 54 | 127 | 174 | 73 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.84 | 0.53 | 0.90 | 0.93 | 0.68 | 0.83 |
| Hourly flow rate (vph) | 164 | 247 | 60 | 137 | 256 | 88 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 557 | 300 | 344 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 557 | 300 | 344 | | | |
| tC, single (s) | 6.4 | 6.2 | 4.1 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | |
| p0 queue free % | 65 | 67 | 95 | | | |
| cM capacity (veh/h) | 467 | 740 | 1215 | | | |
| Direction, Lane # | EB 1 | EB 2 | NB 1 | NB 2 | SB 1 | |
| Volume Total | 164 | 247 | 60 | 137 | 344 | |
| Volume Left | 164 | 0 | 60 | 0 | 0 | |
| Volume Right | 0 | 247 | 0 | 0 | 88 | |
| cSH | 467 | 740 | 1215 | 1700 | 1700 | |
| Volume to Capacity | 0.35 | 0.33 | 0.05 | 0.08 | 0.20 | |
| Queue Length 95th (ft) | 39 | 37 | 4 | 0 | 0 | |
| Control Delay (s) | 16.8 | 12.3 | 8.1 | 0.0 | 0.0 | |
| Lane LOS | C | B | A | | | |
| Approach Delay (s) | 14.1 | | 2.5 | | 0.0 | |
| Approach LOS | B | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 6.6 | | | |
| Intersection Capacity Utilization | | | 34.6% | | ICU Level of Service | A |
| Analysis Period (min) | | | 15 | | | |

HCM Unsignalized Intersection Capacity Analysis
5: Klein & Roadrunner/Stoeger

Existing PM
07/24/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Volume (veh/h) | 11 | 0 | 8 | 0 | 2 | 7 | 9 | 219 | 3 | 22 | 269 | 36 |
| Future Volume (Veh/h) | 11 | 0 | 8 | 0 | 2 | 7 | 9 | 219 | 3 | 22 | 269 | 36 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.69 | 1.00 | 0.29 | 1.00 | 0.25 | 0.58 | 0.56 | 0.90 | 0.75 | 0.79 | 0.73 | 0.64 |
| Hourly flow rate (vph) | 16 | 0 | 28 | 0 | 8 | 12 | 16 | 243 | 4 | 28 | 368 | 56 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | None | | | None | |
| Median storage (veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 745 | 731 | 396 | 757 | 757 | 245 | 424 | | | 247 | | |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 745 | 731 | 396 | 757 | 757 | 245 | 424 | | | 247 | | |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.2 | | | 4.1 | | |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.3 | | | 2.2 | | |
| p0 queue free % | 95 | 100 | 96 | 100 | 98 | 98 | 99 | | | 98 | | |
| cM capacity (veh/h) | 310 | 336 | 653 | 302 | 325 | 794 | 1114 | | | 1319 | | |

| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 |
|------------------------|------|------|------|------|
| Volume Total | 44 | 20 | 263 | 452 |
| Volume Left | 16 | 0 | 16 | 28 |
| Volume Right | 28 | 12 | 4 | 56 |
| cSH | 466 | 503 | 1114 | 1319 |
| Volume to Capacity | 0.09 | 0.04 | 0.01 | 0.02 |
| Queue Length 95th (ft) | 8 | 3 | 1 | 2 |
| Control Delay (s) | 13.5 | 12.4 | 0.6 | 0.7 |
| Lane LOS | B | B | A | A |
| Approach Delay (s) | 13.5 | 12.4 | 0.6 | 0.7 |
| Approach LOS | B | B | | |

| Intersection Summary | | | |
|-----------------------------------|-------|----------------------|---|
| Average Delay | | 1.7 | |
| Intersection Capacity Utilization | 39.6% | ICU Level of Service | A |
| Analysis Period (min) | 15 | | |

HCM Unsignalized Intersection Capacity Analysis

8: Klein & Dove Crossing

Existing PM
07/24/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|-------------|-------------|-------------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 42 | 33 | 14 | 218 | 296 | 73 |
| Future Volume (Veh/h) | 42 | 33 | 14 | 218 | 296 | 73 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.88 | 0.69 | 0.88 | 0.92 | 0.81 | 0.68 |
| Hourly flow rate (vph) | 48 | 48 | 16 | 237 | 365 | 107 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | 6 | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 688 | 418 | 472 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 688 | 418 | 472 | | | |
| tC, single (s) | 6.4 | 6.3 | 4.2 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.4 | 2.3 | | | |
| p0 queue free % | 88 | 92 | 98 | | | |
| cM capacity (veh/h) | 406 | 626 | 1054 | | | |
| Direction, Lane # | EB 1 | NB 1 | SB 1 | | | |
| Volume Total | 96 | 253 | 472 | | | |
| Volume Left | 48 | 16 | 0 | | | |
| Volume Right | 48 | 0 | 107 | | | |
| cSH | 812 | 1054 | 1700 | | | |
| Volume to Capacity | 0.12 | 0.02 | 0.28 | | | |
| Queue Length 95th (ft) | 10 | 1 | 0 | | | |
| Control Delay (s) | 13.1 | 0.7 | 0.0 | | | |
| Lane LOS | B | A | | | | |
| Approach Delay (s) | 13.1 | 0.7 | 0.0 | | | |
| Approach LOS | B | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 1.7 | | | |
| Intersection Capacity Utilization | | | 33.0% | ICU Level of Service | A | |
| Analysis Period (min) | | | 15 | | | |

HCM Signalized Intersection Capacity Analysis
10: Klein & FM 725/FM725

Existing PM
07/24/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|-------|-------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 14 | 678 | 204 | 148 | 603 | 4 | 124 | 4 | 122 | 3 | 1 | 6 |
| Future Volume (vph) | 14 | 678 | 204 | 148 | 603 | 4 | 124 | 4 | 122 | 3 | 1 | 6 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.86 | | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1736 | 1810 | 1583 | 1736 | 1824 | | 1770 | 1570 | | 1770 | 1653 | |
| Flt Permitted | 0.41 | 1.00 | 1.00 | 0.11 | 1.00 | | 0.75 | 1.00 | | 0.62 | 1.00 | |
| Satd. Flow (perm) | 753 | 1810 | 1583 | 205 | 1824 | | 1392 | 1570 | | 1148 | 1653 | |
| Peak-hour factor, PHF | 0.58 | 0.87 | 0.93 | 0.88 | 0.93 | 0.50 | 0.79 | 0.50 | 0.92 | 0.38 | 0.25 | 0.50 |
| Adj. Flow (vph) | 24 | 779 | 219 | 168 | 648 | 8 | 157 | 8 | 133 | 8 | 4 | 12 |
| RTOR Reduction (vph) | 0 | 0 | 58 | 0 | 0 | 0 | 0 | 111 | 0 | 0 | 10 | 0 |
| Lane Group Flow (vph) | 24 | 779 | 161 | 168 | 656 | 0 | 157 | 30 | 0 | 8 | 6 | 0 |
| Heavy Vehicles (%) | 4% | 5% | 2% | 4% | 4% | 2% | 2% | 2% | 4% | 2% | 2% | 2% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | 4 |
| Permitted Phases | 2 | | 2 | 6 | | | 8 | 8 | | 4 | 4 | |
| Actuated Green, G (s) | 49.6 | 49.1 | 49.1 | 53.6 | 53.6 | | 15.2 | 15.2 | | 15.2 | 15.2 | |
| Effective Green, g (s) | 49.6 | 49.1 | 49.1 | 53.6 | 53.6 | | 15.2 | 15.2 | | 15.2 | 15.2 | |
| Actuated g/C Ratio | 0.55 | 0.55 | 0.55 | 0.60 | 0.60 | | 0.17 | 0.17 | | 0.17 | 0.17 | |
| Clearance Time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 470 | 987 | 863 | 285 | 1086 | | 235 | 265 | | 193 | 279 | |
| v/s Ratio Prot | 0.00 | c0.43 | | 0.06 | c0.36 | | | 0.02 | | | 0.00 | |
| v/s Ratio Perm | 0.03 | | 0.10 | 0.29 | | | c0.11 | | | 0.01 | | |
| v/c Ratio | 0.05 | 0.79 | 0.19 | 0.59 | 0.60 | | 0.67 | 0.11 | | 0.04 | 0.02 | |
| Uniform Delay, d1 | 9.5 | 16.3 | 10.3 | 15.1 | 11.5 | | 35.0 | 31.7 | | 31.3 | 31.2 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 6.4 | 0.5 | 3.1 | 2.5 | | 7.0 | 0.2 | | 0.1 | 0.0 | |
| Delay (s) | 9.6 | 22.7 | 10.8 | 18.2 | 14.0 | | 42.0 | 31.9 | | 31.4 | 31.2 | |
| Level of Service | A | C | B | B | B | | D | C | | C | C | |
| Approach Delay (s) | | 19.9 | | | 14.8 | | | 37.2 | | | 31.3 | |
| Approach LOS | | B | | | B | | | D | | | C | |

| Intersection Summary | | |
|-----------------------------------|-------|-----------------------------|
| HCM 2000 Control Delay | 20.5 | HCM 2000 Level of Service C |
| HCM 2000 Volume to Capacity ratio | 0.76 | |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) 16.1 |
| Intersection Capacity Utilization | 70.8% | ICU Level of Service C |
| Analysis Period (min) | 15 | |
| c Critical Lane Group | | |

Intersection: 3: Klein & Walnut

| Movement | EB | EB | NB |
|-----------------------|-----|-----|-----|
| Directions Served | L | R | L |
| Maximum Queue (ft) | 74 | 94 | 53 |
| Average Queue (ft) | 44 | 36 | 8 |
| 95th Queue (ft) | 67 | 58 | 32 |
| Link Distance (ft) | 336 | 336 | |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | | 260 |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: Klein & Roadrunner/Stoeger

| Movement | EB | WB | NB | SB |
|-----------------------|-----|-----|------|-----|
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 31 | 31 | 27 | 70 |
| Average Queue (ft) | 14 | 9 | 1 | 3 |
| 95th Queue (ft) | 39 | 32 | 9 | 25 |
| Link Distance (ft) | 532 | 456 | 2995 | 664 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 8: Klein & Dove Crossing

| Movement | EB | EB | NB | SB |
|-----------------------|-----|-----|-----|------|
| Directions Served | L | R | LT | TR |
| Maximum Queue (ft) | 76 | 31 | 55 | 22 |
| Average Queue (ft) | 19 | 23 | 10 | 1 |
| 95th Queue (ft) | 50 | 44 | 42 | 7 |
| Link Distance (ft) | 608 | | 664 | 1243 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | 150 | | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 10: Klein & FM 725/FM725

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|------|-----|-----|
| Directions Served | L | T | R | L | TR | L | TR | L | TR |
| Maximum Queue (ft) | 51 | 415 | 175 | 95 | 389 | 198 | 112 | 29 | 31 |
| Average Queue (ft) | 8 | 194 | 96 | 66 | 130 | 90 | 50 | 2 | 7 |
| 95th Queue (ft) | 31 | 374 | 204 | 106 | 289 | 157 | 92 | 11 | 27 |
| Link Distance (ft) | | 381 | | | 374 | | 1243 | | 403 |
| Upstream Blk Time (%) | | 4 | | | 1 | | | | |
| Queuing Penalty (veh) | | 0 | | | 0 | | | | |
| Storage Bay Dist (ft) | 120 | | 150 | 70 | | 200 | | 120 | |
| Storage Blk Time (%) | | 15 | 0 | 10 | 10 | 1 | | | |
| Queuing Penalty (veh) | | 32 | 0 | 62 | 15 | 1 | | | |

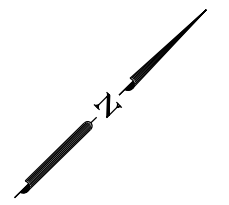
Network Summary

Network wide Queuing Penalty: 111

APPENDIX C4

Plotted on: 7/31/2018

Design Filename: P:\112\01\02\design\Civil\Working\Klein Growth.dgn



NTS

WALNUT AVENUE
ANNUAL GROWTH = 5%
GROWTH FACTOR = 2.93

DOVE CROSSING DRIVE
ANNUAL GROWTH = 2%
GROWTH FACTOR = 1.55

ROADRUNNER AVENUE
ANNUAL GROWTH = 2%
GROWTH FACTOR = 1.55

KLEIN ROAD
ANNUAL GROWTH = 5%
GROWTH FACTOR = 2.93

STOEGER DRIVE
ANNUAL GROWTH = 5%
GROWTH FACTOR = 2.93

FM 725
ANNUAL GROWTH = 5%
GROWTH FACTOR = 2.93

Pape-Dawson
ENGINEERS

SAN ANTONIO | AUSTIN | HOUSTON | FORT WORTH | DALLAS
2000 NW LOOP 410 | SAN ANTONIO, TX 78213 | 210.375.9000
TBPE FIRM REGISTRATION #470 | TBPLS FIRM REGISTRATION #10028800

 Texas Department of Transportation
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KLEIN ROAD
GROWTH RATE SUMMARY

WALNUT AVE TO FM 725

APPENDIX C5

HCM Unsignalized Intersection Capacity Analysis

3: Klein & Walnut

Future (No Build) AM
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|------|------|--------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 119 | 465 | 491 | 785 | 930 | 281 |
| Future Volume (Veh/h) | 119 | 465 | 491 | 785 | 930 | 281 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.73 | 0.83 | 0.76 | 0.78 | 0.64 | 0.68 |
| Hourly flow rate (vph) | 163 | 560 | 646 | 1006 | 1453 | 413 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 3958 | 1660 | 1866 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 3958 | 1660 | 1866 | | | |
| tC, single (s) | 6.4 | 6.2 | 4.1 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | |
| p0 queue free % | 0 | 0 | 0 | | | |
| cM capacity (veh/h) | 0 | 120 | 318 | | | |
| Direction, Lane # | EB 1 | EB 2 | NB 1 | NB 2 | SB 1 | |
| Volume Total | 163 | 560 | 646 | 1006 | 1866 | |
| Volume Left | 163 | 0 | 646 | 0 | 0 | |
| Volume Right | 0 | 560 | 0 | 0 | 413 | |
| cSH | 0 | 120 | 318 | 1700 | 1700 | |
| Volume to Capacity | Err | 4.68 | 2.03 | 0.59 | 1.10 | |
| Queue Length 95th (ft) | Err | Err | 1156 | 0 | 0 | |
| Control Delay (s) | Err | Err | 501.6 | 0.0 | 0.0 | |
| Lane LOS | F | F | F | | | |
| Approach Delay (s) | Err | | 196.2 | | 0.0 | |
| Approach LOS | F | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | Err | | | |
| Intersection Capacity Utilization | | | 109.8% | ICU Level of Service | | H |
| Analysis Period (min) | | | 15 | | | |

HCM Unsignalized Intersection Capacity Analysis
5: Klein & Roadrunner/Stoeger

Future (No Build) AM
07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|--------|----------------------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Volume (veh/h) | 51 | 0 | 21 | 21 | 0 | 71 | 12 | 993 | 12 | 27 | 933 | 8 |
| Future Volume (Veh/h) | 51 | 0 | 21 | 21 | 0 | 71 | 12 | 993 | 12 | 27 | 933 | 8 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.67 | 1.00 | 0.66 | 0.58 | 1.00 | 0.51 | 0.60 | 0.79 | 0.50 | 0.45 | 0.79 | 0.67 |
| Hourly flow rate (vph) | 76 | 0 | 32 | 36 | 0 | 139 | 20 | 1257 | 24 | 60 | 1181 | 12 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | | | | | |
| Median storage veh | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 2755 | 2628 | 1187 | 2648 | 2622 | 1269 | 1193 | | | 1281 | | |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 2755 | 2628 | 1187 | 2648 | 2622 | 1269 | 1193 | | | 1281 | | |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 0 | 100 | 86 | 0 | 100 | 32 | 97 | | | 89 | | |
| cM capacity (veh/h) | 4 | 20 | 230 | 12 | 21 | 205 | 585 | | | 542 | | |
| Direction, Lane # | | | | | | | | | | | | |
| | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 108 | 175 | 1301 | 1253 | | | | | | | | |
| Volume Left | 76 | 36 | 20 | 60 | | | | | | | | |
| Volume Right | 32 | 139 | 24 | 12 | | | | | | | | |
| cSH | 5 | 47 | 585 | 542 | | | | | | | | |
| Volume to Capacity | 20.87 | 3.76 | 0.03 | 0.11 | | | | | | | | |
| Queue Length 95th (ft) | Err | Err | 3 | 9 | | | | | | | | |
| Control Delay (s) | Err | Err | 1.7 | 5.0 | | | | | | | | |
| Lane LOS | F | F | A | A | | | | | | | | |
| Approach Delay (s) | Err | Err | 1.7 | 5.0 | | | | | | | | |
| Approach LOS | F | F | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 1000.4 | | | | | | | | | |
| Intersection Capacity Utilization | | | 83.0% | ICU Level of Service | E | | | | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

8: Klein & Dove Crossing

Future (No Build) AM
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|-------------|-------------|-------------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 86 | 83 | 45 | 1021 | 787 | 30 |
| Future Volume (Veh/h) | 86 | 83 | 45 | 1021 | 787 | 30 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.83 | 0.83 | 0.66 | 0.81 | 0.80 | 0.54 |
| Hourly flow rate (vph) | 104 | 100 | 68 | 1260 | 984 | 56 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | 6 | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 2408 | 1012 | 1040 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 2408 | 1012 | 1040 | | | |
| tC, single (s) | 6.4 | 6.2 | 4.1 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | |
| p0 queue free % | 0 | 66 | 90 | | | |
| cM capacity (veh/h) | 33 | 290 | 669 | | | |
| Direction, Lane # | EB 1 | NB 1 | SB 1 | | | |
| Volume Total | 204 | 1328 | 1040 | | | |
| Volume Left | 104 | 68 | 0 | | | |
| Volume Right | 100 | 0 | 56 | | | |
| cSH | 59 | 669 | 1700 | | | |
| Volume to Capacity | 3.47 | 0.10 | 0.61 | | | |
| Queue Length 95th (ft) | Err | 8 | 0 | | | |
| Control Delay (s) | Err | 4.7 | 0.0 | | | |
| Lane LOS | F | A | | | | |
| Approach Delay (s) | Err | 4.7 | 0.0 | | | |
| Approach LOS | F | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 795.5 | | | |
| Intersection Capacity Utilization | | | 101.7% | ICU Level of Service | G | |
| Analysis Period (min) | | | 15 | | | |

HCM Signalized Intersection Capacity Analysis
10: Klein & FM 725/FM725

Future (No Build) AM
07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|-------|-------|------|-------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 6 | 869 | 344 | 421 | 1895 | 6 | 704 | 6 | 460 | 3 | 6 | 24 |
| Future Volume (vph) | 6 | 869 | 344 | 421 | 1895 | 6 | 704 | 6 | 460 | 3 | 6 | 24 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.85 | | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1776 | 1482 | 1719 | 1775 | | 1752 | 1573 | | 1770 | 1653 | |
| Flt Permitted | 0.11 | 1.00 | 1.00 | 0.11 | 1.00 | | 0.73 | 1.00 | | 0.19 | 1.00 | |
| Satd. Flow (perm) | 201 | 1776 | 1482 | 198 | 1775 | | 1339 | 1573 | | 358 | 1653 | |
| Peak-hour factor, PHF | 0.50 | 0.91 | 0.86 | 0.53 | 0.81 | 0.50 | 0.91 | 0.50 | 0.72 | 0.25 | 0.50 | 0.67 |
| Adj. Flow (vph) | 12 | 955 | 400 | 794 | 2340 | 12 | 774 | 12 | 639 | 12 | 12 | 36 |
| RTOR Reduction (vph) | 0 | 0 | 117 | 0 | 0 | 0 | 0 | 262 | 0 | 0 | 28 | 0 |
| Lane Group Flow (vph) | 12 | 955 | 283 | 794 | 2352 | 0 | 774 | 389 | 0 | 12 | 20 | 0 |
| Heavy Vehicles (%) | 2% | 7% | 9% | 5% | 7% | 2% | 3% | 2% | 3% | 2% | 2% | 2% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | 4 |
| Permitted Phases | 2 | | 2 | 6 | | | 8 | 8 | | 4 | 4 | |
| Actuated Green, G (s) | 40.8 | 40.3 | 40.3 | 49.3 | 49.3 | | 20.8 | 20.8 | | 20.8 | 20.8 | |
| Effective Green, g (s) | 40.8 | 40.3 | 40.3 | 49.3 | 49.3 | | 20.8 | 20.8 | | 20.8 | 20.8 | |
| Actuated g/C Ratio | 0.45 | 0.45 | 0.45 | 0.55 | 0.55 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 157 | 795 | 663 | 324 | 972 | | 309 | 363 | | 82 | 382 | |
| v/s Ratio Prot | 0.00 | c0.54 | | 0.35 | c1.33 | | | 0.25 | | | 0.01 | |
| v/s Ratio Perm | 0.03 | | 0.19 | c0.99 | | | c0.58 | | | 0.03 | | |
| v/c Ratio | 0.08 | 1.20 | 0.43 | 2.45 | 2.42 | | 2.50 | 1.07 | | 0.15 | 0.05 | |
| Uniform Delay, d1 | 36.3 | 24.9 | 17.0 | 26.4 | 20.4 | | 34.6 | 34.6 | | 27.5 | 26.9 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.2 | 102.5 | 2.0 | 662.0 | 642.0 | | 686.7 | 67.4 | | 0.8 | 0.1 | |
| Delay (s) | 36.5 | 127.4 | 19.0 | 688.4 | 662.4 | | 721.3 | 102.0 | | 28.4 | 27.0 | |
| Level of Service | D | F | B | F | F | | F | F | | C | C | |
| Approach Delay (s) | | 94.8 | | | 669.0 | | | 438.4 | | | 27.3 | |
| Approach LOS | | F | | | F | | | F | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|--------|---------------------------|------|
| HCM 2000 Control Delay | 476.9 | HCM 2000 Level of Service | F |
| HCM 2000 Volume to Capacity ratio | 2.42 | | |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) | 16.1 |
| Intersection Capacity Utilization | 162.5% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

Intersection: 3: Klein & Walnut

| Movement | EB | EB | NB | NB |
|-----------------------|-----|-----|-----|-----|
| Directions Served | L | R | L | T |
| Maximum Queue (ft) | 351 | 399 | 285 | 410 |
| Average Queue (ft) | 338 | 246 | 258 | 344 |
| 95th Queue (ft) | 354 | 496 | 360 | 501 |
| Link Distance (ft) | 336 | 336 | | 347 |
| Upstream Blk Time (%) | 97 | 66 | | 56 |
| Queuing Penalty (veh) | 0 | 0 | | 0 |
| Storage Bay Dist (ft) | | | 260 | |
| Storage Blk Time (%) | | | 19 | 45 |
| Queuing Penalty (veh) | | | 150 | 219 |

Intersection: 5: Klein & Roadrunner/Stoeger

| Movement | EB | WB | NB | SB |
|-----------------------|-----|-----|------|-----|
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 548 | 471 | 3005 | 94 |
| Average Queue (ft) | 360 | 344 | 2316 | 12 |
| 95th Queue (ft) | 691 | 597 | 4074 | 49 |
| Link Distance (ft) | 532 | 456 | 2995 | 664 |
| Upstream Blk Time (%) | 44 | 42 | 15 | |
| Queuing Penalty (veh) | 0 | 0 | 134 | |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 8: Klein & Dove Crossing

| Movement | EB | EB | NB |
|-----------------------|-----|-----|-----|
| Directions Served | L | R | LT |
| Maximum Queue (ft) | 624 | 175 | 679 |
| Average Queue (ft) | 460 | 55 | 651 |
| 95th Queue (ft) | 814 | 177 | 784 |
| Link Distance (ft) | 608 | | 664 |
| Upstream Blk Time (%) | 52 | | 33 |
| Queuing Penalty (veh) | 0 | | 365 |
| Storage Bay Dist (ft) | | 150 | |
| Storage Blk Time (%) | 76 | 0 | |
| Queuing Penalty (veh) | 63 | 0 | |

Intersection: 10: Klein & FM 725/FM725

| Movement | EB | EB | EB | WB | WB | NB | NB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|------|-----|
| Directions Served | L | T | R | L | TR | L | TR | TR |
| Maximum Queue (ft) | 30 | 433 | 175 | 95 | 437 | 225 | 1260 | 53 |
| Average Queue (ft) | 3 | 405 | 150 | 87 | 403 | 224 | 1252 | 17 |
| 95th Queue (ft) | 18 | 425 | 223 | 107 | 429 | 225 | 1261 | 43 |
| Link Distance (ft) | | 381 | | | 374 | | 1243 | 403 |
| Upstream Blk Time (%) | | 43 | | | 50 | | 37 | |
| Queuing Penalty (veh) | | 0 | | | 0 | | 408 | |
| Storage Bay Dist (ft) | 120 | | 150 | 70 | | 200 | | |
| Storage Blk Time (%) | | 43 | 0 | 35 | 29 | 80 | 3 | |
| Queuing Penalty (veh) | | 150 | 3 | 659 | 122 | 374 | 24 | |

Network Summary

Network wide Queuing Penalty: 2672

HCM Unsignalized Intersection Capacity Analysis

3: Klein & Walnut

Future (No Build) MID
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|------|------|-------|------|----------------------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 108 | 131 | 99 | 240 | 199 | 117 |
| Future Volume (Veh/h) | 108 | 131 | 99 | 240 | 199 | 117 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.71 | 0.80 | 0.65 | 0.82 | 0.65 | 0.71 |
| Hourly flow rate (vph) | 152 | 164 | 152 | 293 | 306 | 165 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 986 | 388 | 471 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 986 | 388 | 471 | | | |
| tC, single (s) | 6.4 | 6.2 | 4.1 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | |
| p0 queue free % | 35 | 75 | 86 | | | |
| cM capacity (veh/h) | 234 | 655 | 1086 | | | |
| Direction, Lane # | EB 1 | EB 2 | NB 1 | NB 2 | SB 1 | |
| Volume Total | 152 | 164 | 152 | 293 | 471 | |
| Volume Left | 152 | 0 | 152 | 0 | 0 | |
| Volume Right | 0 | 164 | 0 | 0 | 165 | |
| cSH | 234 | 655 | 1086 | 1700 | 1700 | |
| Volume to Capacity | 0.65 | 0.25 | 0.14 | 0.17 | 0.28 | |
| Queue Length 95th (ft) | 100 | 25 | 12 | 0 | 0 | |
| Control Delay (s) | 44.9 | 12.3 | 8.9 | 0.0 | 0.0 | |
| Lane LOS | E | B | A | | | |
| Approach Delay (s) | 28.0 | | 3.0 | | 0.0 | |
| Approach LOS | D | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 8.3 | | | |
| Intersection Capacity Utilization | | | 39.1% | | ICU Level of Service | A |
| Analysis Period (min) | | | 15 | | | |

HCM Unsignalized Intersection Capacity Analysis
5: Klein & Roadrunner/Stoeger

Future (No Build) MID
07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------------|-------------|-------------|-------------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Volume (veh/h) | 18 | 2 | 4 | 3 | 2 | 42 | 5 | 342 | 6 | 24 | 299 | 10 |
| Future Volume (Veh/h) | 18 | 2 | 4 | 3 | 2 | 42 | 5 | 342 | 6 | 24 | 299 | 10 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.56 | 0.25 | 0.50 | 0.25 | 0.25 | 0.58 | 0.42 | 0.70 | 0.50 | 0.67 | 0.85 | 0.50 |
| Hourly flow rate (vph) | 32 | 8 | 8 | 12 | 8 | 72 | 12 | 489 | 12 | 36 | 352 | 20 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | None | | | None | |
| Median storage (veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 1029 | 959 | 362 | 965 | 963 | 495 | 372 | | | 501 | | |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 1029 | 959 | 362 | 965 | 963 | 495 | 372 | | | 501 | | |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 82 | 97 | 99 | 95 | 97 | 87 | 99 | | | 97 | | |
| cM capacity (veh/h) | 175 | 246 | 683 | 218 | 244 | 575 | 1186 | | | 1063 | | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 48 | 92 | 513 | 408 | | | | | | | | |
| Volume Left | 32 | 12 | 12 | 36 | | | | | | | | |
| Volume Right | 8 | 72 | 12 | 20 | | | | | | | | |
| cSH | 211 | 432 | 1186 | 1063 | | | | | | | | |
| Volume to Capacity | 0.23 | 0.21 | 0.01 | 0.03 | | | | | | | | |
| Queue Length 95th (ft) | 21 | 20 | 1 | 3 | | | | | | | | |
| Control Delay (s) | 27.0 | 15.6 | 0.3 | 1.1 | | | | | | | | |
| Lane LOS | D | C | A | A | | | | | | | | |
| Approach Delay (s) | 27.0 | 15.6 | 0.3 | 1.1 | | | | | | | | |
| Approach LOS | D | C | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 3.1 | | | | | | | | | |
| Intersection Capacity Utilization | | | 45.3% | | ICU Level of Service | | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis
8: Klein & Dove Crossing

Future (No Build) MID
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|-------------|-------------|-------------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 41 | 7 | 9 | 419 | 330 | 40 |
| Future Volume (Veh/h) | 41 | 7 | 9 | 419 | 330 | 40 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.47 | 0.58 | 0.45 | 0.85 | 0.83 | 0.50 |
| Hourly flow rate (vph) | 87 | 12 | 20 | 493 | 398 | 80 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | 6 | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 971 | 438 | 478 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 971 | 438 | 478 | | | |
| tC, single (s) | 6.4 | 6.2 | 4.1 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | |
| p0 queue free % | 68 | 98 | 98 | | | |
| cM capacity (veh/h) | 275 | 619 | 1084 | | | |
| Direction, Lane # | EB 1 | NB 1 | SB 1 | | | |
| Volume Total | 99 | 513 | 478 | | | |
| Volume Left | 87 | 20 | 0 | | | |
| Volume Right | 12 | 0 | 80 | | | |
| cSH | 313 | 1084 | 1700 | | | |
| Volume to Capacity | 0.32 | 0.02 | 0.28 | | | |
| Queue Length 95th (ft) | 33 | 1 | 0 | | | |
| Control Delay (s) | 22.4 | 0.5 | 0.0 | | | |
| Lane LOS | C | A | | | | |
| Approach Delay (s) | 22.4 | 0.5 | 0.0 | | | |
| Approach LOS | C | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 2.3 | | | |
| Intersection Capacity Utilization | | | 39.3% | ICU Level of Service | A | |
| Analysis Period (min) | | | 15 | | | |

HCM Signalized Intersection Capacity Analysis
 10: Klein & FM 725/FM725

Future (No Build) MID
 07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|-------|-------|------|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 27 | 1215 | 307 | 88 | 1256 | 9 | 352 | 3 | 134 | 3 | 0 | 15 |
| Future Volume (vph) | 27 | 1215 | 307 | 88 | 1256 | 9 | 352 | 3 | 134 | 3 | 0 | 15 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.86 | | 1.00 | 0.85 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1687 | 1792 | 1524 | 1671 | 1758 | | 1703 | 1589 | | 1770 | 1583 | |
| Flt Permitted | 0.09 | 1.00 | 1.00 | 0.08 | 1.00 | | 0.74 | 1.00 | | 0.61 | 1.00 | |
| Satd. Flow (perm) | 163 | 1792 | 1524 | 147 | 1758 | | 1329 | 1589 | | 1140 | 1583 | |
| Peak-hour factor, PHF | 0.56 | 0.92 | 0.87 | 0.76 | 0.89 | 0.75 | 0.91 | 0.25 | 0.88 | 0.25 | 1.00 | 0.63 |
| Adj. Flow (vph) | 48 | 1321 | 353 | 116 | 1411 | 12 | 387 | 12 | 152 | 12 | 0 | 24 |
| RTOR Reduction (vph) | 0 | 0 | 69 | 0 | 0 | 0 | 0 | 110 | 0 | 0 | 17 | 0 |
| Lane Group Flow (vph) | 48 | 1321 | 284 | 116 | 1423 | 0 | 387 | 54 | 0 | 12 | 7 | 0 |
| Heavy Vehicles (%) | 7% | 6% | 6% | 8% | 8% | 2% | 6% | 2% | 3% | 2% | 2% | 2% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | 4 |
| Permitted Phases | 2 | | 2 | 6 | | | 8 | 8 | | 4 | 4 | |
| Actuated Green, G (s) | 47.7 | 43.5 | 43.5 | 56.5 | 47.9 | | 25.8 | 25.8 | | 25.8 | 25.8 | |
| Effective Green, g (s) | 47.7 | 43.5 | 43.5 | 56.5 | 47.9 | | 25.8 | 25.8 | | 25.8 | 25.8 | |
| Actuated g/C Ratio | 0.51 | 0.46 | 0.46 | 0.60 | 0.51 | | 0.27 | 0.27 | | 0.27 | 0.27 | |
| Clearance Time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 150 | 829 | 705 | 227 | 895 | | 364 | 436 | | 312 | 434 | |
| v/s Ratio Prot | 0.01 | 0.74 | | c0.05 | c0.81 | | | 0.03 | | | 0.00 | |
| v/s Ratio Perm | 0.15 | | 0.19 | 0.26 | | | c0.29 | | | 0.01 | | |
| v/c Ratio | 0.32 | 1.59 | 0.40 | 0.51 | 1.59 | | 1.06 | 0.12 | | 0.04 | 0.02 | |
| Uniform Delay, d1 | 20.3 | 25.2 | 16.7 | 19.0 | 23.1 | | 34.1 | 25.6 | | 25.0 | 24.8 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.2 | 272.8 | 0.4 | 1.9 | 270.5 | | 64.9 | 0.1 | | 0.1 | 0.0 | |
| Delay (s) | 21.5 | 298.0 | 17.1 | 21.0 | 293.6 | | 99.0 | 25.7 | | 25.1 | 24.9 | |
| Level of Service | C | F | B | C | F | | F | C | | C | C | |
| Approach Delay (s) | | 232.7 | | | 273.0 | | | 77.2 | | | 24.9 | |
| Approach LOS | | F | | | F | | | E | | | C | |

| Intersection Summary | | |
|-----------------------------------|--------|-----------------------------|
| HCM 2000 Control Delay | 224.6 | HCM 2000 Level of Service F |
| HCM 2000 Volume to Capacity ratio | 1.37 | |
| Actuated Cycle Length (s) | 94.0 | Sum of lost time (s) 16.1 |
| Intersection Capacity Utilization | 108.4% | ICU Level of Service G |
| Analysis Period (min) | 15 | |
| c Critical Lane Group | | |

Intersection: 3: Klein & Walnut

| Movement | EB | EB | NB |
|-----------------------|-----|-----|-----|
| Directions Served | L | R | L |
| Maximum Queue (ft) | 75 | 56 | 53 |
| Average Queue (ft) | 39 | 35 | 13 |
| 95th Queue (ft) | 62 | 50 | 40 |
| Link Distance (ft) | 336 | 336 | |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | | 260 |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: Klein & Roadrunner/Stoeger

| Movement | EB | WB | SB |
|-----------------------|-----|-----|-----|
| Directions Served | LTR | LTR | LTR |
| Maximum Queue (ft) | 31 | 56 | 29 |
| Average Queue (ft) | 14 | 32 | 5 |
| 95th Queue (ft) | 39 | 60 | 23 |
| Link Distance (ft) | 532 | 456 | 664 |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 8: Klein & Dove Crossing

| Movement | EB | EB | NB |
|-----------------------|-----|-----|-----|
| Directions Served | L | R | LT |
| Maximum Queue (ft) | 51 | 31 | 77 |
| Average Queue (ft) | 27 | 7 | 5 |
| 95th Queue (ft) | 47 | 28 | 30 |
| Link Distance (ft) | 608 | | 664 |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | 150 | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 10: Klein & FM 725/FM725

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|------|-----|-----|
| Directions Served | L | T | R | L | TR | L | TR | L | TR |
| Maximum Queue (ft) | 145 | 444 | 175 | 94 | 437 | 224 | 371 | 30 | 53 |
| Average Queue (ft) | 26 | 408 | 127 | 52 | 401 | 170 | 121 | 2 | 8 |
| 95th Queue (ft) | 86 | 427 | 239 | 101 | 426 | 243 | 298 | 14 | 32 |
| Link Distance (ft) | | 381 | | | 374 | | 1243 | | 403 |
| Upstream Blk Time (%) | | 44 | | | 47 | | | | |
| Queuing Penalty (veh) | | 0 | | | 0 | | | | |
| Storage Bay Dist (ft) | 120 | | 150 | 70 | | 200 | | 120 | |
| Storage Blk Time (%) | | 40 | 0 | 6 | 39 | 8 | | | |
| Queuing Penalty (veh) | | 135 | 3 | 75 | 34 | 11 | | | |

Network Summary

Network wide Queuing Penalty: 259

HCM Unsignalized Intersection Capacity Analysis

3: Klein & Walnut

Future (No Build) PM
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|--------|-------|--------|------|----------------------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 432 | 383 | 158 | 372 | 509 | 229 |
| Future Volume (Veh/h) | 432 | 383 | 158 | 372 | 509 | 229 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.84 | 0.53 | 0.90 | 0.94 | 0.68 | 0.83 |
| Hourly flow rate (vph) | 514 | 723 | 176 | 396 | 749 | 276 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 1635 | 887 | 1025 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 1635 | 887 | 1025 | | | |
| tC, single (s) | 6.4 | 6.2 | 4.1 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | |
| p0 queue free % | 0 | 0 | 74 | | | |
| cM capacity (veh/h) | 82 | 343 | 677 | | | |
| Direction, Lane # | EB 1 | EB 2 | NB 1 | NB 2 | SB 1 | |
| Volume Total | 514 | 723 | 176 | 396 | 1025 | |
| Volume Left | 514 | 0 | 176 | 0 | 0 | |
| Volume Right | 0 | 723 | 0 | 0 | 276 | |
| cSH | 82 | 343 | 677 | 1700 | 1700 | |
| Volume to Capacity | 6.25 | 2.11 | 0.26 | 0.23 | 0.60 | |
| Queue Length 95th (ft) | Err | 1316 | 26 | 0 | 0 | |
| Control Delay (s) | Err | 533.1 | 12.2 | 0.0 | 0.0 | |
| Lane LOS | F | F | B | | | |
| Approach Delay (s) | 4466.4 | | 3.7 | | 0.0 | |
| Approach LOS | F | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 1950.3 | | | |
| Intersection Capacity Utilization | | | 83.4% | | ICU Level of Service | E |
| Analysis Period (min) | | | 15 | | | |

HCM Unsignalized Intersection Capacity Analysis
5: Klein & Roadrunner/Stoeger

Future (No Build) PM
07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|-------|----------------------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↕ | | | ↕ | | | ↕ | | | ↕ | |
| Traffic Volume (veh/h) | 17 | 0 | 13 | 0 | 3 | 21 | 15 | 664 | 9 | 65 | 828 | 56 |
| Future Volume (Veh/h) | 17 | 0 | 13 | 0 | 3 | 21 | 15 | 664 | 9 | 65 | 828 | 56 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.71 | 1.00 | 0.30 | 1.00 | 0.25 | 0.58 | 0.63 | 0.90 | 0.75 | 0.81 | 0.73 | 0.64 |
| Hourly flow rate (vph) | 24 | 0 | 43 | 0 | 12 | 36 | 24 | 738 | 12 | 80 | 1134 | 88 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | | | | | |
| | | | | | | | | None | | | None | |
| Median storage veh | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 2172 | 2136 | 1178 | 2173 | 2174 | 744 | 1222 | | | 750 | | |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 2172 | 2136 | 1178 | 2173 | 2174 | 744 | 1222 | | | 750 | | |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.2 | | | 4.1 | | |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.3 | | | 2.2 | | |
| p0 queue free % | 0 | 100 | 81 | 100 | 70 | 91 | 96 | | | 91 | | |
| cM capacity (veh/h) | 21 | 43 | 232 | 25 | 40 | 415 | 557 | | | 859 | | |
| Direction, Lane # | | | | | | | | | | | | |
| | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 67 | 48 | 774 | 1302 | | | | | | | | |
| Volume Left | 24 | 0 | 24 | 80 | | | | | | | | |
| Volume Right | 43 | 36 | 12 | 88 | | | | | | | | |
| cSH | 51 | 125 | 557 | 859 | | | | | | | | |
| Volume to Capacity | 1.31 | 0.38 | 0.04 | 0.09 | | | | | | | | |
| Queue Length 95th (ft) | 152 | 40 | 3 | 8 | | | | | | | | |
| Control Delay (s) | 359.6 | 50.8 | 1.2 | 3.6 | | | | | | | | |
| Lane LOS | F | F | A | A | | | | | | | | |
| Approach Delay (s) | 359.6 | 50.8 | 1.2 | 3.6 | | | | | | | | |
| Approach LOS | F | F | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 14.7 | | | | | | | | | |
| Intersection Capacity Utilization | | | 95.6% | ICU Level of Service | | | | | | F | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis
8: Klein & Dove Crossing

Future (No Build) PM
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-----------------------------------|-------------|-------------|-------------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 66 | 51 | 21 | 638 | 866 | 114 |
| Future Volume (Veh/h) | 66 | 51 | 21 | 638 | 866 | 114 |
| Sign Control | Stop | | | Free | Free | |
| Grade | 0% | | | 0% | 0% | |
| Peak Hour Factor | 0.87 | 0.67 | 0.88 | 0.92 | 0.81 | 0.68 |
| Hourly flow rate (vph) | 76 | 76 | 24 | 693 | 1069 | 168 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | 6 | | | | | |
| Median type | | | | None | None | |
| Median storage (veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 1894 | 1153 | 1237 | | | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 1894 | 1153 | 1237 | | | |
| tC, single (s) | 6.4 | 6.3 | 4.2 | | | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.4 | 2.3 | | | |
| p0 queue free % | 0 | 68 | 96 | | | |
| cM capacity (veh/h) | 73 | 236 | 540 | | | |
| Direction, Lane # | EB 1 | NB 1 | SB 1 | | | |
| Volume Total | 152 | 717 | 1237 | | | |
| Volume Left | 76 | 24 | 0 | | | |
| Volume Right | 76 | 0 | 168 | | | |
| cSH | 147 | 540 | 1700 | | | |
| Volume to Capacity | 1.04 | 0.04 | 0.73 | | | |
| Queue Length 95th (ft) | 197 | 3 | 0 | | | |
| Control Delay (s) | 120.8 | 1.3 | 0.0 | | | |
| Lane LOS | F | A | | | | |
| Approach Delay (s) | 120.8 | 1.3 | 0.0 | | | |
| Approach LOS | F | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 9.1 | | | |
| Intersection Capacity Utilization | | | 62.8% | ICU Level of Service | B | |
| Analysis Period (min) | | | 15 | | | |

HCM Signalized Intersection Capacity Analysis
 10: Klein & FM 725/FM725

Future (No Build) PM
 07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|--------|------|-------|-------|------|-------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 42 | 1983 | 632 | 443 | 1764 | 12 | 383 | 12 | 362 | 9 | 3 | 18 |
| Future Volume (vph) | 42 | 1983 | 632 | 443 | 1764 | 12 | 383 | 12 | 362 | 9 | 3 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.86 | | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1736 | 1810 | 1583 | 1736 | 1824 | | 1770 | 1570 | | 1770 | 1653 | |
| Flt Permitted | 0.16 | 1.00 | 1.00 | 0.17 | 1.00 | | 0.73 | 1.00 | | 0.19 | 1.00 | |
| Satd. Flow (perm) | 297 | 1810 | 1583 | 303 | 1824 | | 1352 | 1570 | | 358 | 1653 | |
| Peak-hour factor, PHF | 0.58 | 0.87 | 0.93 | 0.88 | 0.93 | 0.50 | 0.80 | 0.50 | 0.92 | 0.38 | 0.25 | 0.50 |
| Adj. Flow (vph) | 72 | 2279 | 680 | 503 | 1897 | 24 | 479 | 24 | 393 | 24 | 12 | 36 |
| RTOR Reduction (vph) | 0 | 0 | 84 | 0 | 1 | 0 | 0 | 302 | 0 | 0 | 28 | 0 |
| Lane Group Flow (vph) | 72 | 2279 | 596 | 503 | 1920 | 0 | 479 | 115 | 0 | 24 | 20 | 0 |
| Heavy Vehicles (%) | 4% | 5% | 2% | 4% | 4% | 2% | 2% | 2% | 4% | 2% | 2% | 2% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | | Perm | NA | | Perm | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | | 4 |
| Permitted Phases | 2 | | 2 | 6 | | | 8 | 8 | | 4 | | 4 |
| Actuated Green, G (s) | 34.8 | 34.3 | 34.3 | 42.9 | 42.9 | | 20.8 | 20.8 | | 20.8 | 20.8 | |
| Effective Green, g (s) | 34.8 | 34.3 | 34.3 | 42.9 | 42.9 | | 20.8 | 20.8 | | 20.8 | 20.8 | |
| Actuated g/C Ratio | 0.39 | 0.38 | 0.38 | 0.48 | 0.48 | | 0.23 | 0.23 | | 0.23 | 0.23 | |
| Clearance Time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | | 5.2 | 5.2 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 277 | 689 | 603 | 443 | 869 | | 312 | 362 | | 82 | 382 | |
| v/s Ratio Prot | 0.03 | c1.26 | | 0.24 | c1.05 | | | 0.07 | | | 0.01 | |
| v/s Ratio Perm | 0.07 | | 0.38 | 0.30 | | | c0.35 | | | 0.07 | | |
| v/c Ratio | 0.26 | 3.31 | 0.99 | 1.14 | 2.21 | | 1.54 | 0.32 | | 0.29 | 0.05 | |
| Uniform Delay, d1 | 32.3 | 27.9 | 27.7 | 24.9 | 23.6 | | 34.6 | 28.7 | | 28.5 | 26.9 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.5 | 1042.2 | 34.1 | 85.3 | 548.3 | | 256.4 | 0.5 | | 2.0 | 0.1 | |
| Delay (s) | 32.8 | 1070.0 | 61.8 | 110.2 | 571.8 | | 291.0 | 29.2 | | 30.5 | 27.0 | |
| Level of Service | C | F | E | F | F | | F | C | | C | C | |
| Approach Delay (s) | | 819.2 | | | 476.0 | | | 169.2 | | | 28.2 | |
| Approach LOS | | F | | | F | | | F | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|--------|---------------------------|------|
| HCM 2000 Control Delay | 590.1 | HCM 2000 Level of Service | F |
| HCM 2000 Volume to Capacity ratio | 2.61 | | |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) | 16.1 |
| Intersection Capacity Utilization | 170.2% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

Intersection: 3: Klein & Walnut

| Movement | EB | EB | NB |
|-----------------------|-----|-----|-----|
| Directions Served | L | R | L |
| Maximum Queue (ft) | 388 | 388 | 53 |
| Average Queue (ft) | 354 | 354 | 29 |
| 95th Queue (ft) | 368 | 369 | 57 |
| Link Distance (ft) | 336 | 336 | |
| Upstream Blk Time (%) | 95 | 73 | |
| Queuing Penalty (veh) | 0 | 0 | |
| Storage Bay Dist (ft) | | | 260 |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 5: Klein & Roadrunner/Stoeger

| Movement | EB | WB | NB | SB |
|-----------------------|-----|-----|------|-----|
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 56 | 52 | 75 | 97 |
| Average Queue (ft) | 26 | 16 | 10 | 20 |
| 95th Queue (ft) | 50 | 42 | 49 | 68 |
| Link Distance (ft) | 532 | 456 | 2995 | 664 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 8: Klein & Dove Crossing

| Movement | EB | EB | NB |
|-----------------------|-----|-----|-----|
| Directions Served | L | R | LT |
| Maximum Queue (ft) | 74 | 79 | 114 |
| Average Queue (ft) | 30 | 32 | 9 |
| 95th Queue (ft) | 60 | 58 | 50 |
| Link Distance (ft) | 608 | | 664 |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | 150 | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 10: Klein & FM 725/FM725

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|------|-----|-----|
| Directions Served | L | T | R | L | TR | L | TR | L | TR |
| Maximum Queue (ft) | 140 | 420 | 175 | 95 | 426 | 225 | 756 | 71 | 52 |
| Average Queue (ft) | 18 | 400 | 132 | 91 | 397 | 205 | 338 | 8 | 12 |
| 95th Queue (ft) | 75 | 414 | 240 | 107 | 417 | 255 | 648 | 34 | 39 |
| Link Distance (ft) | | 381 | | | 374 | | 1243 | | 403 |
| Upstream Blk Time (%) | | 51 | | | 53 | | | | |
| Queuing Penalty (veh) | | 0 | | | 0 | | | | |
| Storage Bay Dist (ft) | 120 | | 150 | 70 | | 200 | | 120 | |
| Storage Blk Time (%) | | 48 | 0 | 40 | 28 | 36 | 8 | | |
| Queuing Penalty (veh) | | 324 | 4 | 710 | 126 | 133 | 32 | | |

Network Summary

Network wide Queuing Penalty: 1329

APPENDIX C6

HCM Signalized Intersection Capacity Analysis

3: Walnut & Klein

Future (Proposed) AM
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|------------------------|-------|------|-------|-------|-------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 119 | 465 | 491 | 785 | 930 | 281 |
| Future Volume (vph) | 119 | 465 | 491 | 785 | 930 | 281 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.5 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 0.95 | 0.95 | 1.00 |
| Frt | 0.91 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.98 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3181 | 1427 | 1736 | 3471 | 3471 | 1568 |
| Flt Permitted | 0.98 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3181 | 1427 | 1736 | 3471 | 3471 | 1568 |
| Peak-hour factor, PHF | 0.73 | 0.83 | 0.76 | 0.78 | 0.64 | 0.68 |
| Adj. Flow (vph) | 163 | 560 | 646 | 1006 | 1453 | 413 |
| RTOR Reduction (vph) | 255 | 255 | 0 | 0 | 0 | 78 |
| Lane Group Flow (vph) | 188 | 25 | 646 | 1006 | 1453 | 335 |
| Heavy Vehicles (%) | 3% | 3% | 4% | 4% | 4% | 3% |
| Turn Type | Prot | Prot | Prot | NA | NA | Perm |
| Protected Phases | 2 | 2 | 3 | 8 | 4 | |
| Permitted Phases | | | | | | 4 |
| Actuated Green, G (s) | 10.7 | 10.7 | 43.5 | 101.3 | 53.3 | 53.3 |
| Effective Green, g (s) | 10.7 | 10.7 | 43.5 | 101.3 | 53.3 | 53.3 |
| Actuated g/C Ratio | 0.09 | 0.09 | 0.36 | 0.84 | 0.44 | 0.44 |
| Clearance Time (s) | 4.0 | 4.0 | 4.5 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 283 | 127 | 629 | 2930 | 1541 | 696 |
| v/s Ratio Prot | c0.06 | 0.02 | c0.37 | 0.29 | c0.42 | |
| v/s Ratio Perm | | | | | | 0.21 |
| v/c Ratio | 0.66 | 0.20 | 1.03 | 0.34 | 0.94 | 0.48 |
| Uniform Delay, d1 | 52.9 | 50.7 | 38.2 | 2.1 | 31.9 | 23.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.61 | 0.51 |
| Incremental Delay, d2 | 5.8 | 0.8 | 43.0 | 0.1 | 11.4 | 0.5 |
| Delay (s) | 58.7 | 51.4 | 81.2 | 2.1 | 30.9 | 12.4 |
| Level of Service | E | D | F | A | C | B |
| Approach Delay (s) | 55.9 | | | 33.0 | 26.8 | |
| Approach LOS | E | | | C | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 34.2 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.95 | | |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | 12.5 |
| Intersection Capacity Utilization | 71.2% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Unsignalized Intersection Capacity Analysis
5: Klein & Roadrunner/Stoeger

Future (Proposed) AM
07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|------|-------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | ↕ | | | ↕ | | ↕ | ↕ | | ↕ | ↕ | |
| Traffic Volume (veh/h) | 51 | 0 | 21 | 21 | 0 | 71 | 12 | 993 | 12 | 27 | 933 | 8 |
| Future Volume (Veh/h) | 51 | 0 | 21 | 21 | 0 | 71 | 12 | 993 | 12 | 27 | 933 | 8 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.67 | 1.00 | 0.66 | 0.58 | 1.00 | 0.51 | 0.60 | 0.79 | 0.50 | 0.45 | 0.79 | 0.67 |
| Hourly flow rate (vph) | 76 | 0 | 32 | 36 | 0 | 139 | 20 | 1257 | 24 | 60 | 1181 | 12 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | | | | | |
| Median storage veh | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 2114 | 2628 | 596 | 2052 | 2622 | 640 | 1193 | | | 1281 | | |
| vC1, stage 1 conf vol | 1307 | 1307 | | 1309 | 1309 | | | | | | | |
| vC2, stage 2 conf vol | 808 | 1321 | | 742 | 1313 | | | | | | | |
| vCu, unblocked vol | 2114 | 2628 | 596 | 2052 | 2622 | 640 | 1193 | | | 1281 | | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | 6.5 | 5.5 | | 6.5 | 5.5 | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 28 | 100 | 93 | 74 | 100 | 67 | 97 | | | 89 | | |
| cM capacity (veh/h) | 106 | 121 | 446 | 139 | 135 | 418 | 581 | | | 538 | | |
| Direction, Lane # | | | | | | | | | | | | |
| | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 | | | | |
| Volume Total | 108 | 175 | 20 | 838 | 443 | 60 | 787 | 406 | | | | |
| Volume Left | 76 | 36 | 20 | 0 | 0 | 60 | 0 | 0 | | | | |
| Volume Right | 32 | 139 | 0 | 0 | 24 | 0 | 0 | 12 | | | | |
| cSH | 137 | 295 | 581 | 1700 | 1700 | 538 | 1700 | 1700 | | | | |
| Volume to Capacity | 0.79 | 0.59 | 0.03 | 0.49 | 0.26 | 0.11 | 0.46 | 0.24 | | | | |
| Queue Length 95th (ft) | 120 | 88 | 3 | 0 | 0 | 9 | 0 | 0 | | | | |
| Control Delay (s) | 91.1 | 33.5 | 11.4 | 0.0 | 0.0 | 12.5 | 0.0 | 0.0 | | | | |
| Lane LOS | F | D | B | | | B | | | | | | |
| Approach Delay (s) | 91.1 | 33.5 | 0.2 | | | 0.6 | | | | | | |
| Approach LOS | F | D | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 5.9 | | | | | | | | | |
| Intersection Capacity Utilization | | | 45.0% | | ICU Level of Service | | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis
8: Klein & Dove Crossing

Future (Proposed) AM
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
|-----------------------------------|------|------|-------|----------------------|------|------|------|
| Lane Configurations | | | | | | | |
| Traffic Volume (veh/h) | 86 | 83 | 45 | 1021 | 787 | 30 | |
| Future Volume (Veh/h) | 86 | 83 | 45 | 1021 | 787 | 30 | |
| Sign Control | Stop | | | Free | Free | | |
| Grade | 0% | | | 0% | 0% | | |
| Peak Hour Factor | 0.83 | 0.83 | 0.66 | 0.81 | 0.80 | 0.54 | |
| Hourly flow rate (vph) | 104 | 100 | 68 | 1260 | 984 | 56 | |
| Pedestrians | | | | | | | |
| Lane Width (ft) | | | | | | | |
| Walking Speed (ft/s) | | | | | | | |
| Percent Blockage | | | | | | | |
| Right turn flare (veh) | | | | | | | |
| Median type | | | | | | | |
| TWLTL TWLTL | | | | | | | |
| Median storage veh | | | | | | | |
| 2 2 | | | | | | | |
| Upstream signal (ft) | | | | | | | |
| pX, platoon unblocked | | | | | | | |
| vC, conflicting volume | 1778 | 520 | 1040 | | | | |
| vC1, stage 1 conf vol | 1012 | | | | | | |
| vC2, stage 2 conf vol | 766 | | | | | | |
| vCu, unblocked vol | 1778 | 520 | 1040 | | | | |
| tC, single (s) | 6.8 | 6.9 | 4.1 | | | | |
| tC, 2 stage (s) | 5.8 | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | | |
| p0 queue free % | 57 | 80 | 90 | | | | |
| cM capacity (veh/h) | 242 | 501 | 664 | | | | |
| Direction, Lane # | EB 1 | EB 2 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |
| Volume Total | 104 | 100 | 68 | 630 | 630 | 656 | 384 |
| Volume Left | 104 | 0 | 68 | 0 | 0 | 0 | 0 |
| Volume Right | 0 | 100 | 0 | 0 | 0 | 0 | 56 |
| cSH | 242 | 501 | 664 | 1700 | 1700 | 1700 | 1700 |
| Volume to Capacity | 0.43 | 0.20 | 0.10 | 0.37 | 0.37 | 0.39 | 0.23 |
| Queue Length 95th (ft) | 51 | 18 | 9 | 0 | 0 | 0 | 0 |
| Control Delay (s) | 30.6 | 14.0 | 11.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Lane LOS | D | B | B | | | | |
| Approach Delay (s) | 22.4 | | 0.6 | | | 0.0 | |
| Approach LOS | C | | | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 2.1 | | | | |
| Intersection Capacity Utilization | | | 40.8% | ICU Level of Service | | A | |
| Analysis Period (min) | | | 15 | | | | |

HCM Signalized Intersection Capacity Analysis
10: Klein & FM 725

Future (Proposed) AM
07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|-------|-------|------|-------|------|------|-------|-------|------|
| Lane Configurations | ↙ | ↑↑↑ | ↗ | ↙↗ | ↑↑↑ | | ↙↗ | ↑ | ↗ | ↙ | ↑ | |
| Traffic Volume (vph) | 6 | 869 | 344 | 421 | 1895 | 6 | 704 | 6 | 460 | 3 | 6 | 24 |
| Future Volume (vph) | 6 | 869 | 344 | 421 | 1895 | 6 | 704 | 6 | 460 | 3 | 6 | 24 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.5 | 4.0 | 4.0 | 4.5 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 0.97 | 0.91 | | 0.97 | 0.95 | 0.95 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.86 | 0.85 | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 4848 | 1482 | 3335 | 4845 | | 3400 | 1500 | 1490 | 1770 | 1653 | |
| Flt Permitted | 0.11 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 200 | 4848 | 1482 | 3335 | 4845 | | 3400 | 1500 | 1490 | 1770 | 1653 | |
| Peak-hour factor, PHF | 0.50 | 0.91 | 0.86 | 0.53 | 0.81 | 0.50 | 0.91 | 0.50 | 0.72 | 0.25 | 0.50 | 0.67 |
| Adj. Flow (vph) | 12 | 955 | 400 | 794 | 2340 | 12 | 774 | 12 | 639 | 12 | 12 | 36 |
| RTOR Reduction (vph) | 0 | 0 | 276 | 0 | 0 | 0 | 0 | 234 | 244 | 0 | 35 | 0 |
| Lane Group Flow (vph) | 12 | 955 | 124 | 794 | 2352 | 0 | 774 | 91 | 82 | 12 | 13 | 0 |
| Heavy Vehicles (%) | 2% | 7% | 9% | 5% | 7% | 2% | 3% | 2% | 3% | 2% | 2% | 2% |
| Turn Type | pm+pt | NA | Perm | Prot | NA | | Split | NA | Perm | Split | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | 2 | | 2 | | | | | | 8 | | | |
| Actuated Green, G (s) | 39.2 | 37.2 | 37.2 | 31.5 | 66.7 | | 30.1 | 30.1 | 30.1 | 4.7 | 4.7 | |
| Effective Green, g (s) | 39.2 | 37.2 | 37.2 | 31.5 | 66.7 | | 30.1 | 30.1 | 30.1 | 4.7 | 4.7 | |
| Actuated g/C Ratio | 0.33 | 0.31 | 0.31 | 0.26 | 0.56 | | 0.25 | 0.25 | 0.25 | 0.04 | 0.04 | |
| Clearance Time (s) | 4.5 | 4.0 | 4.0 | 4.5 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 91 | 1502 | 459 | 875 | 2693 | | 852 | 376 | 373 | 69 | 64 | |
| v/s Ratio Prot | 0.00 | 0.20 | | c0.24 | c0.49 | | c0.23 | 0.06 | | 0.01 | c0.01 | |
| v/s Ratio Perm | 0.04 | | 0.08 | | | | | | 0.05 | | | |
| v/c Ratio | 0.13 | 0.64 | 0.27 | 0.91 | 0.87 | | 0.91 | 0.24 | 0.22 | 0.17 | 0.21 | |
| Uniform Delay, d1 | 28.4 | 35.6 | 31.2 | 42.8 | 23.0 | | 43.6 | 35.8 | 35.6 | 55.8 | 55.9 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 0.95 | 0.71 | 0.73 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.7 | 2.1 | 1.4 | 12.9 | 3.4 | | 13.1 | 0.3 | 0.3 | 1.2 | 1.6 | |
| Delay (s) | 29.1 | 37.6 | 32.6 | 55.8 | 26.4 | | 54.6 | 25.8 | 26.2 | 57.0 | 57.5 | |
| Level of Service | C | D | C | E | C | | D | C | C | E | E | |
| Approach Delay (s) | | 36.1 | | | 33.8 | | | 41.5 | | | 57.4 | |
| Approach LOS | | D | | | C | | | D | | | E | |

| Intersection Summary | | |
|-----------------------------------|-------|---------------------------|
| HCM 2000 Control Delay | 36.4 | HCM 2000 Level of Service |
| HCM 2000 Volume to Capacity ratio | 0.88 | D |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) |
| Intersection Capacity Utilization | 78.1% | 16.5 |
| Analysis Period (min) | 15 | ICU Level of Service |
| c Critical Lane Group | | D |

Intersection: 3: Walnut & Klein

| Movement | EB | EB | EB | NB | NB | NB | SB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|------|------|-----|
| Directions Served | L | LR | R | L | T | T | T | T | R |
| Maximum Queue (ft) | 314 | 360 | 175 | 174 | 392 | 320 | 449 | 449 | 125 |
| Average Queue (ft) | 111 | 294 | 172 | 173 | 324 | 165 | 296 | 312 | 108 |
| 95th Queue (ft) | 264 | 372 | 183 | 177 | 448 | 298 | 401 | 415 | 159 |
| Link Distance (ft) | 312 | 312 | | | 340 | 340 | 1098 | 1098 | |
| Upstream Blk Time (%) | 2 | 29 | | | 17 | 0 | | | |
| Queuing Penalty (veh) | 0 | 0 | | | 0 | 0 | | | |
| Storage Bay Dist (ft) | | | 150 | 150 | | | | | 100 |
| Storage Blk Time (%) | | 61 | 17 | 38 | 0 | | 43 | 1 | |
| Queuing Penalty (veh) | | 143 | 49 | 148 | 2 | | 122 | 4 | |

Intersection: 5: Klein & Roadrunner/Stoeger

| Movement | EB | WB | NB | SB |
|-----------------------|-----|-----|-----|-----|
| Directions Served | LTR | LTR | L | L |
| Maximum Queue (ft) | 160 | 78 | 50 | 29 |
| Average Queue (ft) | 62 | 38 | 5 | 10 |
| 95th Queue (ft) | 123 | 66 | 24 | 33 |
| Link Distance (ft) | 514 | 438 | | |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | 150 | 150 |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 8: Klein & Dove Crossing

| Movement | EB | EB | NB | SB |
|-----------------------|-----|-----|-----|------|
| Directions Served | L | R | L | T |
| Maximum Queue (ft) | 227 | 94 | 55 | 48 |
| Average Queue (ft) | 87 | 37 | 17 | 2 |
| 95th Queue (ft) | 183 | 64 | 46 | 16 |
| Link Distance (ft) | 596 | 596 | | 1217 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | 150 | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 10: Klein & FM 725

| Movement | EB | EB | EB | EB | EB | WB | WB | WB | WB | WB | NB | NB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
| Directions Served | L | T | T | T | R | L | L | T | T | TR | L | L |
| Maximum Queue (ft) | 29 | 386 | 333 | 295 | 275 | 262 | 274 | 567 | 491 | 329 | 275 | 444 |
| Average Queue (ft) | 4 | 276 | 216 | 67 | 116 | 178 | 214 | 212 | 212 | 122 | 216 | 252 |
| 95th Queue (ft) | 20 | 386 | 318 | 192 | 211 | 261 | 291 | 368 | 333 | 222 | 302 | 375 |
| Link Distance (ft) | | 371 | 371 | 371 | | | | 552 | 552 | 552 | | 1217 |
| Upstream Blk Time (%) | | 2 | | | | | | 0 | | | | |
| Queuing Penalty (veh) | | 0 | | | | | | 0 | | | | |
| Storage Bay Dist (ft) | 150 | | | | 250 | 250 | 250 | | | | 250 | |
| Storage Blk Time (%) | | 30 | | | 1 | 0 | 3 | 1 | | | 2 | 9 |
| Queuing Penalty (veh) | | 2 | | | 2 | 1 | 18 | 6 | | | 8 | 33 |

Intersection: 10: Klein & FM 725

| Movement | NB | NB | SB | SB |
|-----------------------|------|-----|-----|-----|
| Directions Served | TR | R | L | TR |
| Maximum Queue (ft) | 76 | 106 | 31 | 72 |
| Average Queue (ft) | 50 | 55 | 2 | 21 |
| 95th Queue (ft) | 81 | 86 | 14 | 52 |
| Link Distance (ft) | 1217 | | | 375 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | 150 | 120 | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Network Summary

Network wide Queuing Penalty: 537

HCM Signalized Intersection Capacity Analysis

3: Walnut & Klein

Future (Proposed) MID
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|------------------------|-------|------|-------|------|-------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 108 | 131 | 99 | 240 | 199 | 117 |
| Future Volume (vph) | 108 | 131 | 99 | 240 | 199 | 117 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.5 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 0.95 | 0.95 | 1.00 |
| Frt | 0.96 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.97 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3272 | 1413 | 1752 | 3438 | 3343 | 1524 |
| Flt Permitted | 0.97 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3272 | 1413 | 1752 | 3438 | 3343 | 1524 |
| Peak-hour factor, PHF | 0.71 | 0.80 | 0.65 | 0.82 | 0.65 | 0.71 |
| Adj. Flow (vph) | 152 | 164 | 152 | 293 | 306 | 165 |
| RTOR Reduction (vph) | 46 | 71 | 0 | 0 | 0 | 107 |
| Lane Group Flow (vph) | 170 | 29 | 152 | 293 | 306 | 58 |
| Heavy Vehicles (%) | 4% | 4% | 3% | 5% | 8% | 6% |
| Turn Type | Prot | Prot | Prot | NA | NA | Perm |
| Protected Phases | 2 | 2 | 3 | 8 | 4 | |
| Permitted Phases | | | | | | 4 |
| Actuated Green, G (s) | 17.3 | 17.3 | 9.1 | 34.7 | 21.1 | 21.1 |
| Effective Green, g (s) | 17.3 | 17.3 | 9.1 | 34.7 | 21.1 | 21.1 |
| Actuated g/C Ratio | 0.29 | 0.29 | 0.15 | 0.58 | 0.35 | 0.35 |
| Clearance Time (s) | 4.0 | 4.0 | 4.5 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 943 | 407 | 265 | 1988 | 1175 | 535 |
| v/s Ratio Prot | c0.05 | 0.02 | c0.09 | 0.09 | c0.09 | |
| v/s Ratio Perm | | | | | | 0.04 |
| v/c Ratio | 0.18 | 0.07 | 0.57 | 0.15 | 0.26 | 0.11 |
| Uniform Delay, d1 | 16.0 | 15.5 | 23.6 | 5.8 | 13.9 | 13.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.88 | 0.50 |
| Incremental Delay, d2 | 0.1 | 0.1 | 3.0 | 0.0 | 0.1 | 0.1 |
| Delay (s) | 16.1 | 15.6 | 26.6 | 5.9 | 12.3 | 6.7 |
| Level of Service | B | B | C | A | B | A |
| Approach Delay (s) | 16.0 | | | 13.0 | 10.3 | |
| Approach LOS | B | | | B | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 12.7 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.29 | | |
| Actuated Cycle Length (s) | 60.0 | Sum of lost time (s) | 12.5 |
| Intersection Capacity Utilization | 25.9% | ICU Level of Service | A |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Unsignalized Intersection Capacity Analysis

5: Klein & Roadrunner/Stoeger

Future (Proposed) MID
07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|------|-------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | ↕ | | | ↕ | | ↕ | ↕ | | ↕ | ↕ | |
| Traffic Volume (veh/h) | 18 | 2 | 4 | 3 | 2 | 42 | 5 | 342 | 6 | 24 | 299 | 10 |
| Future Volume (Veh/h) | 18 | 2 | 4 | 3 | 2 | 42 | 5 | 342 | 6 | 24 | 299 | 10 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.56 | 0.25 | 0.50 | 0.25 | 0.25 | 0.58 | 0.42 | 0.70 | 0.50 | 0.67 | 0.85 | 0.50 |
| Hourly flow rate (vph) | 32 | 8 | 8 | 12 | 8 | 72 | 12 | 489 | 12 | 36 | 352 | 20 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | | | | | |
| Median storage veh | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 778 | 959 | 186 | 779 | 963 | 250 | 372 | | | 501 | | |
| vC1, stage 1 conf vol | 434 | 434 | | 519 | 519 | | | | | | | |
| vC2, stage 2 conf vol | 344 | 525 | | 260 | 444 | | | | | | | |
| vCu, unblocked vol | 778 | 959 | 186 | 779 | 963 | 250 | 372 | | | 501 | | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | 6.5 | 5.5 | | 6.5 | 5.5 | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 93 | 98 | 99 | 97 | 98 | 90 | 99 | | | 97 | | |
| cM capacity (veh/h) | 432 | 416 | 824 | 451 | 426 | 749 | 1183 | | | 1059 | | |
| Direction, Lane # | | | | | | | | | | | | |
| | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 | | | | |
| Volume Total | 48 | 92 | 12 | 326 | 175 | 36 | 235 | 137 | | | | |
| Volume Left | 32 | 12 | 12 | 0 | 0 | 36 | 0 | 0 | | | | |
| Volume Right | 8 | 72 | 0 | 0 | 12 | 0 | 0 | 20 | | | | |
| cSH | 466 | 650 | 1183 | 1700 | 1700 | 1059 | 1700 | 1700 | | | | |
| Volume to Capacity | 0.10 | 0.14 | 0.01 | 0.19 | 0.10 | 0.03 | 0.14 | 0.08 | | | | |
| Queue Length 95th (ft) | 9 | 12 | 1 | 0 | 0 | 3 | 0 | 0 | | | | |
| Control Delay (s) | 13.6 | 11.4 | 8.1 | 0.0 | 0.0 | 8.5 | 0.0 | 0.0 | | | | |
| Lane LOS | B | B | A | | | A | | | | | | |
| Approach Delay (s) | 13.6 | 11.4 | 0.2 | | | 0.8 | | | | | | |
| Approach LOS | B | B | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 2.0 | | | | | | | | | |
| Intersection Capacity Utilization | | | 31.0% | | ICU Level of Service | | | A | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

8: Klein & Dove Crossing

Future (Proposed) MID
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
|-----------------------------------|------|------|-------|----------------------|------|------|------|
| Lane Configurations | | | | | | | |
| Traffic Volume (veh/h) | 41 | 7 | 9 | 419 | 330 | 40 | |
| Future Volume (Veh/h) | 41 | 7 | 9 | 419 | 330 | 40 | |
| Sign Control | Stop | | | Free | Free | | |
| Grade | 0% | | | 0% | 0% | | |
| Peak Hour Factor | 0.47 | 0.58 | 0.45 | 0.85 | 0.83 | 0.50 | |
| Hourly flow rate (vph) | 87 | 12 | 20 | 493 | 398 | 80 | |
| Pedestrians | | | | | | | |
| Lane Width (ft) | | | | | | | |
| Walking Speed (ft/s) | | | | | | | |
| Percent Blockage | | | | | | | |
| Right turn flare (veh) | | | | | | | |
| Median type | | | | | | | |
| TWLTL TWLTL | | | | | | | |
| Median storage veh | | | | | | | |
| 2 2 | | | | | | | |
| Upstream signal (ft) | | | | | | | |
| pX, platoon unblocked | | | | | | | |
| vC, conflicting volume | 724 | 239 | 478 | | | | |
| vC1, stage 1 conf vol | 438 | | | | | | |
| vC2, stage 2 conf vol | 286 | | | | | | |
| vCu, unblocked vol | 724 | 239 | 478 | | | | |
| tC, single (s) | 6.8 | 6.9 | 4.1 | | | | |
| tC, 2 stage (s) | 5.8 | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | | |
| p0 queue free % | 84 | 98 | 98 | | | | |
| cM capacity (veh/h) | 544 | 762 | 1081 | | | | |
| Direction, Lane # | EB 1 | EB 2 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |
| Volume Total | 87 | 12 | 20 | 246 | 246 | 265 | 213 |
| Volume Left | 87 | 0 | 20 | 0 | 0 | 0 | 0 |
| Volume Right | 0 | 12 | 0 | 0 | 0 | 0 | 80 |
| cSH | 544 | 762 | 1081 | 1700 | 1700 | 1700 | 1700 |
| Volume to Capacity | 0.16 | 0.02 | 0.02 | 0.14 | 0.14 | 0.16 | 0.13 |
| Queue Length 95th (ft) | 14 | 1 | 1 | 0 | 0 | 0 | 0 |
| Control Delay (s) | 12.9 | 9.8 | 8.4 | 0.0 | 0.0 | 0.0 | 0.0 |
| Lane LOS | B | A | A | | | | |
| Approach Delay (s) | 12.5 | | 0.3 | | | 0.0 | |
| Approach LOS | B | | | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 1.3 | | | | |
| Intersection Capacity Utilization | | | 21.6% | ICU Level of Service | | A | |
| Analysis Period (min) | | | 15 | | | | |

HCM Signalized Intersection Capacity Analysis
10: Klein & FM 725

Future (Proposed) MID
07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|-------|-------|------|-------|------|------|-------|------|------|
| Lane Configurations | ↘ | ↑↑↑ | ↗ | ↘↗ | ↑↑↑ | | ↘↗ | ↑ | ↗ | ↘ | ↑ | |
| Traffic Volume (vph) | 27 | 1215 | 307 | 88 | 1256 | 9 | 352 | 3 | 134 | 3 | 0 | 15 |
| Future Volume (vph) | 27 | 1215 | 307 | 88 | 1256 | 9 | 352 | 3 | 134 | 3 | 0 | 15 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.5 | 4.0 | 4.0 | 4.5 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 0.97 | 0.91 | | 0.97 | 0.95 | 0.95 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.87 | 0.85 | 1.00 | 0.85 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1687 | 4893 | 1524 | 3242 | 4799 | | 3303 | 1530 | 1490 | 1770 | 1583 | |
| Flt Permitted | 0.16 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 277 | 4893 | 1524 | 3242 | 4799 | | 3303 | 1530 | 1490 | 1770 | 1583 | |
| Peak-hour factor, PHF | 0.56 | 0.92 | 0.87 | 0.76 | 0.89 | 0.75 | 0.91 | 0.25 | 0.88 | 0.25 | 1.00 | 0.63 |
| Adj. Flow (vph) | 48 | 1321 | 353 | 116 | 1411 | 12 | 387 | 12 | 152 | 12 | 0 | 24 |
| RTOR Reduction (vph) | 0 | 0 | 202 | 0 | 1 | 0 | 0 | 58 | 67 | 0 | 23 | 0 |
| Lane Group Flow (vph) | 48 | 1321 | 151 | 116 | 1422 | 0 | 387 | 25 | 14 | 12 | 1 | 0 |
| Heavy Vehicles (%) | 7% | 6% | 6% | 8% | 8% | 2% | 6% | 2% | 3% | 2% | 2% | 2% |
| Turn Type | pm+pt | NA | Perm | Prot | NA | | Split | NA | Perm | Split | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | 2 | | 2 | | | | | | 8 | | | |
| Actuated Green, G (s) | 28.6 | 25.6 | 25.6 | 4.9 | 27.5 | | 10.6 | 10.6 | 10.6 | 2.4 | 2.4 | |
| Effective Green, g (s) | 28.6 | 25.6 | 25.6 | 4.9 | 27.5 | | 10.6 | 10.6 | 10.6 | 2.4 | 2.4 | |
| Actuated g/C Ratio | 0.48 | 0.43 | 0.43 | 0.08 | 0.46 | | 0.18 | 0.18 | 0.18 | 0.04 | 0.04 | |
| Clearance Time (s) | 4.5 | 4.0 | 4.0 | 4.5 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 202 | 2087 | 650 | 264 | 2199 | | 583 | 270 | 263 | 70 | 63 | |
| v/s Ratio Prot | 0.01 | 0.27 | | c0.04 | c0.30 | | c0.12 | 0.02 | | c0.01 | 0.00 | |
| v/s Ratio Perm | 0.10 | | 0.10 | | | | | | 0.01 | | | |
| v/c Ratio | 0.24 | 0.63 | 0.23 | 0.44 | 0.65 | | 0.66 | 0.09 | 0.05 | 0.17 | 0.02 | |
| Uniform Delay, d1 | 15.5 | 13.5 | 10.9 | 26.2 | 12.5 | | 23.0 | 20.7 | 20.5 | 27.8 | 27.7 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 0.97 | 1.04 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.6 | 1.5 | 0.8 | 1.2 | 0.7 | | 2.8 | 0.1 | 0.1 | 1.2 | 0.1 | |
| Delay (s) | 16.1 | 15.0 | 11.8 | 27.4 | 13.2 | | 25.2 | 21.7 | 20.6 | 29.0 | 27.8 | |
| Level of Service | B | B | B | C | B | | C | C | C | C | C | |
| Approach Delay (s) | | 14.4 | | | 14.2 | | | 24.0 | | | 28.2 | |
| Approach LOS | | B | | | B | | | C | | | C | |

| Intersection Summary | | |
|-----------------------------------|-------|-----------------------------|
| HCM 2000 Control Delay | 15.8 | HCM 2000 Level of Service B |
| HCM 2000 Volume to Capacity ratio | 0.62 | |
| Actuated Cycle Length (s) | 60.0 | Sum of lost time (s) 16.5 |
| Intersection Capacity Utilization | 55.8% | ICU Level of Service B |
| Analysis Period (min) | 15 | |
| c Critical Lane Group | | |

Intersection: 3: Walnut & Klein

| Movement | EB | EB | NB | NB | NB | SB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|------|------|-----|
| Directions Served | L | LR | L | T | T | T | T | R |
| Maximum Queue (ft) | 88 | 103 | 96 | 108 | 79 | 55 | 133 | 125 |
| Average Queue (ft) | 37 | 41 | 44 | 34 | 15 | 16 | 53 | 45 |
| 95th Queue (ft) | 67 | 79 | 74 | 73 | 50 | 47 | 95 | 85 |
| Link Distance (ft) | 312 | 312 | | 340 | 340 | 1095 | 1095 | |
| Upstream Blk Time (%) | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | |
| Storage Bay Dist (ft) | | | 150 | | | | | 100 |
| Storage Blk Time (%) | | | | | | | 1 | 0 |
| Queuing Penalty (veh) | | | | | | | 1 | 0 |

Intersection: 5: Klein & Roadrunner/Stoeger

| Movement | EB | WB | NB | SB |
|-----------------------|-----|-----|-----|-----|
| Directions Served | LTR | LTR | L | L |
| Maximum Queue (ft) | 31 | 54 | 28 | 52 |
| Average Queue (ft) | 18 | 27 | 2 | 8 |
| 95th Queue (ft) | 42 | 51 | 13 | 31 |
| Link Distance (ft) | 515 | 438 | | |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | 150 | 150 |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 8: Klein & Dove Crossing

| Movement | EB | EB | NB |
|-----------------------|-----|-----|-----|
| Directions Served | L | R | L |
| Maximum Queue (ft) | 53 | 30 | 29 |
| Average Queue (ft) | 26 | 2 | 2 |
| 95th Queue (ft) | 51 | 14 | 14 |
| Link Distance (ft) | 596 | 596 | |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | | 150 |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 10: Klein & FM 725

| Movement | EB | EB | EB | EB | EB | WB | WB | WB | WB | WB | NB | NB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
| Directions Served | L | T | T | T | R | L | L | T | T | TR | L | L |
| Maximum Queue (ft) | 97 | 253 | 208 | 89 | 100 | 123 | 130 | 367 | 213 | 114 | 114 | 158 |
| Average Queue (ft) | 33 | 165 | 106 | 32 | 54 | 10 | 54 | 120 | 77 | 22 | 73 | 92 |
| 95th Queue (ft) | 72 | 243 | 186 | 73 | 88 | 50 | 92 | 237 | 165 | 62 | 114 | 137 |
| Link Distance (ft) | | 371 | 371 | 371 | | | | 352 | 352 | 352 | | 1216 |
| Upstream Blk Time (%) | | | | | | | | 0 | | | | |
| Queuing Penalty (veh) | | | | | | | | 0 | | | | |
| Storage Bay Dist (ft) | 150 | | | | 250 | 250 | 250 | | | | 250 | |
| Storage Blk Time (%) | | 8 | | | | | | 1 | | | | |
| Queuing Penalty (veh) | | 2 | | | | | | 1 | | | | |

Intersection: 10: Klein & FM 725

| Movement | NB | NB | SB | SB |
|-----------------------|------|-----|-----|-----|
| Directions Served | TR | R | L | TR |
| Maximum Queue (ft) | 56 | 101 | 31 | 31 |
| Average Queue (ft) | 28 | 24 | 2 | 7 |
| 95th Queue (ft) | 46 | 61 | 14 | 28 |
| Link Distance (ft) | 1216 | | | 375 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | 150 | 120 | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Network Summary

| |
|---------------------------------|
| Network wide Queuing Penalty: 4 |
|---------------------------------|

HCM Signalized Intersection Capacity Analysis

3: Walnut & Klein

Future (Proposed) PM
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|------------------------|-------|------|-------|------|-------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 404 | 383 | 158 | 372 | 509 | 213 |
| Future Volume (vph) | 404 | 383 | 158 | 372 | 509 | 213 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 0.95 | 0.95 | 1.00 |
| Frt | 0.94 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.97 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3293 | 1441 | 1770 | 3471 | 3539 | 1482 |
| Flt Permitted | 0.97 | 1.00 | 0.20 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3293 | 1441 | 374 | 3471 | 3539 | 1482 |
| Peak-hour factor, PHF | 0.84 | 0.53 | 0.90 | 0.94 | 0.68 | 0.83 |
| Adj. Flow (vph) | 481 | 723 | 176 | 396 | 749 | 257 |
| RTOR Reduction (vph) | 170 | 235 | 0 | 0 | 0 | 152 |
| Lane Group Flow (vph) | 651 | 148 | 176 | 396 | 749 | 105 |
| Heavy Vehicles (%) | 2% | 2% | 2% | 4% | 2% | 9% |
| Turn Type | Prot | Prot | pm+pt | NA | NA | Perm |
| Protected Phases | 2 | 2 | 3 | 8 | 4 | |
| Permitted Phases | | | 8 | | | 4 |
| Actuated Green, G (s) | 26.5 | 26.5 | 39.5 | 39.5 | 25.9 | 25.9 |
| Effective Green, g (s) | 26.5 | 26.5 | 39.5 | 39.5 | 25.9 | 25.9 |
| Actuated g/C Ratio | 0.35 | 0.35 | 0.53 | 0.53 | 0.35 | 0.35 |
| Clearance Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 1163 | 509 | 366 | 1828 | 1222 | 511 |
| v/s Ratio Prot | c0.20 | 0.10 | c0.06 | 0.11 | c0.21 | |
| v/s Ratio Perm | | | 0.19 | | | 0.07 |
| v/c Ratio | 0.56 | 0.29 | 0.48 | 0.22 | 0.61 | 0.21 |
| Uniform Delay, d1 | 19.5 | 17.5 | 11.0 | 9.5 | 20.4 | 17.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.73 | 0.67 |
| Incremental Delay, d2 | 1.9 | 1.4 | 1.0 | 0.3 | 1.9 | 0.7 |
| Delay (s) | 21.5 | 18.9 | 12.0 | 9.8 | 16.7 | 12.4 |
| Level of Service | C | B | B | A | B | B |
| Approach Delay (s) | 20.7 | | | 10.5 | 15.6 | |
| Approach LOS | C | | | B | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 16.7 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.57 | | |
| Actuated Cycle Length (s) | 75.0 | Sum of lost time (s) | 13.5 |
| Intersection Capacity Utilization | 49.6% | ICU Level of Service | A |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Unsignalized Intersection Capacity Analysis
5: Klein & Roadrunner/Stoeger

Future (Proposed) PM
07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|------|-------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | ↕ | | | ↕ | | ↕ | ↕ | | ↕ | ↕ | |
| Traffic Volume (veh/h) | 17 | 0 | 13 | 0 | 3 | 21 | 15 | 640 | 9 | 65 | 787 | 56 |
| Future Volume (Veh/h) | 17 | 0 | 13 | 0 | 3 | 21 | 15 | 640 | 9 | 65 | 787 | 56 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.71 | 1.00 | 0.30 | 1.00 | 0.25 | 0.58 | 0.63 | 0.90 | 0.75 | 0.81 | 0.73 | 0.64 |
| Hourly flow rate (vph) | 24 | 0 | 43 | 0 | 12 | 36 | 24 | 711 | 12 | 80 | 1078 | 88 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | | | | | |
| Median storage veh | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 1728 | 2053 | 583 | 1507 | 2091 | 362 | 1166 | | | 723 | | |
| vC1, stage 1 conf vol | 1282 | 1282 | | 765 | 765 | | | | | | | |
| vC2, stage 2 conf vol | 446 | 771 | | 742 | 1326 | | | | | | | |
| vCu, unblocked vol | 1728 | 2053 | 583 | 1507 | 2091 | 362 | 1166 | | | 723 | | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.2 | | | 4.1 | | |
| tC, 2 stage (s) | 6.5 | 5.5 | | 6.5 | 5.5 | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.3 | | | 2.2 | | |
| p0 queue free % | 84 | 100 | 91 | 100 | 93 | 94 | 96 | | | 91 | | |
| cM capacity (veh/h) | 148 | 176 | 456 | 224 | 162 | 635 | 573 | | | 875 | | |
| Direction, Lane # | | | | | | | | | | | | |
| | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 | | | | |
| Volume Total | 67 | 48 | 24 | 474 | 249 | 80 | 719 | 447 | | | | |
| Volume Left | 24 | 0 | 24 | 0 | 0 | 80 | 0 | 0 | | | | |
| Volume Right | 43 | 36 | 0 | 0 | 12 | 0 | 0 | 88 | | | | |
| cSH | 261 | 367 | 573 | 1700 | 1700 | 875 | 1700 | 1700 | | | | |
| Volume to Capacity | 0.26 | 0.13 | 0.04 | 0.28 | 0.15 | 0.09 | 0.42 | 0.26 | | | | |
| Queue Length 95th (ft) | 25 | 11 | 3 | 0 | 0 | 8 | 0 | 0 | | | | |
| Control Delay (s) | 23.5 | 16.3 | 11.6 | 0.0 | 0.0 | 9.5 | 0.0 | 0.0 | | | | |
| Lane LOS | C | C | B | | | A | | | | | | |
| Approach Delay (s) | 23.5 | 16.3 | 0.4 | | | 0.6 | | | | | | |
| Approach LOS | C | C | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 1.6 | | | | | | | | | |
| Intersection Capacity Utilization | | | 45.3% | | ICU Level of Service | | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis
8: Klein & Dove Crossing

Future (Proposed) PM
07/26/2018



| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
|-----------------------------------|------|------|-------|----------------------|------|------|------|
| Lane Configurations | | | | | | | |
| Traffic Volume (veh/h) | 66 | 51 | 21 | 638 | 866 | 114 | |
| Future Volume (Veh/h) | 66 | 51 | 21 | 638 | 866 | 114 | |
| Sign Control | Stop | | | Free | Free | | |
| Grade | 0% | | | 0% | 0% | | |
| Peak Hour Factor | 0.87 | 0.67 | 0.88 | 0.92 | 0.81 | 0.68 | |
| Hourly flow rate (vph) | 76 | 76 | 24 | 693 | 1069 | 168 | |
| Pedestrians | | | | | | | |
| Lane Width (ft) | | | | | | | |
| Walking Speed (ft/s) | | | | | | | |
| Percent Blockage | | | | | | | |
| Right turn flare (veh) | | | | | | | |
| Median type | | | | | | | |
| TWLTL TWLTL | | | | | | | |
| Median storage veh | | | | | | | |
| 2 2 | | | | | | | |
| Upstream signal (ft) | | | | | | | |
| pX, platoon unblocked | | | | | | | |
| vC, conflicting volume | 1548 | 618 | 1237 | | | | |
| vC1, stage 1 conf vol | 1153 | | | | | | |
| vC2, stage 2 conf vol | 394 | | | | | | |
| vCu, unblocked vol | 1548 | 618 | 1237 | | | | |
| tC, single (s) | 6.8 | 7.0 | 4.3 | | | | |
| tC, 2 stage (s) | 5.8 | | | | | | |
| tF (s) | 3.5 | 3.4 | 2.3 | | | | |
| p0 queue free % | 69 | 82 | 95 | | | | |
| cM capacity (veh/h) | 245 | 422 | 522 | | | | |
| Direction, Lane # | EB 1 | EB 2 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |
| Volume Total | 76 | 76 | 24 | 346 | 346 | 713 | 524 |
| Volume Left | 76 | 0 | 24 | 0 | 0 | 0 | 0 |
| Volume Right | 0 | 76 | 0 | 0 | 0 | 0 | 168 |
| cSH | 245 | 422 | 522 | 1700 | 1700 | 1700 | 1700 |
| Volume to Capacity | 0.31 | 0.18 | 0.05 | 0.20 | 0.20 | 0.42 | 0.31 |
| Queue Length 95th (ft) | 32 | 16 | 4 | 0 | 0 | 0 | 0 |
| Control Delay (s) | 26.1 | 15.4 | 12.2 | 0.0 | 0.0 | 0.0 | 0.0 |
| Lane LOS | D | C | B | | | | |
| Approach Delay (s) | 20.7 | | 0.4 | | | 0.0 | |
| Approach LOS | C | | | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 1.6 | | | | |
| Intersection Capacity Utilization | | | 37.9% | ICU Level of Service | A | | |
| Analysis Period (min) | | | 15 | | | | |

HCM Signalized Intersection Capacity Analysis
10: Klein & FM 725

Future (Proposed) PM
07/26/2018



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|-------|------|-------|------|------|-------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 42 | 1983 | 597 | 434 | 1764 | 12 | 363 | 12 | 358 | 9 | 3 | 18 |
| Future Volume (vph) | 42 | 1983 | 597 | 434 | 1764 | 12 | 363 | 12 | 358 | 9 | 3 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | 5.2 | 5.2 | 5.2 | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 0.97 | 0.91 | | 0.97 | 0.95 | 0.95 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.87 | 0.85 | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1736 | 4940 | 1583 | 3367 | 4979 | | 3433 | 1509 | 1475 | 1770 | 1653 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1736 | 4940 | 1583 | 3367 | 4979 | | 3433 | 1509 | 1475 | 1770 | 1653 | |
| Peak-hour factor, PHF | 0.58 | 0.87 | 0.93 | 0.88 | 0.93 | 0.50 | 0.80 | 0.50 | 0.92 | 0.38 | 0.25 | 0.50 |
| Adj. Flow (vph) | 72 | 2279 | 642 | 493 | 1897 | 24 | 454 | 24 | 389 | 24 | 12 | 36 |
| RTOR Reduction (vph) | 0 | 0 | 201 | 0 | 1 | 0 | 0 | 150 | 169 | 0 | 34 | 0 |
| Lane Group Flow (vph) | 72 | 2279 | 441 | 493 | 1920 | 0 | 454 | 57 | 37 | 24 | 14 | 0 |
| Heavy Vehicles (%) | 4% | 5% | 2% | 4% | 4% | 2% | 2% | 2% | 4% | 2% | 2% | 2% |
| Turn Type | Prot | NA | Perm | Prot | NA | | Split | NA | Perm | Split | NA | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | | | 8 | 8 | | | 4 |
| Actuated Green, G (s) | 10.8 | 71.8 | 71.8 | 23.2 | 84.2 | | 27.1 | 27.1 | 27.1 | 6.6 | 6.6 | |
| Effective Green, g (s) | 10.8 | 71.8 | 71.8 | 23.2 | 84.2 | | 27.1 | 27.1 | 27.1 | 6.6 | 6.6 | |
| Actuated g/C Ratio | 0.07 | 0.48 | 0.48 | 0.15 | 0.56 | | 0.18 | 0.18 | 0.18 | 0.04 | 0.04 | |
| Clearance Time (s) | 5.2 | 5.7 | 5.7 | 5.2 | 5.7 | | 5.2 | 5.2 | 5.2 | 5.2 | 5.2 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 124 | 2364 | 757 | 520 | 2794 | | 620 | 272 | 266 | 77 | 72 | |
| v/s Ratio Prot | 0.04 | c0.46 | | c0.15 | 0.39 | | c0.13 | 0.04 | | c0.01 | 0.01 | |
| v/s Ratio Perm | | | 0.28 | | | | | | 0.03 | | | |
| v/c Ratio | 0.58 | 0.96 | 0.58 | 0.95 | 0.69 | | 0.73 | 0.21 | 0.14 | 0.31 | 0.19 | |
| Uniform Delay, d1 | 67.4 | 37.9 | 28.3 | 62.8 | 23.5 | | 58.0 | 52.3 | 51.7 | 69.5 | 69.1 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 0.98 | 0.99 | 1.10 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 6.8 | 11.8 | 3.3 | 26.7 | 1.4 | | 4.3 | 0.4 | 0.2 | 2.3 | 1.3 | |
| Delay (s) | 74.2 | 49.7 | 31.5 | 89.5 | 24.9 | | 61.0 | 52.2 | 57.1 | 71.8 | 70.4 | |
| Level of Service | E | D | C | F | C | | E | D | E | E | E | |
| Approach Delay (s) | | 46.4 | | | 38.1 | | | 58.0 | | | 70.9 | |
| Approach LOS | | D | | | D | | | E | | | E | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 45.1 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.88 | | |
| Actuated Cycle Length (s) | 150.0 | Sum of lost time (s) | 21.3 |
| Intersection Capacity Utilization | 81.1% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

Intersection: 3: Walnut & Klein

| Movement | EB | EB | EB | NB | NB | NB | SB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|------|------|-----|
| Directions Served | L | LR | R | L | T | T | T | T | R |
| Maximum Queue (ft) | 265 | 327 | 175 | 138 | 137 | 98 | 163 | 291 | 125 |
| Average Queue (ft) | 134 | 171 | 77 | 71 | 75 | 41 | 90 | 119 | 81 |
| 95th Queue (ft) | 210 | 280 | 190 | 118 | 128 | 89 | 149 | 211 | 148 |
| Link Distance (ft) | 312 | 312 | | | 340 | 340 | 1094 | 1094 | |
| Upstream Blk Time (%) | | 1 | | | | | | | |
| Queuing Penalty (veh) | | 0 | | | | | | | |
| Storage Bay Dist (ft) | | | 150 | 150 | | | | | 100 |
| Storage Blk Time (%) | | 10 | 1 | 0 | 0 | | | 10 | 0 |
| Queuing Penalty (veh) | | 18 | 2 | 0 | 0 | | | 22 | 1 |

Intersection: 5: Klein & Roadrunner/Stoeger

| Movement | EB | WB | NB | SB |
|-----------------------|-----|-----|-----|-----|
| Directions Served | LTR | LTR | L | L |
| Maximum Queue (ft) | 55 | 55 | 28 | 52 |
| Average Queue (ft) | 22 | 16 | 8 | 20 |
| 95th Queue (ft) | 50 | 45 | 28 | 48 |
| Link Distance (ft) | 515 | 438 | | |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | 150 | 150 |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 8: Klein & Dove Crossing

| Movement | EB | EB | NB | SB |
|-----------------------|-----|-----|-----|------|
| Directions Served | L | R | L | TR |
| Maximum Queue (ft) | 117 | 69 | 31 | 22 |
| Average Queue (ft) | 51 | 35 | 12 | 1 |
| 95th Queue (ft) | 102 | 58 | 36 | 7 |
| Link Distance (ft) | 596 | 596 | | 1216 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | 150 | |
| Storage Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |

Intersection: 10: Klein & FM 725

| Movement | EB | EB | EB | EB | EB | WB | WB | WB | WB | WB | NB | NB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
| Directions Served | L | T | T | T | R | L | L | T | T | TR | L | L |
| Maximum Queue (ft) | 174 | 386 | 410 | 386 | 275 | 262 | 275 | 391 | 391 | 367 | 225 | 259 |
| Average Queue (ft) | 66 | 383 | 368 | 288 | 198 | 199 | 248 | 268 | 246 | 175 | 122 | 137 |
| 95th Queue (ft) | 146 | 401 | 431 | 443 | 325 | 276 | 304 | 423 | 390 | 314 | 191 | 201 |
| Link Distance (ft) | | 371 | 371 | 371 | | | | 352 | 352 | 352 | | 1216 |
| Upstream Blk Time (%) | | 25 | 10 | 5 | | | | 3 | 2 | 0 | | |
| Queuing Penalty (veh) | | 0 | 0 | 0 | | | | 0 | 0 | 0 | | |
| Storage Bay Dist (ft) | 150 | | | | 250 | 250 | 250 | | | | 250 | |
| Storage Blk Time (%) | 0 | 38 | | 5 | 3 | 0 | 9 | 4 | | | | 1 |
| Queuing Penalty (veh) | 0 | 16 | | 29 | 20 | 1 | 55 | 19 | | | | 1 |

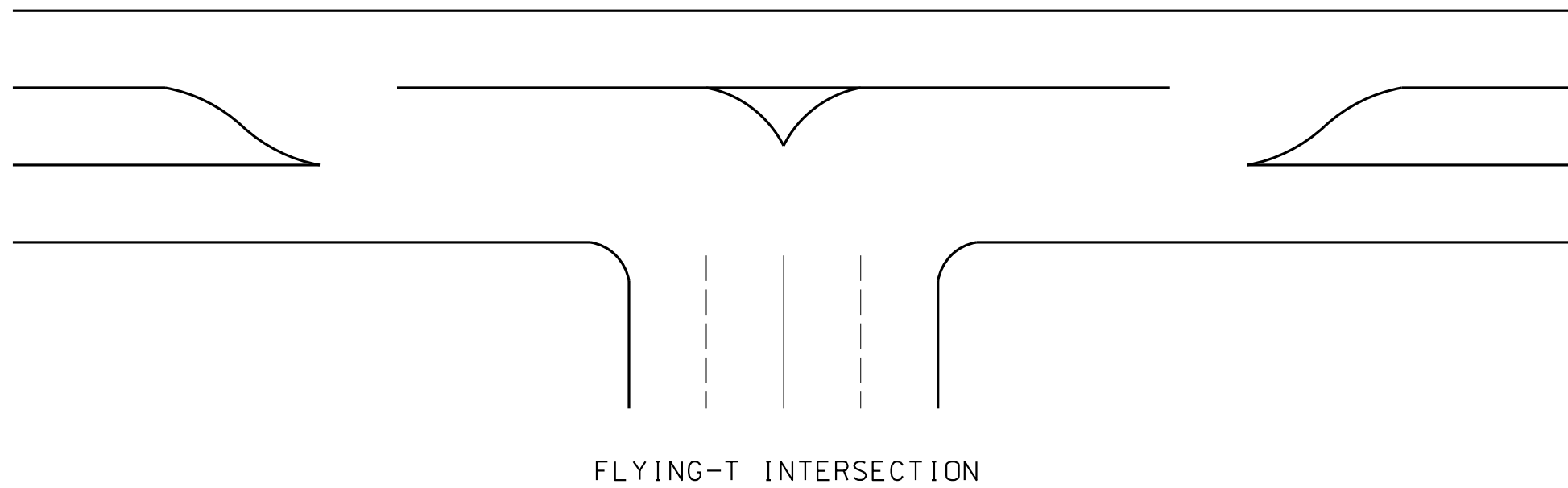
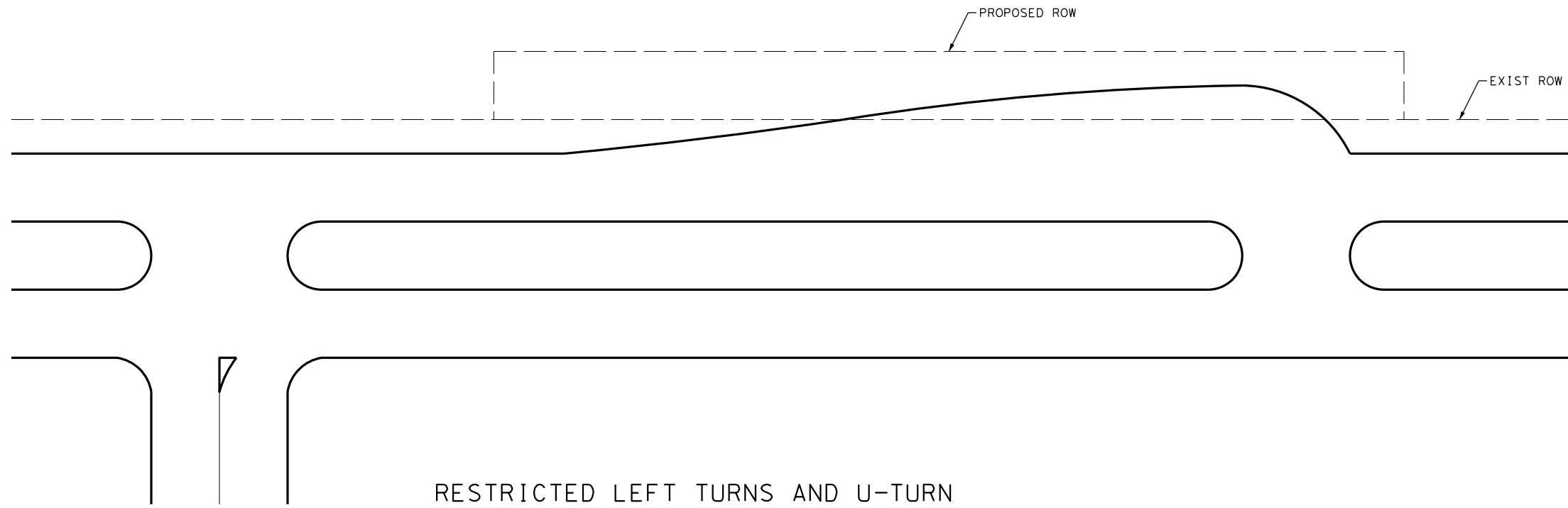
Intersection: 10: Klein & FM 725

| Movement | NB | NB | SB | SB |
|-----------------------|------|-----|-----|-----|
| Directions Served | TR | R | L | TR |
| Maximum Queue (ft) | 139 | 166 | 50 | 53 |
| Average Queue (ft) | 87 | 91 | 15 | 17 |
| 95th Queue (ft) | 137 | 158 | 40 | 43 |
| Link Distance (ft) | 1216 | | | 375 |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | 150 | 120 | |
| Storage Blk Time (%) | 0 | 1 | | |
| Queuing Penalty (veh) | 0 | 2 | | |

Network Summary


| |
|-----------------------------------|
| Network wide Queuing Penalty: 188 |
|-----------------------------------|

APPENDIX C7



**Pape-Dawson
ENGINEERS**

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